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B.M. (boris.mizaikoff@
uni-ulm.de)Real-time monitoring of ozone in air using
substrate-integrated hollow waveguide
mid-infrared sensorsJoão Flávio da Silveira Petrucci^{1,2}, Paula Regina Fortes^{2,3}, Vjekoslav Kokoric², Andreas Wilk²,
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Ozone is a strong oxidant that is globally used as disinfection agent for many purposes including indoor building air cleaning, during food preparation procedures, and for control and killing of bacteria such as *E. coli* and *S. aureus*. However, it has been shown that effective ozone concentrations for controlling e.g., microbial growth need to be higher than 5 ppm, thereby exceeding the recommended U.S. EPA threshold more than 10 times. Consequently, real-time monitoring of such ozone concentration levels is essential. Here, we describe the first online gas sensing system combining a compact Fourier transform infrared (FTIR) spectrometer with a new generation of gas cells, a so-called substrate-integrated hollow waveguide (iHWG). The sensor was calibrated using an UV lamp for the controlled generation of ozone in synthetic air. A calibration function was established in the concentration range of 0.3–5.4 mmol m^{−3} enabling a calculated limit of detection (LOD) at 0.14 mmol m^{−3} (3.5 ppm) of ozone. Given the adaptability of the developed IR sensing device toward a series of relevant air pollutants, and considering the potential for miniaturization e.g., in combination with tunable quantum cascade lasers in lieu of the FTIR spectrometer, a wide range of sensing and monitoring applications of beyond ozone analysis are anticipated.

During recent decades, ozone has evolved into the main disinfection agent at a global scale¹. Due to its substantial oxidation potential (+ 2.07 V vs. standard hydrogen electrode) and facile generation, ozone is nowadays used in a wide variety of disinfection scenarios such eliminating indoor odors², food preservation³, residential air cleaning⁴, treatment of carious lesions⁵, and for microbial control⁶.

The effect of ozone on the human health was initially reported as an irritant gas⁷. However, long-term exposure has been proven to potentially result in decrease of lung function and respiratory diseases such as asthma^{8,9}. The Environmental Protection Agency of the United States (U.S. E.P.A) has therefore established an ozone threshold of 0.08 ppm for an exposure period of 8 hours, and 0.09 ppm for an exposure period of 1 hour. Complementarily, the World Health Organization (WHO) has limited the ozone threshold at 0.06 ppm for an exposure period of 8 hours¹⁰.

However, the apparent disinfection power of ozone is limited at concentrations yielding such exposure limits^{7,11}. Moreover, most commercial ozone generators produce substantially higher levels of ozone by nature of the generation process, i.e., via electrical discharge (corona) or by photoreaction with ultraviolet (UV) radiation^{12,13}. Consequently, a series of studies have reported that useful ozone levels for disinfection readily exceed the regulated ozone concentrations by a factor of ten or more^{14,15}.

As ozone is a highly reactive compound, indirect chemical methods are frequently used for its determination. However, secondary reactions and other oxidizing species may affect the accuracy of the obtained results¹⁶. Iodometry, based on the reaction between ozone and iodide forming the colored ion triiodide (I₃[−]) is to date the standard method for the - indirect - determination of high levels of ozone in air¹⁷. Among other practical limitations for in-field usage, this method is not suitable for real-time analysis. As ozone is an excellent UV absorber, UV spectroscopy based and chemiluminescent analyzers have been considered the most sensitive techniques for online monitoring to date^{18,19}. Nevertheless, other absorbing constituents in the UV wavelength range may cause false positive signals²⁰; also, considerable costs and the rather bulky dimensions are major arguments against widespread field usage.

Figure 1 | (a) Calibration curve of ozone determination, (b) Continuous online monitoring of ozone concentrations in real-time, and (c) contour plot (top view) of the ozone plume migrating through the iHWG via 2D IR-spectra of the spectral region comprising the relevant ozone IR signatures; the color bar encodes the absorption intensity (i.e., the ozone concentration) from low (blue) to high (red).

Even though ozone has distinct absorption features at mid-infrared frequencies, the use of mid-infrared (MIR) sensing techniques for quantification in indoor and outdoor air has not been reported in literature. This may be attributed to the fact that until recently the bulkiness and cost of instrumentation along with the moderate sensitivity rendered this wavelength regime less suitable for environmental and especially for atmospheric analysis, which demands analyzing ozone concentrations at approximately 5–100 ppb. At these trace levels, to date only chemiluminescence, high-resolution FTIR and UV spectroscopy based methods are applicable^{21–23}.

However, as mentioned above a series of applications requires the detection of ozone at elevated concentration levels. Serra et al. have evaluated the use of ozone to reduce molds in a cheese ripening room via the generation of 8 g h⁻¹¹⁵. 5 ppm of ozone was used during 60 minutes in order to disinfect vegetables³. For building disinfections purposes, 24 materials were exposed for 16 h to ozone concentrations of 1000 – 1200 ppm¹⁴. Particularly for these types of applications, real-time monitoring of ozone is essential. The approach presented herein takes advantage of the inherent molecular selectivity provided by mid-infrared vibrational spectroscopy using particularly compact and portable FTIR spectrometers combined with a new

generation of miniaturized gas cells based on hollow waveguide technology.

A hollow waveguide (HWG) may generally be described as a light pipe made from dielectric materials or metals with a coaxial hollow core enabling radiation propagation by reflection at the inside wall²⁴. If gaseous samples are injected into the hollow core, the HWG may simultaneously act as a miniaturized gas cell with a well-defined optical absorption path length, thereby enabling quantitative optical analysis²⁵. Recent studies have already demonstrated the utility of HWGs coupled to FTIR spectroscopy operating in the MIR band (3–20 μm) as gas sensing system^{26–31}. Very recently, a fundamentally new generation of hollow waveguides has been developed, so-called substrate-integrated hollow waveguides (iHWG). The most remarkable features are the compact dimensions of the waveguide substrate (75 × 50 × 12 mm; made from aluminum), the adaptable optical path length via integration of a meandered hollow waveguide channel at virtually any desired geometry into an otherwise planar substrate, the small volume of gas sample required for analysis, and the short transient time of such small volumes (few hundred microliters) through the active transducer region facilitating real-time monitoring³².

Table 1 | Analytical performance of the iHWG-FTIR ozone gas sensing system

Parameter	Value
Limit of detection ($3 \times \text{SD}$ of blank)	0.14 mmol m^{-3}
Limit of quantification ($10 \times \text{SD}$ of blank)	0.47 mmol m^{-3}
Correlation coefficient	0.9956
Intra-day repeatability	1.41%
Inter-day repeatability	2.26%
Linear range	$0.36\text{--}5.40 \text{ } \mu\text{mol m}^{-3}$
Regression equation	$A = 0.023 [\text{O}_3]$

As MIR sensing has not been explored as an analytical tool for the quantification and monitoring of ozone in gaseous samples, the present study demonstrate for the first time the capability of this new generation of iHWG-based sensing devices providing a compact, simply assembled, and robust system as a versatile alternative to conventional analytical techniques.

Results

Reproducibility of ozone generation. A critical parameter in chemical analysis is the reliability of standards used for device calibration. As commercial ozone cylinders providing certified standards are not available, any ozone generation must be tested for reproducibility. Here, the precision was evaluated using the peak area at 1055 cm^{-1} during 25 independent measurements of 4.10 mmol m^{-3} of ozone. The achieved intra-day relative standard deviation (RSD) was 1.41%. Inter-day repeatability was determined within three consecutive days, and was better than 2.26%.

Analytical figures-of-merit. For quantitative purposes, a calibration function was established based on the evaluation of the peak area at 1055 cm^{-1} versus the ozone concentration. For each concentration, the mean value of five replicate measurements was calculated. The goodness of the fit was determined at $r^2 > 0.99$ in the concentration range of 0.36 to 5.40 mmol m^{-3} of ozone following $A = 0.234 [\text{O}_3]$. A represents the peak area at 1055 cm^{-1} and $[\text{O}_3]$ is the ozone

concentration in mmol m^{-3} (Figure 1a) The calculated limit of detection (LOD) was considered to be three times the standard deviation of the blank signal, and was determined at 0.14 mmol m^{-3} (3.49 ppm). The validation results are summarized in Table 1.

Real-time monitoring of ozone. The capabilities of the developed iHWG-FTIR sensor for online monitoring was evaluated by continuously monitoring the sample flow provided from the ozone generator. For this purpose, the UV lamp was switched off at intervals of 1.1 min, in order to instantaneously reduce the ozone concentration, and switched back on after 1.1 min, again producing ozone. The maximum signal value was obtained once the dead volume of the device was completely filled with ozone, which occurred within 55 seconds. The obtained results are shown in Figure 1b and 1c. Excellent reproducibility of the peak height, and of the transient signal for different ozone concentrations was obtained.

Discussion

Within the mid-infrared band, the most pronounced band of ozone is located at 1055 cm^{-1} , and is associated with the ν_3 asymmetric stretching vibration³³. Furthermore, a Fermi resonance band at 2100 cm^{-1} , associated with the $\nu_1 + \nu_3$ combination band, is evident, yet though with at least 4-times less intensity. Hence, the peak at 1055 cm^{-1} is most suitable for quantitative data evaluation. Figure 2 shows an exemplary IR spectrum obtained for 5.40 mmol m^{-3} of ozone using the gold-coated iHWG coupled with the FTIR spectrometer. A typical signal-to-noise ratio (SNR) for such measurements was determined at 159.

An online real-time gas sensing system for the quantitative determination of high levels of ozone in air was developed using for the first time substrate-integrated hollow waveguides (iHWG) coupled to an FTIR spectrometer operating in the mid-infrared spectral range. Next to a rapid dynamic response toward concentration changes of 55 s, the sensing device provides an LOD of 0.14 mmol m^{-3} for ozone, with a significant dynamic range suitable for threshold sensing at U.S. EPA and WHO demanded levels. In future, a significant size reduction of the sensing device is anticipated by

Figure 2 | IR spectrum of ozone at a concentration of 5.40 mmol m^{-3} recorded with the iHWG-FTIR sensor at a spectral resolution of 4 cm^{-1} . The obtained signal-to-noise ratio (SNR) was determined at 159.

Figure 3 | (a) Scheme of the O₃ generation system coupled to the gas mixing device and the FTIR-iHWG sensor. (b) Home-made O₃ generation system using a coiled quartz tube (length of coiled segment: 95 cm) and an UV lamp emitting at 185 nm.

replacing the FTIR spectrometer with a suitable tunable quantum cascade laser (QCL)^{24,34–36}. Moreover, the sensitivity may be further improved by extending the optical path length via variation of the meandered waveguide channel geometry integrated into the iHWG, as previously demonstrated³².

Methods

Ozone generation. Synthetic air and nitrogen were provided by MTI Industriegase AG (Neu-Ulm, Germany). Ozone was generated by exposing synthetic air to ultraviolet radiation (UV Technik, Germany) using a home-made quartz tube flow device. This device facilitates the interaction between the sample gas and UV radiation at a wavelength of 185 nm, as illustrated in Figure 3.

Ozone calibration. The obtained ozone concentration was verified using the conventional iodometric method prior to IR analysis¹⁷. The method is based on the reaction between ozone and potassium iodide in buffered solution (pH 6.8; phosphate buffer). The absorbance of the formed triiodide ion was analyzed at 357 nm using an UV-VIS spectrophotometer (SPECORD S600, Analytik Jena, Jena, Germany). A custom-made gas mixing system prototype based on mass flow controllers was developed by the Institute of Analytical and Bioanalytical Chemistry at University of Ulm and Lawrence Livermore National Laboratory, and was used for preparing and delivering synthetic air samples at a flow rate of 20 mL min⁻¹. The obtained concentration of ozone was 5.40 ± 0.80 mmol m⁻³. Dilutions of ozone-containing samples were prepared by mixing different ratios of nitrogen and synthetic air, which were then flown through the quartz tube coiled around the UV lamp at a constant flow rate at 20 mL min⁻¹ for all experiments.

FTIR spectrometer. All measurements reported herein were performed using a compact FTIR spectrometer (IR cube, Bruker Optics Inc, Ettlingen, Germany) equipped with a liquid nitrogen cooled mercury-cadmium-telluride (MCT) detector (Infrared Associates, Stuart/FL, USA). A gold-coated iHWG with an absorption path length of 23 cm and dimensions of 75 × 50 × 12 mm (length × width × depth) was coupled to the spectrometer using off-axis parabolic mirrors with a focal length of 2" (Thorlabs, Germany). The ozone standards were injected into the iHWG at a constant flow rate of 20 mL min⁻¹. The IR spectra were recorded in the range of 4000–650 cm⁻¹ at a spectral resolution of 4 cm⁻¹; 100 spectra were averaged per measurement. The OPUS 6.5 software package (Bruker Optics Inc, Ettlingen, Germany) was used for data acquisition.

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Author contributions

J.F.S.P., V.K., P.R.F., I.M.R.Jr., A.A.C. and B.M. have designed and discussed the experiments. J.F.S.P. and V.K. have performed the experiments. A.W. and B.M. have designed the substrate integrated hollow waveguides. J.F.S.P., A.A.C. and B.M. have written and edited the manuscript. J.F.S.P., V.K. and B.M. contributed to the discussions during data analysis. All authors contributed to discussion of the obtained results, and to assembly of the manuscript.

Additional information

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