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OPEN Near-field collimation of light carrying orbital angular momentum with bull's-eyeassisted plasmonic coaxial waveguides

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The orbital angular momentum (OAM) of light, as an emerging hotspot in optics and photonics, introduces many degrees of freedom for applications ranging from optical communication and quantum processing to micromanipulation. To achieve a high degree of integration, optical circuits for OAM light are essential, which are, however, challenging in the optical regime owing to the lack of well-developed theory. Here we provide a scheme to guide and collimate the OAM beam at the micro- and nano-levels. The coaxial plasmonic slit was exploited as a naturally occurring waveguide for light carrying OAM. Concentric grooves etched on the output surface of the coaxial waveguide were utilized as a plasmonic metasurface to couple the OAM beam to free space with greatly increased beam directivity. Experimental results at $\lambda = 532$ nm validated the novel transportation and collimating effect of the OAM beam. Furthermore, dynamic tuning of the topological charges was demonstrated by using a liquid crystal spatial light modulator (SLM).

In the modern theory of quantum physics, light possesses a range of properties that are historically thought to belong to particles and waves, respectively. The understanding of the relation between the particle-like and wave-like properties is of both fundamental and practical interest^{1,2}. As one of the particle-like properties of light, the optical momentum manifests itself in the mechanical interaction with matter, i.e., the momentum transfer between light and the objects^{3,4}.

Among the various kinds of momenta, the orbital angular momentum (OAM) of light has attracted special attention immediately after it was discovered by Allen et al. in 1992⁵. The OAM beam is typically characterized by a doughnut-shaped intensity profile associated with an azimuthal phase term $\exp(i\ell\varphi)$, i.e., a momentum of lh per photon at a quantum level. Nowadays, the unique properties of OAM have been intensively studied and successfully applied in many realms such as optical tweezers^{6,7}, microsco-

In 2004, it was realized that OAM can provide an additional degree of freedom for data multiplexing in optical communications systems¹⁰. The orthogonality of the intrinsically unbounded OAM modes makes it possible to transfer information via each OAM channel. Unfortunately, the diffraction of OAM in free space will eventually lead to the rapid fall-off of the energy on the beam axis where the phase singularity exists. Therefore, it is argued that the OAM is an efficient communication protocol only when the propagation length is less than the Rayleigh length¹¹. In this case, the OAM-based communication

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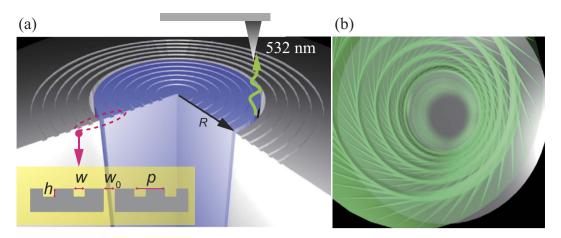


Figure 1. Coaxial waveguide for guiding and collimating OAM beam. (a) Sketch of the waveguide, with grooves etched on the output surface. (b) Schematic diagram of the collimating effect of the OAM beam in free-space.

frame could be considered as a specific solution of the general multiple input multiple output (MIMO) techniques, where orthogonal multi-modes are exploited to enhance the capacity.

In the last several years, the interaction of light with structured material was extensively studied to generate the required OAM states. The diverse structures include liquid crystal spatial light modulator (SLM)⁸, space-variant antenna arrays¹², ring resonators¹³, nano-wires^{14,15} and nano-holes¹⁶⁻¹⁹. Among these devices, plasmonic structures are of particular importance because the development requirement of integrated opto-electro system is becoming more and more urgent²⁰⁻²⁴. Owing to the extremely small effective wavelength²⁵, the OAM modes in the nano-holes and similar plasmonic structures offer great opportunity to reduce the dimension of optical waveguides^{26,27}. Nevertheless, the difficulty of efficient coupling between external light and the plasmonic waveguides is increasing along with the decrease of the waveguide size. As a result of the intrinsic diffraction, the focus spot of free-space OAM light may be much larger than the waveguide mode area, resulting in dramatically reduced coupling efficiency. Similarly, the divergence angle of the OAM beam radiated from the waveguide is inversely proportional to the size of the dielectric core. The mismatch between the waveguide and the light source poses a great challenge for practical on-chip applications.

Here we report the experimental observation of OAM coupling and transportation in plasmonic coaxial waveguides. Owing to the subwavelength core width, extremely large topological charges were demonstrated to be able to transfer in the waveguides. With the aid of circular grooves at the output surface of the waveguide, the guided plasmonic OAM beam was first converted to spiral surface plasmon polariton (SSPP) and then scattered into the far-field. Scanning near-field optical microscopy (SNOM) was utilized to detect the optical fields directly in the near field. By employing liquid crystal SLM as an active element, dynamic change of the topological charge was also enabled.

Results

Principle and numerical results. It is well known that coaxial waveguides in the microwave regime are able to transfer radially polarized modes carrying OAM, whereas their optical counterparts have long been prohibited by the large ohmic loss in the metallic structures. In recent years, it was demonstrated that the plasmonic coaxial waveguides could be used in some special cases by sacrificing the propagation length^{28–32}. Since light is not confined by total internal reflection, sharp bending of wave is possible. Nevertheless, it seems surprising that little work has been reported regarding the OAM transfer in plasmonic coaxial waveguide²⁶. In the following, we show that the coaxial OAM waveguide is able to support the steady propagation of OAM light. With the help of periodic shallow grooves (also known as a type of metasurface²⁵), we demonstrated that the OAM waveguide modes could be efficiently coupled to free-space, accompanied with an enhanced directivity. This new technique can provide much larger degree of freedom compared to fiber-based OAM waveguide³³ because more OAM modes could be utilized in a single waveguide.

The schematic of the plasmonic OAM waveguide is illustrated in Fig. 1(a), where periodic shallow grooves are etched on the metallic surface with a width of w, depth of h, and period of p. The dielectric core is placed at the center of these grooves, with a width of w_0 and radius of R. The whole structure is referred to as a reformed bull's eye, following the definition in previous proposals^{20,24}.

In essence, this plasmonic coaxial waveguide could be treated as a rounded metal-insulator-metal (MIM) waveguide²⁰, where the polarization state changes from transverse magnetic (TM) to radial polarization, i.e., all the electric field vectors are polarized along the radial direction³⁰. After the radially-polarized OAM beam is emitted out from the central slit, SSPP would be excited at the metal-dielectric surfaces

and then coherently scattered by these grooves. As depicted in Fig. 1(b), the superposition of the directly emitted OAM and scattered SSPP could become highly collimated. In principle, the *z*-component of the electric field in the SSPP could be written in a simple form as follows:

$$E_z = A_0 \exp(ik_r r + il\varphi) \tag{1}$$

where A_0 is the amplitude, l is the topological charge of the OAM beam, k_r is the wavevector along the radial direction, which can be calculated by the relation:

$$k_r = \sqrt{\beta^2 - \left(\frac{l}{R}\right)^2} \tag{2}$$

Here β is the wavevector of the SSPP at the metal-dielectric surface²⁵:

$$\beta = n_{eff}k_0 = k_0 \sqrt{\frac{\varepsilon_m \varepsilon_d}{\varepsilon_m + \varepsilon_d}}$$
(3)

where ε_m and ε_d are the dielectric constants of the metal and dielectric, $n_{\rm eff}$ is the effective refractive index, k_0 is the wavevector in free space. In this paper, the metal is chosen as silver (Ag) and dielectric is air. At a wavelength of $\lambda = 532 \, \rm nm^{34}$, the calculated effective refractive index is 1.0524 and the effective wavelength is 505.5 nm.

The coherent scattering of SSPP at the periodically placed grooves can increase the effective radiation width. As a result, the angular width of the radiation pattern would decrease correspondingly. Interestingly, we find that the reduction of the divergence angle in the bull's eye is not only resulted from the increased effective radiation aperture, but also from the contribution of super-oscillatory field, which is a universal phenomenon in electromagnetics as first recognized by Toraldo in 1952³⁵.

As shown in Fig. 2(a), 16 concentric grooves were etched on the two sides of the dielectric core symmetrically. To investigate the impact of geometric parameters on the beaming performance, we focused on the two-dimensional (2D) counterpart of this structure, as indicated by the dashed line along the radial direction. The groove width w and height h were set as 230 nm and 40 nm. The slit radius R and width w_0 were chosen as 7.5 μ m and 230 nm, respectively. Under TM polarized illumination, the magnetic field distributions in the xz plane (Fig. 2(b)) validated the beaming effect, coinciding well with the initial results given by Ebbesen et $al.^{20}$. Figure 2(c) represents the radiation pattern for varying periods between 460 nm and 490 nm (the step is chosen as 10 nm), where the angular full width at half maximum (FWHM) is 8.6°, 5.9°, 4.5°, and 3.6°, respectively.

The most obvious sign of the super-oscillation effect is that the reduction of the angular FWHM is accompanied with the increase of side lobe. As a result, the angular resolution can surpass the limit value set by Abbe and Rayleigh. For the traditional slit-grooves or bull's eye²⁰, super-oscillation effect can be exploited to reduce the angular width. However, for OAM light, the side lobe at one direction may interfere with the main lobe at the opposite side, because of the fact that the main lobe of OAM is in a doughnut shape. Consequently, the side lobe should be confined to some extent so as to reduce the negative impacts on the main lobe. In the rest of this paper, we set the period of the grooves to be $p = 470 \, \text{nm}$, corresponding to a careful balance of the main lobe divergence angle and the side lobe level.

Subsequently, we numerically calculated the electric fields distributions for the spiral surface plasmon for l=2 using commercial software CST MWS. As shown in Fig. 3, the effective radiation aperture is about 5 μ m, corresponding to a divergence angle of 5.7°. As depicted in Fig. 3(c), the SSPP is not propagating along a straight line any more. Instead, it propagates along a spiral line as determined by the topological charge of the incident OAM beam. Owing to the contribution of SSPP, the emitted OAM light becomes highly directional.

Experimental validation. In order to validate our proposal, a sample was fabricated by focused ion beam (FIB) milling on a 300 nm thick silver film deposited on a quartz (SiO₂) substrate. The geometric parameters were chosen as the same as those in the theoretical simulations. Figure 4(a) shows the scanning electron microscope (SEM) image and atomic force microscope (AFM) image of the sample. The inset AFM image indicates that the groove depth is actually about 35 nm. The near field measurement was performed with a scanning near-field optical microscope (SNOM) (Fig. 4(b)). A linearly polarized laser beam at $\lambda = 532$ nm was first transformed into a Laguerre-Gaussian mode through a reflective SLM, and then converted to radial polarization with the help of a rotated waveplate formed by liquid crystal³⁶. The finally collimated radially polarized OAM beam was then projected onto the backside of the sample, with the center of OAM beam superposed with that of the waveguide.

Although the OAM modes with different topological charges are intrinsic orthogonal to each other, all the OAM bemas share similar doughnut-shaped intensity patterns, except that the radius of the doughnut increases with increasing topological charge. In order to characterize the actual topological charge of the OAM beams, traditionally the interference pattern with plane or spherical wave should be exploited^{8,12}. In fact, it is more convenient to use the petal-like interference pattern of two OAM beams with opposite topological charges⁸. The number of petals along the azimuthal direction is just

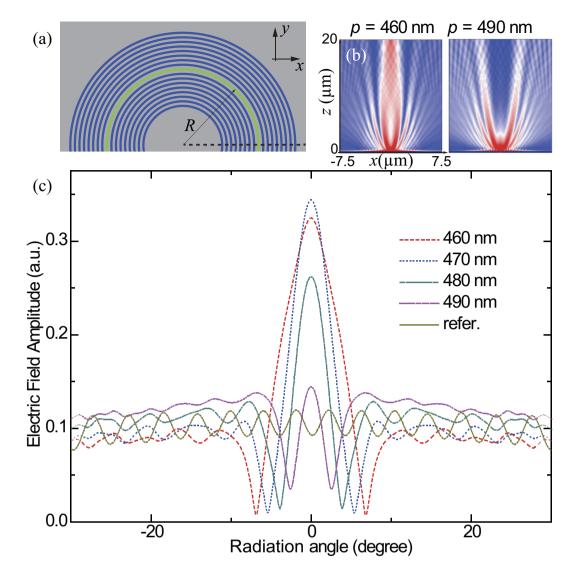


Figure 2. Super oscillation and the beaming effect. (a) Sketch of the circular slit surrounded by both inner and outer grooves. (b) Magnetic field intensity distributions at the xz plane for $p = 460 \,\mathrm{nm}$ and $490 \,\mathrm{nm}$. (c) Far-field electric field amplitudes calculated by Fourier transformation. The radiation angle is defined with respect to the z-axis.

the magnitude of the topological charge. In the experiment, we measured the near-field light intensity above the sample by using two superimposed waves carrying topological changes of $l=\pm 2$. The measured results at $z=750\,\mathrm{nm}$, $1650\,\mathrm{nm}$, and $2550\,\mathrm{nm}$ are illustrated in Fig. 4(c), with small divergence as z increases. Figure 4(d) depicts the horizontal positions of the petals at different positions of z. The angular width was evaluated to be near $\alpha=15.18^{\circ}$ at $z=1\mu\mathrm{m}$, which is larger than the theoretical evaluated result. This difference may be stemmed from the variation of the dielectric constants of metal from the values in Ref. [34], since they are highly dependent on the evaporation environment, especially when the thickness is only hundreds of nanometers. Furthermore, the fabricated sample is still not perfect, as can be seen in the AFM image (the inset of Fig. 4(a)).

One well-known property of the OAM waveguide is that there is a maximal topological charge for a given radius, above which the wave-vector along the propagating direction is imaginary, thus light is prohibited to propagate. For our coaxial OAM waveguide, the wavevector along the z direction follows³⁷:

$$k_z = \sqrt{{\beta_1}^2 - \left(\frac{l}{R}\right)^2} \,, \tag{4}$$

where β_1 is the propagation constant of normal SPP inside a MIM waveguide. The characteristic equation of the fundamental TM mode is²³:

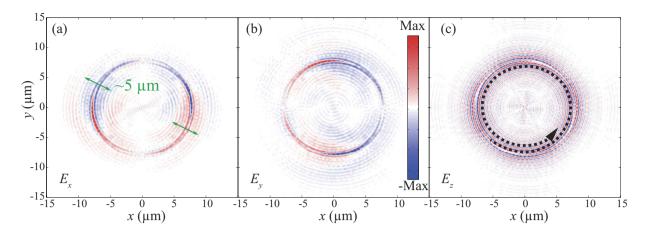


Figure 3. Spiral surface plasmon generated by the OAM light. (a-c) Real parts of the Electric fields polarized along the x, y, and z directions at the xy plane ($z = 0 \,\mu\text{m}$). The effective radiation aperture width is about $5 \,\mu\text{m}$ as indicated in (a). The spiral equal-phase line is indicated in (c).

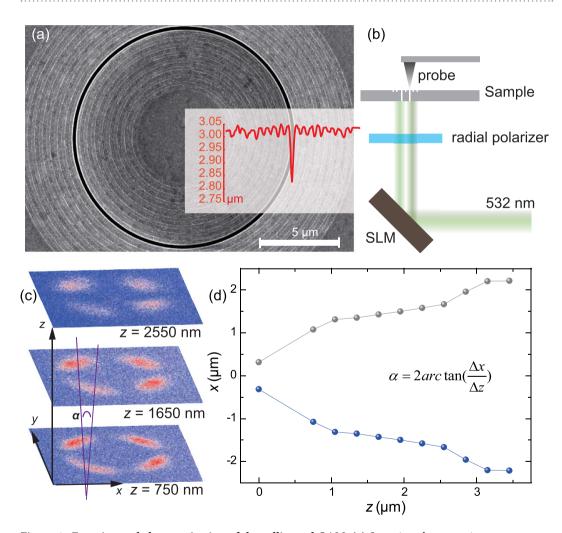


Figure 4. Experimental characterization of the collimated OAM. (a) Scanning electron microscope (SEM) image of the fabricated sample. Inset shows the atomic force microscope (AFM) image. (b) Setup of the measurement. (c) Measured near-field intensity at the xy plane for $l=\pm 2$ at different distances away from the sample surface. The length and width along the x and y directions are both $20\,\mu\text{m}$. (d) Horizontal positions of the petals at different z.

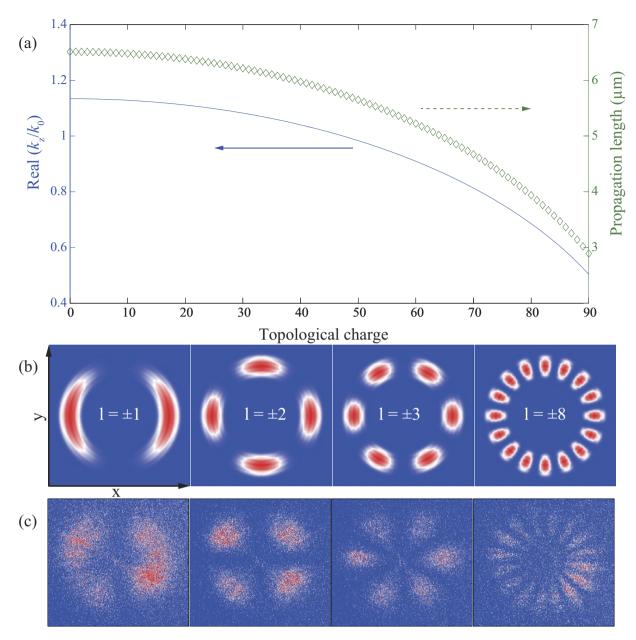


Figure 5. Dependence of the beaming effect on the topological charge. (a) Normalized propagation constants and propagation lengths for different topological charges. (b) Theoretically calculated and (c) experimentally measured petal beams at $z=10\,\mu\text{m}$. The corresponding topological charges are marked in (b). The length and width along the x and y directions in all panels are $20\,\mu\text{m}$.

$$\tanh\left(\sqrt{\beta_1^2 - \varepsilon_d k_0^2} w_0/2\right) = -\frac{\varepsilon_d \sqrt{\beta_1^2 - \varepsilon_m k_0^2}}{\varepsilon_m \sqrt{\beta_1^2 - \varepsilon_d k_0^2}},\tag{5}$$

where k_0 stands for the vacuum wavevector, ε_m and ε_d are the permittivities for the metal and dielectric media, and w_0 is the width of the waveguide core. The propagation length, defined as the distance at which the intensity decrease to 1/2.71828 of its original value, can be calculated by 1/(2Im(k_z)). As shown in Fig. 5(a), the propagation lengths in the designed waveguides are limited to be several microns for almost all topological charges.

When the guided OAM is coupled to the free-space, the dispersion relation at the output surface becomes:

$$k_z = \sqrt{k_0^2 - \left(\frac{l}{R}\right)^2} \,. \tag{6}$$

It seems that such a waveguide is able to support OAM with high topological charge approximating l=90. Nevertheless, the practical topological charge may be much smaller than that obtained through equation (6). This is because that additional wavevector along the radial direction was ignored, which is stemming from the uncertainty principle $\Delta k_r \Delta r \geq 2\pi$, where Δr is the effective width of the petal beam. Owing to the contribution of non-vanishing Δk_r , the actual propagation constant in free-space should be:

$$k_z = \sqrt{k_0^2 - \left(\frac{l}{R}\right)^2 - k_r^2} \,. \tag{7}$$

The above theoretical investigation only provides limited physical insight and guidance for the understanding of the OAM beaming effect. For a more accurate description, the beaming effect was calculated using vectorial diffraction theory³⁸ by assuming an OAM beam with an effective aperture lies between $r_1 = 4.5$ and $r_2 = 10.5$. The results at $z = 10 \,\mu\text{m}$ for $l = \pm 1, \pm 2, \pm 3$ and ± 8 are plotted in Fig. 5(b), in good agreement with the experimental results shown in Fig. 5(c). The deterioration in the experimental performance for larger l may be resulted from the inaccuracy in the experimental process. For example, since there are no coupling grooves fabricated at the entrance size of the waveguide, only a small part of energy can be converted to the waveguide. Combining with the fact that limited energy can be collected by the probe of the SNOM, it is not strange that the signal-to-noise ratio is not high. In order to enhance the efficiency, coupling grooves at the entrance side can be exploited in future experiments.

Discussion

In summary, we have demonstrated a plasmonic coaxial-waveguide-based scheme to transfer OAM beam with sub-wavelength mode confinement. Periodic and concentric grooves are used to coherently scatter the spiral surface plasmon to obtain collimated OAM beam. We found that the divergence angle reduction is accompanied with both the enlargement of the effective radiation aperture and the super-oscillatory superposition of diffracted electromagnetic fields. By employing the previous techniques used for surface plasmon engineering^{20,39}, the angular distribution of OAM beam can be more precisely controlled by properly choosing the geometry of the grooves at the waveguide output surface. We also noted that there are various designs of micro- and nano-scale OAM generators reported in recent years^{4,12,13}. By integrating these devices with the OAM waveguide, further enhancement of performance is foreseeable.

Although the plasmonic devices have a relatively large propagation loss, they are still feasible for on-chip applications²⁸. For long-range propagation of OAM beam, cylindrical multilayers can be exploited to mimic the near-perfect reflection properties of metals and form all-dielectric coaxial waveguides⁴⁰.

Methods

Numerical simulation. The commercial solvers CST microwave studio and COMSOL Multiphysics were used for the numerical evaluation of the 3D and 2D structure, respectively. Since the memory requirement for the 3D structure is much larger than its 2D counterpart, we only simulated a relatively small propagation distance (1 micron) along the *z*-direction. The electric fields at this output plane were then used as the input for a home-made solver based on vectorial plane wave expansion. The results of the 3D and 2D structures are comparable to each other.

Sample fabrication. The sample was fabricated on a 1 mm thick quartz substrate. A 300-nm-thick Ag film was deposited on the cleaned substrate by magnetron sputtering in a sputter chamber. The sputter-deposition rate for Ag was $R_{\rm Ag} \approx 0.83 \, \rm nms^{-1}$. The slit and grooves were then milled on the Ag film using a Ga⁺ focused ion beam (FIB, FEI Helios Nanolab 650), and the accelerating voltage and current of the Ga⁺ beam were set as 30 KV and 24 pA, respectively.

Measurement. The near field measurement was performed with a scanning near-field optical microscope (SNOM). A continuous-wave (CW) laser with vacuum wavelength of 532 nm (Cobolt SambaTM) was used as the light source. After passing through the beam extender and polarizing filter, the laser beam was exposed to a spatial light modulator (SLM). There are 1980×1080 pixels on SLM (Holoeye, Pluto, phase only SLM). The size of each pixel is $8\,\mu\mathrm{m} \times 8\,\mu\mathrm{m}$. We could independently control the phase of every pixel with a computer by creating a grey-scale map. Different grey levels (0–255) correspond to the different phases (0–2 π). In this way, orbital angular momenta with different topological charges were added to the laser beam. Subsequently, a radial polarization converter (ARCoptix Switzerland) was used to convert the linear polarized OAM beam to radially polarized OAM. The propagation behavior of the OAM beam after passing through the designed sample were experimentally measured using a SNOM (NT-MDT, NTEGRA Solaris). When the probe (MF112_NTF) approached the surface of the sample, the elongation distance of the tube was recorded. After we turned off the feedback of the head, the tube

would retract the same distance. So in this way, we could control the distance between the probe and the sample surface. The scanning size was chosen to be $20\,\mu\text{m} \times 20\,\mu\text{m}$, with points of 300×300 , and the scanning velocity was $10\,\mu\text{m/s}$.

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Author Contributions

M.B.P., X.L.M. and Z.Y.Z. contributed equally in the design and analysis of the experiment. X.L., Y.Q.W. and H.G. characterized the sample. C.G.H., P.G. and C.T.W. fabricated the sample. M.B.P. and X.G.L. wrote the manuscript. All the authors contributed to the discussion of the results. X.G.L. proposed the original idea and supervised the project.

Additional Information

Competing financial interests: The authors declare no competing financial interests.

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