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# Facile synthesis of Persian gum–graphene oxide composite as a novel adsorbent for CO<sub>2</sub> capture: characterization and optimization

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Burning fossil fuels releases toxic gases into the environment and has negative effects on it. In this study, Persian gum@Graphene oxide (Pg@GO) was synthesized and used as a novel adsorbent for CO<sub>2</sub> capture. The characterization of materials was determined through XRD, FTIR, FE-SEM, and TGA analysis. The operating parameters including temperature, Pressure, and adsorbent weight were studied and optimized by response surface methodology via Box–Behnken design (RSM-BBD). The highest amount of CO<sub>2</sub> adsorption capacity was 4.80 mmol/g, achieved at 300 K and 7.8 bar and 0.4 g of adsorbent weight. To identify the behavior and performance of the Pg@GO, various isotherm and kinetic models were used to fit with the highest correlation coefficient (R<sup>2</sup>) amounts of 0.955 and 0.986, respectively. The results proved that the adsorption of CO<sub>2</sub> molecules on the adsorbent surface is heterogeneous. Based on thermodynamic results, as the value of ΔG° is –8.169 at 300 K, the CO<sub>2</sub> adsorption process is exothermic, and spontaneous.

**Keywords** CO<sub>2</sub>, Adsorption, Response surface methodology, Persian gum, Thermodynamic

Today, burning fossil fuels as the main energy source causes increases in toxic gases emission such as CO<sub>2</sub>, CO, and NO<sub>x</sub>. These toxic gases have negative effects on the environment such as air pollution, photochemical smog, acid rain, etc.<sup>1</sup>. Therefore scientists try to solve these environmental problems using practical and cost-effective technologies to capture materials like toxic gases<sup>2</sup>. Using solid adsorbents such as covalent organic frameworks (COFs), Mg(OH)<sub>2</sub><sup>3</sup>, DEA solution<sup>4</sup>, graphene oxide (GO), sodium hydroxide (NaOH), and Chitosan is more widely applied because of low equipment corrosion, high-performance good chemical and mechanical properties<sup>5</sup>.

Graphene oxide (GO) is a layer of sp<sup>2</sup> carbon atoms that is obtained from natural graphite through oxidation<sup>6</sup>. GO contains various oxygenated functional groups<sup>7</sup> on its basal planes and edges, such as carboxyl, carbonyl, hydroxyl, and epoxy groups<sup>8,9</sup>. These oxygenated functional groups play a significant role in creating either electrostatic interactions or chemical bonding, GO has the potential to serve as a nano-support for biologically active agents, which can be utilized in the creation of innovative catalysts, solid adsorbent, sensors, and drug delivery systems<sup>10</sup>. Furthermore, GO has been explored as a physical adsorbent for harmful greenhouse gases like CO<sub>2</sub>, whose elevated concentrations can pose serious risks to both the environment and human health<sup>11,12</sup>. So, it is need appropriate method for the declining distribution of CO<sub>2</sub> into the biosphere<sup>13,14</sup>.

The oxygenated functional groups of GO caused alkali in nature. Since the CO<sub>2</sub> molecules are acidic in nature, the strong interaction between GO and CO<sub>2</sub> molecules is formed and helps CO<sub>2</sub> adsorption process<sup>15,16</sup>. Furthermore, due to their hydrophilic nature, GO sheets can be easily integrated into a water-based solution and can be produced as single, double, or multiple layers with exceptional stability. This character makes the both GO surface and its active sites highly effective in improving the capacity of solid adsorption<sup>17</sup>. Although pure GO has limited ability to adsorb CO<sub>2</sub> and N<sub>2</sub>, its capacity can be enhanced by forming diverse structures.

Bio-polymers like chitin, chitosan, and Persian gum have different advantages including economical, eco-friendly, safe, and suitable approaches. In addition, bio-polymer structures usually have amine groups which

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enhance the alkali properties of bio-polymer<sup>18</sup>. One of the bio-polymers is Persian gum (Pg). Persian gum is secreted from *Amygdalus scoparia Spach* and is a non-starch hydrocolloid with an acidic polysaccharide nature. The main part of its body consists of the sugar unit of galactose with a smaller amount of arabinose<sup>19</sup>. It is considered in the pharmaceutical, food, textile industries, etc. The resulting solutions cause the medium to become viscous and have emulsifying, texturing, stabilizing, and suspending properties. This gum consists of two insoluble and soluble parts. Iran is known as a good source of Persian gum<sup>20</sup>. The insoluble part of this gum is less used, therefore, in this work, this part is used for synthesis new adsorbent for CO<sub>2</sub> capture by incorporating with GO.

In this study, Persian gum (Pg) as a biopolymer was used as a part of the solid adsorbent for the CO<sub>2</sub> adsorption process. By mixing Pg with graphene oxide (GO), Pg@GO was synthesized and used as a novel adsorbent for the CO<sub>2</sub> adsorption process. Characterization of the adsorbent was studied via X-ray diffraction (XRD), Field Emission Scanning Microscopy (FESEM), Energy Dispersive X-ray (EDX), Fourier transform infrared spectroscopy (FTIR), Thermogravimetric (TGA) analysis. The response surface methodology (RSM) was used to optimize the effect of various independent parameters including temperature, pressure, and adsorbent weight on CO<sub>2</sub> adsorption capacity. Isotherm, kinetic and thermodynamic models were applied to evaluate the behavior and performance of the adsorption process. Finally, the regeneration of the adsorbent was evaluated at optimum conditions.

## Materials and methods

### Materials

Sulfuric acid (H<sub>2</sub>SO<sub>4</sub>, 98%), nitric acid (HNO<sub>3</sub>, 65%), hydrochloric acid (HCl, 37%), and potassium chloride (KClO<sub>3</sub>, 99%) were collected from Merck company and used without any purification. Carbon dioxide (CO<sub>2</sub>) gas was purchased from Hmtagas company.

### Synthesis GO

The study involved creating GO using a modified version of the Hummers and Offeman method, which overcomes the drawbacks of previous methods and produces high-quality and pure GO<sup>21</sup>. To prepare the GO, two different acids including sulfuric acid and nitric acid were combined in a ratio of 2:1, and graphite powder was added. The mixture was then placed in an ice bath, and potassium chlorate as an oxidation agent was slowly added. After 7 days, the solution turned green. The prepared sample as the oxidized suspension was washed with hydrochloric acid and deionized water to remove impurities and neutralize the sample. Finally, the GO was dried at 60 °C in a vacuum oven.

### Preparation of the insoluble part of Persian gum

For this purpose, a colloidal suspension of Persian gum was prepared. After an overnight, the insoluble part is separated and another solution is prepared, and this process is repeated three times. Finally, the separated insoluble part was dried in an oven and its particle size was reduced by grinding and meshing<sup>20</sup>.

### Synthesis of Pg@GO adsorbent

To synthesis Pg@GO as a solid adsorbent, first, 0.5 g of Persian gum was dissolved in 50 mL deionized water for 2 h at 40 °C until a homogenous solution was achieved. Then, 0.5 g GO was added to the solution and stirred over the night. Next, the solution was dried at room temperature for two weeks. Finally, the prepared sample was used as a solid adsorbent for CO<sub>2</sub> adsorption. Figure 1 shows each step of synthesis of Pg@GO as a solid adsorbent.

### CO<sub>2</sub> adsorption setup

The laboratory-scale reactor depicted in Fig. 2 was utilized for the CO<sub>2</sub> adsorption process and consisted of four main parts: gas injection, a reactor system, an instrument for controlling CO<sub>2</sub> pressure variations during the adsorption process, and a thermocouple for monitoring test heat. During the adsorption process, CO<sub>2</sub> gas flowed from a high-purity capsule into the chamber, with different weights of solid adsorbent used in each run. As the adsorption process commenced, the chamber's pressure decreased due to CO<sub>2</sub> adsorption, as the volume of both the chamber and reactor remained constant. The amount of CO<sub>2</sub> adsorbed was calculated based on the pressure reduction. In another word, when unadulterated CO<sub>2</sub> was implanted into the system, the adsorption operation was as takes after. The CO<sub>2</sub> gas stream was traded from the capsule to the chamber containing the specified adsorbent inside the reactor. At that point, the adsorption started, and CO<sub>2</sub> was ingested by the adsorbent. Due to the steady volume of the reactor and the chamber, the CO<sub>2</sub> adsorption decreased weight inside the chamber, and concurring to the entirety of weight diminish utilizing conditions related to adsorption, the amount of CO<sub>2</sub> adsorption (%) and the value of CO<sub>2</sub> adsorbed were measured by Eqs. (1) and (2):

$$\text{Adsorption}(\%) = \left( \frac{P_i - P_f}{P_i} \right) \times 100 \quad (1)$$

$$n_{\text{CO}_2} = \frac{(P_i - P_f)V}{RTZ} \quad (2)$$

where  $p_i$  is initial pressure,  $p_f$  is final pressure.  $w$  is the weight of the adsorbent. In addition, the adsorption capacity of adsorbent was measured by Eq. (3)<sup>22</sup>:

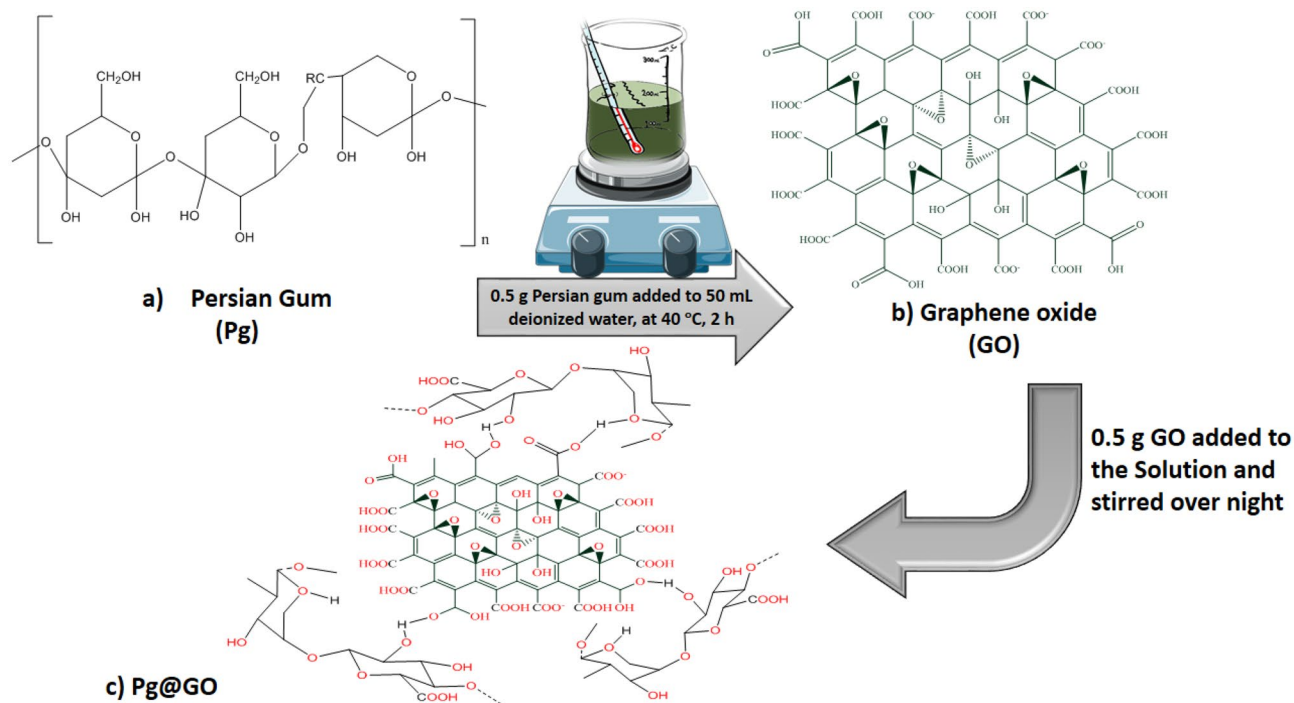


Figure 1. The steps of the synthesis of Pg@GO as a solid adsorbent.

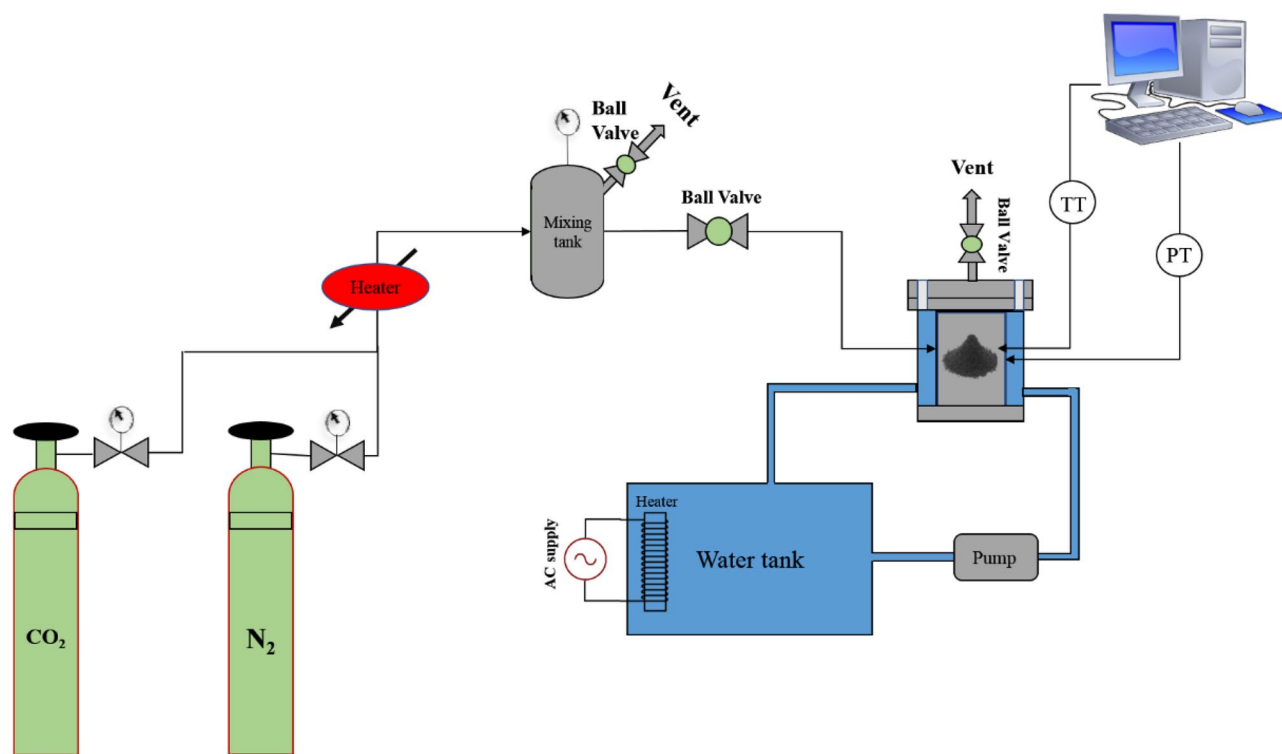


Figure 2. CO<sub>2</sub> adsorption setup.

$$q_e = \left( (p_i - p_f) V M_{\text{CO}_2} / RTZ \right) \times 10^3 \quad (3)$$

where  $V$  is the reactor volume,  $M_{\text{CO}_2}$  is 44 g/mol, and  $R$  is the gas constant.

### Characterization of adsorbent

The synthesis of Pg@GO was studied by various analysis methods to check structure, morphology, and composition. The structures and surface features of solid the adsorbent was examined using Scanning Electron Microscopy (SEM, Philips XL30 ESEM). X-ray power diffraction (XRD, Philips PW1730) was used to analyze the characteristics and recognition of a crystalline catalyst. The XRD result was recorded for a period of 2 h, covering a range of 5–70° with an increment of 0.05° and a duration of 1 s per step. The Brunauer–Emmett–Teller (BJH, BELSORP MINI II, and BEL) was utilized to identify the shapes and surface areas of non-porous adsorbents and a mesoporous solid with varying pore sizes. It means that the results of BET analysis assist in understanding adsorbent is macroporous (> 50 nm) or mesoporous (2–50 nm) or microporous (< 2 nm)<sup>23</sup>. The Fourier Transform Infrared spectroscopy (FTIR, Thermo, Avatar) provided information on the molecular vibrations of the catalysts within the 400–4000 cm<sup>-1</sup> range. Data on the thermal stability of Pg@GO was obtained using Thermo gravimetric analysis (TGA, TA, Q600, USA) by measuring the change in weight of the adsorbent as it is heated at a constant rate.

### Experimental design

To improve the process of CO<sub>2</sub> adsorption by Pg@GO, the response surface methodology (RSM) based on the Box–Behnken design (BBD) was utilized. RSM-BBD as an experimental design statistical tool was applied to specific interactions between two independent parameters and optimized response of multiple parameter processes. Alhajabdalla et al.<sup>24</sup> reported the main benefit of RSM-BBD. RSM-BBD ability is to analyze independent variables by performing few experimental runs than other RSM methods<sup>25</sup>. The study focused on three independent factors: pressure, time, and adsorbent weight. The dependent factor is CO<sub>2</sub> adsorption capacity. Table 1 provides the design and range levels for each parameter. To determine the absolute errors, seventeen experiments with six duplicate runs were conducted at central points, including 16 factorial points, six central, and eight axial<sup>26</sup>. The results of these experiments are presented in Table 2.

$$q_{\text{CO}_2} = \alpha_0 + \sum_{i=1}^k \alpha_{ii}X_i + \sum_{i=1}^k \alpha_{ii}X_i^2 + \sum_{i=1}^2 \sum_{j=1+1}^3 \alpha_{ij}X_iX_j + \varepsilon \quad (4)$$

Factors	Units	symbol	Levels		
			-1	0	+1
Adsorbent weight	g	A	0.1	0.3	0.5
Pressure	bar	B	1	4.5	8
Temperature	°C	C	25	40	55

**Table 1.** Experimental design levels of factors according to BBD.

Run	A: adsorbent weight	B: pressure	C: temperature	Adsorption capacity
	g	P	°C	mmol/g
1	0.5	4.5	55	3.49
2	0.1	1.0	40	1.95
3	0.5	4.5	25	4.30
4	0.3	1.0	25	2.81
5	0.3	4.5	40	3.07
6	0.5	8.0	40	4.74
7	0.3	1.0	55	1.76
8	0.3	4.5	40	3.00
9	0.1	4.5	25	3.61
10	0.3	8.0	55	3.04
11	0.1	8.0	40	3.43
12	0.3	4.5	40	3.02
13	0.3	8.0	25	4.68
14	0.3	4.5	40	3.06
15	0.1	4.5	55	1.60
16	0.5	1.0	40	3.12
17	0.3	4.5	40	3.04

**Table 2.** Experimental results for CO<sub>2</sub> adsorption capacity obtained from BBD.

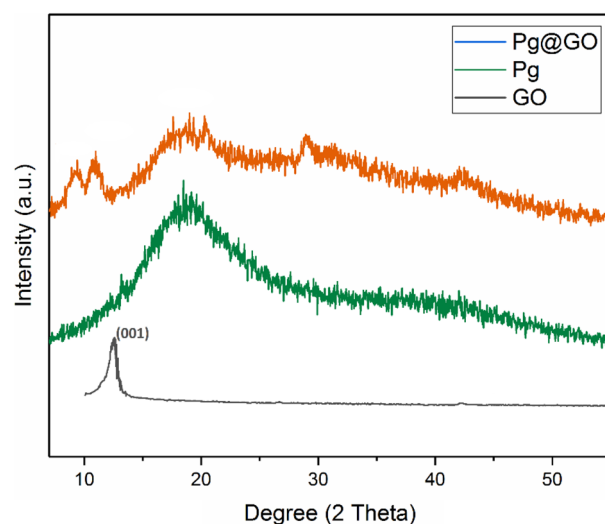
The value of  $q_{CO_2}$ , which represents the  $CO_2$  adsorbent capacity, is determined by the coefficients  $\alpha_0$ ,  $\alpha_i$ ,  $\alpha_{ii}$ , and  $\alpha_{ij}$  calculated through regression programming. These coefficients represent the constant, linear, quadratic, and interaction factors.  $X_i$  and  $X_j$  are independent variables, while  $\epsilon$  represents error<sup>27,28</sup>.

## Result and discussion

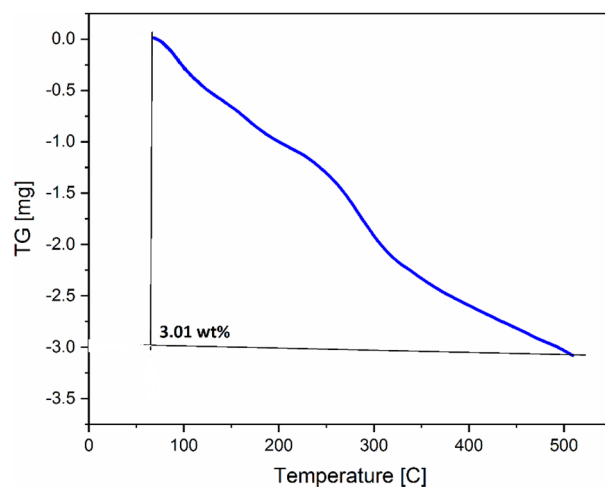
### Structure properties of Pg@GO

The crystal structure of raw Persian gum (Pg), GO and Pg@GO was studied by XRD analysis and the results are shown in Fig. 3. Persian gum has broad diffraction peaks at 20–42° which shows semi-crystal micro-structure of Pg@GO<sup>29</sup>. Bashir and Haripriya reported that lacking of sharp peaks in the XRD pattern of Pg showed its amorphous character<sup>29</sup>. The diffraction peak at GO appeared 2 $\theta$  of 10.01°, a crystal plane with a d-value of 8.75 Å correspond to the typical diffraction peaks of GO sheets<sup>30</sup>. The XRD pattern of Pg@GO has main peaks at 9.22°, 10.20°, and 20° related to the crystalline structure of GO and Pg. The accessibility of these peaks shows that the synthesis of Pg@GO was successful, however, the intensity of GO peak at 9.22° decreases. The thermal stability of Pg@GO was determined by TGA analysis and showed three stages of the weight loss (Fig. 4). The first step at < 100 °C related to the loss of adsorbent water and moisture. It was increasing temperature from 100 to 360 °C related to the thermal decomposition of oxygen-containing groups in GO and Persian gum to  $CO_2$ , CO, and  $H_2O$ <sup>31,32</sup>. The third stage occurs at 360 to 1000 °C because of oxidative pyrolysis of the carbon frame work of GO after the elimination of the oxygen-containing groups<sup>33</sup>.

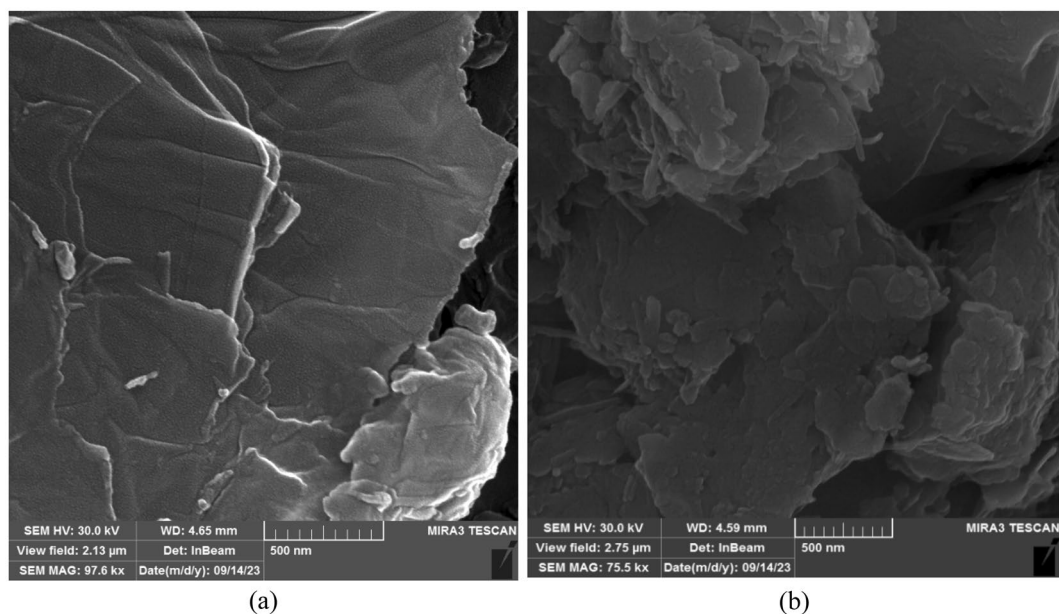
The morphology structure of raw GO and Pg@GO was studied by FESEM analysis, and the result is shown in Fig. 5. The flat morphology of GO is shown in Fig. 5a, and it has oxygen functional groups that cause the surface of GO seem smooth and wrinkled<sup>34</sup>. GO's thin layers structure displays that GO has a folded and rippled



**Figure 3.** XRD patterns for raw GO, raw Persian gum, Pg@GO.



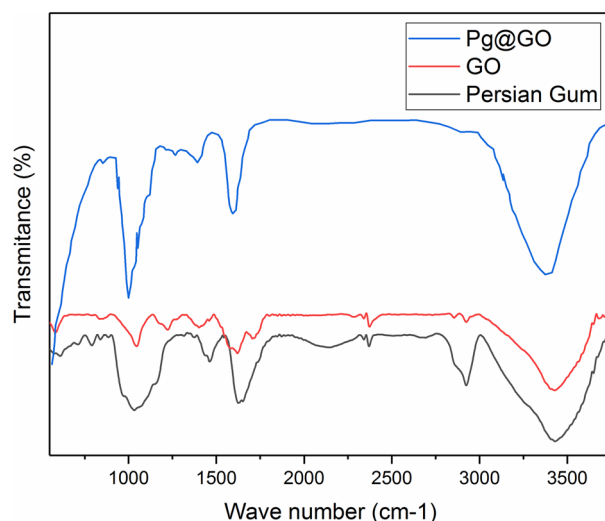
**Figure 4.** TGA analysis for Pg@GO as a solid adsorbent.



**Figure 5.** FESEM images for (a) raw GO, (b) Pg@GO.

wavy shape. The oxidation process causes the edges of the exfoliated GO to crumple<sup>35</sup>. The unique structure of GO induced its porous location on the sheet or between sheets<sup>36</sup>. Based on Fig. 5b, after the immobilization of Persian gum on GO, the surface of GO creates a surface remarkably rougher<sup>37</sup>. Also, as Pg has a soft, and free pores structure<sup>38</sup>, Pg@GO has low amount of pores in its structure.

The functional groups of raw GO, Persian gum, and Pg@GO as adsorbent were determined by FTIR analysis, and its results are shown in Fig. 6. The board peaks at  $3200\text{--}3400\text{ cm}^{-1}$  which can be related to  $\text{--OH}$  stretching vibration. The characteristic peaks at  $1035\text{ cm}^{-1}$  and  $1167\text{ cm}^{-1}$  are related to either epoxy or alkoxy (C–O), and stretching vibration of C–O, respectively. The peak at  $1415\text{ cm}^{-1}$  relates to the carboxy (C–O). The peak at  $1720$  is related to the carboxylic acid (C=O)<sup>39</sup>. The FTIR spectra of raw Persian gum have a board peaks at  $3300\text{--}3400\text{ cm}^{-1}$  showed  $\text{--OH}$  stretching vibration. The main peaks at  $2927$ ,  $2926$ , and  $2924\text{ cm}^{-1}$  are related to the asymmetric  $\text{--CH}_2\text{--}$  functional group. The peak at  $2855\text{ cm}^{-1}$  corresponds to the symmetric stretching vibrations of the  $\text{--CH}_2\text{--}$  functional group. The peaks at  $1601$  and  $1602\text{ cm}^{-1}$  are assigned to the asymmetrical stretching of carboxylate groups or the intramolecularly bound water. The amid I in protein has peaks at  $1600$  and  $1700\text{ cm}^{-1}$ . The stretching vibration of alcoholic groups creates peaks at  $1023$  and  $1024\text{ cm}^{-1}$ . The carbohydrate fingerprint has peaks at  $1500$  and  $500\text{ cm}^{-1}$ <sup>40,41</sup>. The FTIR spectra of Pg@GO has characteristic bands of Persian gum on the solid adsorbent which show the presence of Persian gum species without any ruin after loading on GO.



**Figure 6.** FTIR spectrum for raw GO, pure Persian gum, and GO@Pg.

However, the characteristic bands of Pg@GO are displacement and become visible very weaker comparing the FTIR spectra of the raw Persian gum.

### Adsorbent mechanism

The results showed that in low temperatures, the adsorption of CO<sub>2</sub> on Pg@GO was physisorption. Both GO and Persian gum have hexagonal structures with hydroxyl, epoxy, and carbonyl groups<sup>42,43</sup>. The interaction between CO<sub>2</sub> molecules and the delocalized π-aromatic system of GO are seen because of the presence of oxygen groups in the interlayers. Based on the different reports, the high amount of oxygen groups on Pg@GO has a positive effect on CO<sub>2</sub> adsorption. As both Persian gum and GO have oxygen functional groups on their chemical structures, CO<sub>2</sub> adsorption capacity was performed with increasing pressures<sup>9,11,44</sup>. Figure 7 shows the suggested mechanism for CO<sub>2</sub> adsorption via Pg@GO.

### Adsorption modeling

#### Isotherm modeling

Adsorption isotherm is used for understating how CO<sub>2</sub> molecules as adsorbed interact with the active sites of adsorbent in a variation of gas pressures at constant temperature<sup>45,46</sup>. This interaction usually is determined by adsorption isotherm models including Langmuir, Freundlich, Dubinin–Radushkevich (D–R), Sips, and Temkin. Equation (5) shows Langmuir isotherm model. Based on Langmuir model as a simple and empirical model, the rate of adsorption and desorption of CO<sub>2</sub> molecules on solid surface is equal. The adsorption process happens in limited specific sites and adsorb only one molecule<sup>47</sup>.

$$q_e = \frac{q_m K_L P_{CO_2}}{1 + K_L P_{CO_2}} \quad (5)$$

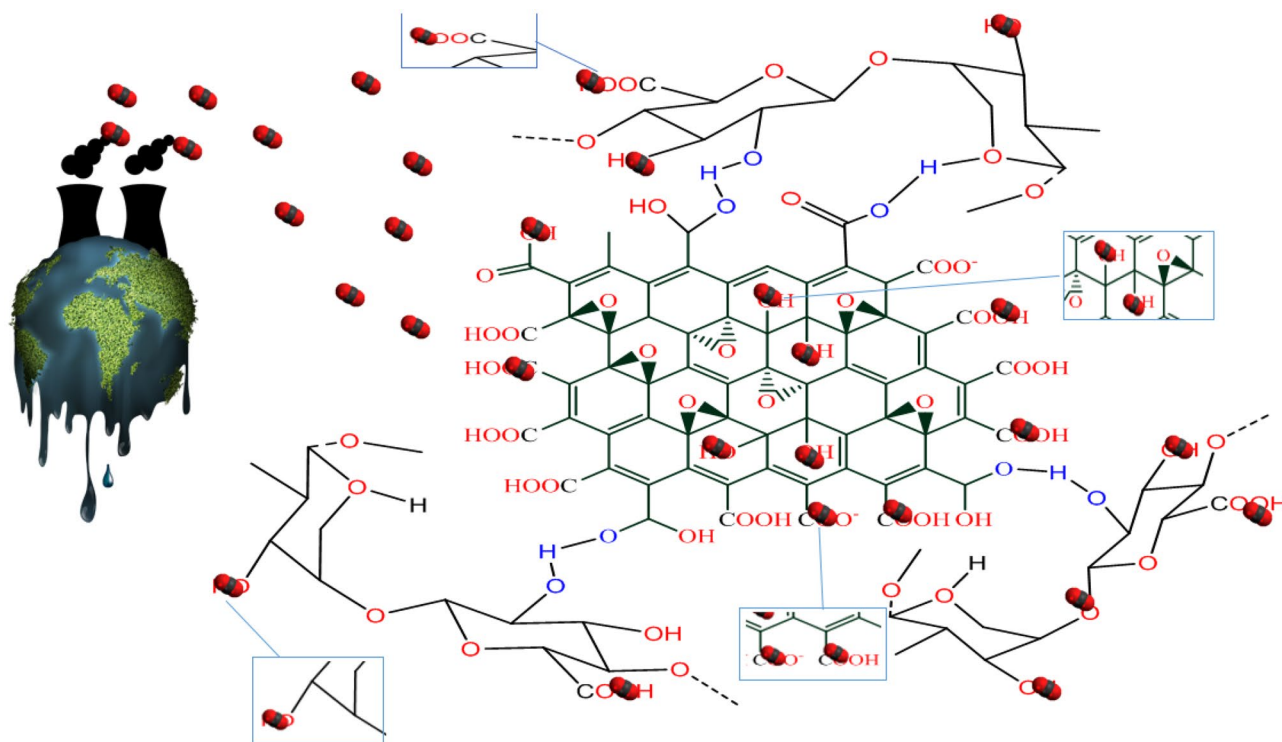
where  $q_e$  is the maximum adsorption capacity (mmol g<sup>-1</sup>),  $q_m$  is the amount of CO<sub>2</sub> adsorbed at equilibrium (mg g<sup>-1</sup>), and  $K_L$  is constant Langmuir (bar<sup>-1</sup>).  $P_{CO_2}$  is the equilibrium pressure of the gas. The Freundlich model is calculated based on Eq. (6). This model is used for inhomogeneous and homogenous surfaces. It can use for chemical and physical adsorption<sup>48</sup>.

$$q_e = K_F P^{1/n} \quad (6)$$

$K_f$  and  $n$  is the Freundlich constant (g bar mmol<sup>-1</sup>).

Dubinin–Radushkevich model (D–R) is applied for the recognition of either chemical or physical sorption<sup>48</sup>. D–R model is calculated by Eq. (7).

$$\ln q_e = \ln q_m - \beta \cdot \varepsilon^2 \quad (7)$$



**Figure 7.** Proposed mechanism for adsorption of CO<sub>2</sub> molecules using Pg@GO.

where  $q_m$  shows a single-layer adsorption capacity,  $\beta$  and  $\varepsilon$  are the constant related to the adsorption energy ( $\text{mol}^2 \text{KJ}^{-2}$ ). The sign of  $\varepsilon$  or the Polanyi potential ( $\text{KJ}^2 \text{mol}^{-2}$ ) is calculated by Eq. (8):

$$\varepsilon = RT \ln \left[ 1 + \frac{1}{P_{\text{CO}_2}} \right] \quad (8)$$

where  $R$  is gas constant ( $\text{J mol}^{-1} \text{K}^{-1}$ ), and  $T$  is the absolute temperature (k). Temkin isotherm model is determined by Eq. (9). According to the Temkin isotherm assumption, the adsorption heat related to the adsorption process correlated to all adsorbent molecules and reduced linearly rather than logarithmic with coverage<sup>49</sup>.

$$q_e = B \ln(K_T p) \quad (9)$$

In this equation,  $B$ , and  $K_T$  ( $\text{atm}^{-1}$ ) are Temkin constant. By mixing Langmuir and Freundlich isotherm models, the Sips model is obtained, while the main difference between Sips and Langmuir models is  $n_s$ . The  $n_s$  is the heterogeneity parameter. Usually, it is lower than 1 which shows more heterogeneity of the surface of adsorbents. If  $n_s$  is equal to 1, the adsorbent surface is homogenous, and the Sips model reduces to Langmuir model<sup>50</sup>. Sips isotherm model is determined by Eq. (10).

$$\begin{aligned} b_s &= b_0 \cdot \exp\left(\frac{Q}{R \cdot T_0}\right) \cdot \left(\frac{T_0}{T} - 1\right); n_s = n_0 + \alpha \left(1 - \frac{T_0}{T}\right); \\ q_{ms} &= q_{m0} \cdot \exp\left(\chi \left(1 - \frac{T}{T_0}\right)\right) \end{aligned} \quad (10)$$

where  $b_0$  is adsorption affinity,  $n_0$  is heterogeneity coefficient,  $q_{m0}$  describes maximum adsorption capacity,  $R$  and  $T_0$  are gas constant and reference temperature which assumed 298 K, respectively. Two signs including  $\chi$  and  $\alpha$  are Sips constants.

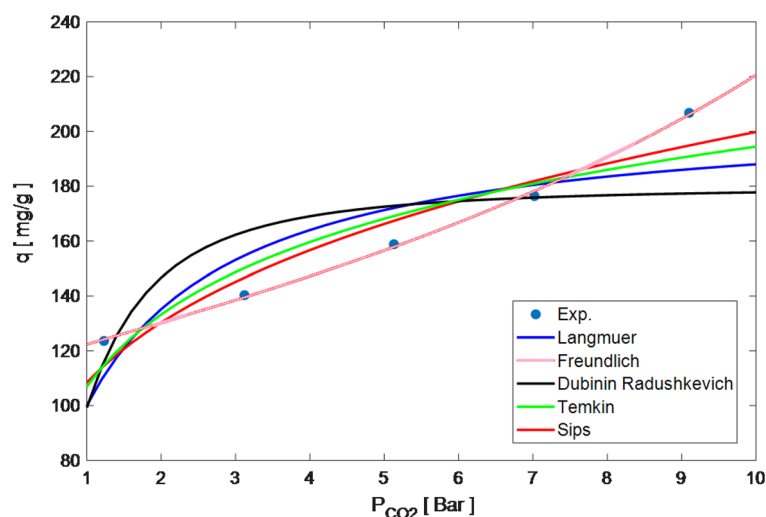
Figure 8, and Table 3 display the  $\text{CO}_2$  adsorption isotherm models. The isotherm experiments were performed at constant temperature of 298 K and at pressure in range of 1–9 bar. For each isotherm model, the high value of  $R^2$  proves which isotherm model is well fitted to experimental data. According to Table 3, the Sips model has a high value of  $R^2$  and has the highest accuracy. This means that  $\text{CO}_2$  adsorption process was carried out heterogeneous and multi-layered on Pg@GO.

#### Kinetic modeling

Both the adsorption rate and mechanism are calculated by adsorption kinetic<sup>51,52</sup>. In this study, four nonlinear kinetic models are used and they are listed in Table 4. The adsorption rate based on adsorption capacity is known as a first-order equation. This phenomenon is seen when the adsorption process happens in different layer by diffusion<sup>53</sup>.

$$q_t = q_e(1 - \exp(-k_1 \cdot t)) \quad (11)$$

where  $q_t$ ,  $q_e$  and  $K_1$  are adsorption capacity at time ( $\text{mg g}^{-1}$ ), equilibrium condition ( $\text{mg g}^{-1}$ ), and first order rate constant ( $\text{min}^{-1}$ ), respectively. Another kinetic model is a second-order kinetic model that is based on solid-phase adsorption. It shows that the rate of chemical adsorption is slow and it can control adsorption process<sup>51,54</sup>. Equation (12) is used for determining second-order kinetic model.



**Figure 8.** Isotherm modelling of  $\text{CO}_2$  adsorption on Pg@GO at 298 K.



Isotherm models	Parameters	Value
Langmuir	$q_m$ (mg/g)	208.346
	$k_l$	0.925
	$R^2$	0.876
Freundlich	$K$	108.469
	$n$	3.769
	$R^2$	0.955
Dubinin Radushkevich	$q_b$	179.775
	$\beta$	0.208
	$E_a$	1.550
	$R^2$	0.777
Temkin	$A$	16.684
	$B$	38.006
	$R^2$	0.931
Sips	$K_s$	-1513.319
	$\beta$	-0.813
	$a_s$	-13.36731
	$R^2$	0.999

**Table 3.** Parameters of isotherm models for CO<sub>2</sub> adsorption process at 25 °C.

Kinetic models	Parameters	25 °C	35 °C	45 °C	55 °C	65 °C
First order	$q_e$ (mg/g)	173.631	173.809	154.185	113.893	116.918
	$k_l$	0.01320	0.01073	0.02253	0.00433	0.00237
	$R^2$	0.859	0.839	0.941	0.838	0.927
Second order	$q_e$ (mg/g)	181.761	183.098	158.318	121.407	127.652
	$k_l$	0.00010	0.00008	0.00025	0.00006	0.00003
	$R^2$	0.931	0.921	0.972	0.909	0.963
Ritchie second order	$q_e$ (mg/g)	181.761	183.098	158.418	121.407	127.652
	$k_l$	0.01870	0.01490	0.03944	0.0067	0.0034
	$R^2$	0.931	0.921	0.972	0.909	0.963
Elovich	$\alpha$	1.991	0.490	5210.568	0.034	0.006
	$\beta$	15.753	17.773	8.467	15.670	19.628
	$R^2$	0.961	0.967	0.959	0.959	0.986

**Table 4.** Kinetic parameters of CO<sub>2</sub> adsorption on Pg@GO at different temperature.

$$q_t = K_2 \cdot q_e^2 \frac{t}{(1 + K_2 \cdot q_e \cdot t)} \quad (12)$$

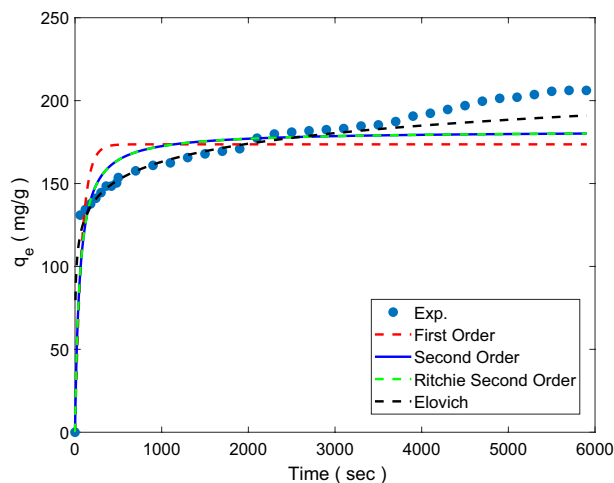
where  $K_2$  is second order rate constant ( $\text{min}^{-1}$ ), and  $t$  is adsorption time (min). The theory of Ritchie's second-order equation (Eq. 13) is that each adsorption process is performed on two surface sites<sup>47</sup>.

$$q_t = q_e - \frac{q_e}{(1 + K_2 t)} \quad (13)$$

The Elovich model is suggested for chemical adsorption process<sup>55</sup>.

$$q_t = \beta \cdot \log(\alpha \cdot \beta) + \beta \cdot \log(t) \quad (14)$$

$\alpha$  and  $\beta$  are the initial adsorption rate ( $\text{mg g}^{-1} \text{min}^{-1}$ ), and the value dependent on the activation energy and amount of surface coverage ( $\text{g mg}^{-1}$ ), respectively. Parameters related to the different kinetic models that are used in this study for Pg@GO are listed in Table 4. Figure 9 shows CO<sub>2</sub> adsorption capacity (mg/g) against time (sec). Based on Fig. 9, the highest value of  $R^2$  is related to the Elovich model which shows this model is best fitted to the empirical data, and then the second-order model has a high value of  $R^2$ . Elovich's model proves that the CO<sub>2</sub> capture process is not constant during the adsorption process and Pg@GO has a uniform surface because surface coverage increased hence adsorption rate decreased, and the uniform surface area of the adsorbent causes the active sites for CO<sub>2</sub> adsorption are not constant.



**Figure 9.** Kinetic modelling of CO<sub>2</sub> adsorption on Pg@GO at different pressures.

#### Thermodynamic modeling

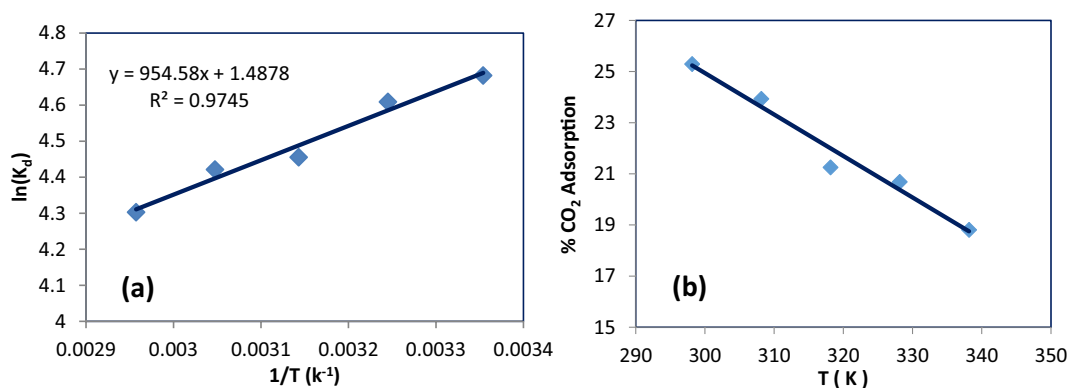
The properties of the CO<sub>2</sub> adsorption mechanism were investigated by thermodynamic factors of enthalpy change ( $\Delta H^\circ$ ), change in entropy ( $\Delta S^\circ$ ), and Gibbs free energy in change ( $\Delta G^\circ$ ) in physical and chemical adsorption. The parameters and magnitude are very important. In other words, the negative value of  $\Delta H^\circ$  shows an exothermic reaction, in contrast, the positive value  $\Delta H^\circ$  illustrates an endothermic reaction. In addition, if  $\Delta H^\circ$  is lower than 20 kJ/mol, absolute physisorption will happen in the process, while if  $\Delta H^\circ$  is more than 40 kJ/mol chemical adsorption will accrue<sup>4,56</sup>. The value of randomness of adsorption capture in the organization at the interface of gas/solid is determined by the positive and the negative signs of  $\Delta S^\circ$ . On one hand, when  $\Delta S^\circ$  is more than zero ( $\Delta S^\circ > 0$ ), the process is more random. On the other hand, if  $\Delta S^\circ$  is lower than zero ( $\Delta S^\circ < 0$ ), the process is less random. Moreover, the spontaneity of the process determines with signs of the Gibbs free energy change<sup>57</sup>. If the  $\Delta G^\circ$  is more than zero ( $\Delta G^\circ > 0$ ), the process is not happen and is nonspontaneous, conversely, the negative value of  $\Delta G^\circ$  ( $\Delta G^\circ < 0$ ), the process is possible and spontaneous, according to Fig. 10a, CO<sub>2</sub> adsorption process via Pg@GO was possible and spontaneity<sup>58,59</sup>. The following equations assist thermodynamic factors to be calculated. The thermal adsorption enthalpy is calculated by Van't Hoff equation (Eq. 17), which was obtained by Eqs. (15) and (16).  $K_d$  as the distribution coefficient calculated by Eq. (18).

$$\Delta G^0 = \Delta H^0 - T\Delta S \quad (15)$$

$$\Delta G^0 = -RT \ln K_d \quad (16)$$

$$\ln K_d = \frac{\Delta S^0}{R} - \frac{\Delta H^0}{RT} \quad (17)$$

$$K_d = (P_i - P_e) \times (V/W) \quad (18)$$



**Figure 10.** CO<sub>2</sub> captures (a) Van't Hoff plot. (b) In different temperatures.

where T and R are absolute temperature and the value of gas constant ( $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ ), respectively. When  $\ln K_d$  against  $1/T$  was plotted the values of  $\Delta H^\circ$  (slop) and  $\Delta S^\circ$  (intercept) were calculated. However, the value of  $\Delta G^\circ$  is measured by Eq. (12).  $K_d$  is the distribution coefficient value calculated by Eq. (15).  $P_i$  (bar) is the initial pressure,  $P_e$  (bar) is the reduced pressure,  $V$  ( $\text{cm}^3$ ), and  $W$  (g) are, the volume, and weight of the adsorbent, respectively.

Based on Fig. 10b, and Table 5, temperature has a significant effect on  $\text{CO}_2$  adsorption. When temperature increases,  $\text{CO}_2$  adsorption decreases. Rashidi et al.<sup>60</sup> reported that since the type of bonds between  $\text{CO}_2$  molecules and solid adsorbents were van der Waals as weak bonds, increasing temperature cause these bonds destroyed. As solid adsorbent faced High  $\text{CO}_2$  molecules penetration, large surface adsorption energy, and instability of adsorption  $\text{CO}_2$  molecules to the solid adsorbent surface, the desorption process by Le Chatelier's principle is an endothermic type and suitable.

### RSM statistical analysis

RSM-BBD was used to optimize the  $\text{CO}_2$  adsorption process on Pg@GO. Based on the BBD, the experimental design was used to extend an RSM by the Quadratic model. Three independent factors such as Adsorbent weight (A), Pressure (B), and Temperature (C), was used in the RSM model while the adsorbent capacity (Y) was used as response. The quadratic equation on the design model was shown in Eq. (19). On the below equation negative coefficient will decline the  $\text{CO}_2$  adsorption capacity, while the positive equation will increase the  $\text{CO}_2$  adsorption capacity.

$$q_{\text{CO}_2} = 3.04 + 0.63A + 0.78B - 0.69C + 0.30AC - 0.15BC + 0.22A^2 + 0.047B^2 \quad (19)$$

To specify the coefficients of the quadratic of the empirical results, Analysis Of Variance (ANOVA) was applied. The coefficient of determination ( $R^2$ ) was used to calculate the accuracy of the suggested model, and then F-test was applied to check statistical significance<sup>61,62</sup>. According to Table 6, the quadratic model has an F-value equal to 1404.32 low error probability value ( $(\text{Prob} > F) < 0.0001$ ) displayed that the mathematical models can be statistically illustrating the achieved experimental results. The F-value is obtained by dividing two mean squares, which allows for the assessment of the ratio between explained variance and unexplained variance. The calculation of the  $p$ -value is dependent on the sampling distribution of the test statistic assuming the null hypothesis, the data collected from the sample, and the specific type of test conducted (lower-tailed, upper-tailed, or two-sided)<sup>63</sup>.

Since the  $R^2$  value was 0.9994, therefore, experimental results have good agreement with the model. The significance of each factor was introduced by  $p$ -value and F-test. The smaller  $p$ -value and larger F-test show the significant effects of independent factors<sup>64</sup>. It was clear that the order of priority among those factors on the

P( $\text{CO}_2$ ) Bar	$\Delta H$ (kJ/mol)	$\Delta S$ (kJ/mole K)	$\Delta G$ (kJ/mol)				
			25	35	45	55	65
6.000	-11.441	-0.011	-8.169	-8.059	-7.949	-7.83949	-7.730

**Table 5.** Thermodynamic variables for  $\text{CO}_2$  adsorption on Pg@GO adsorbent.

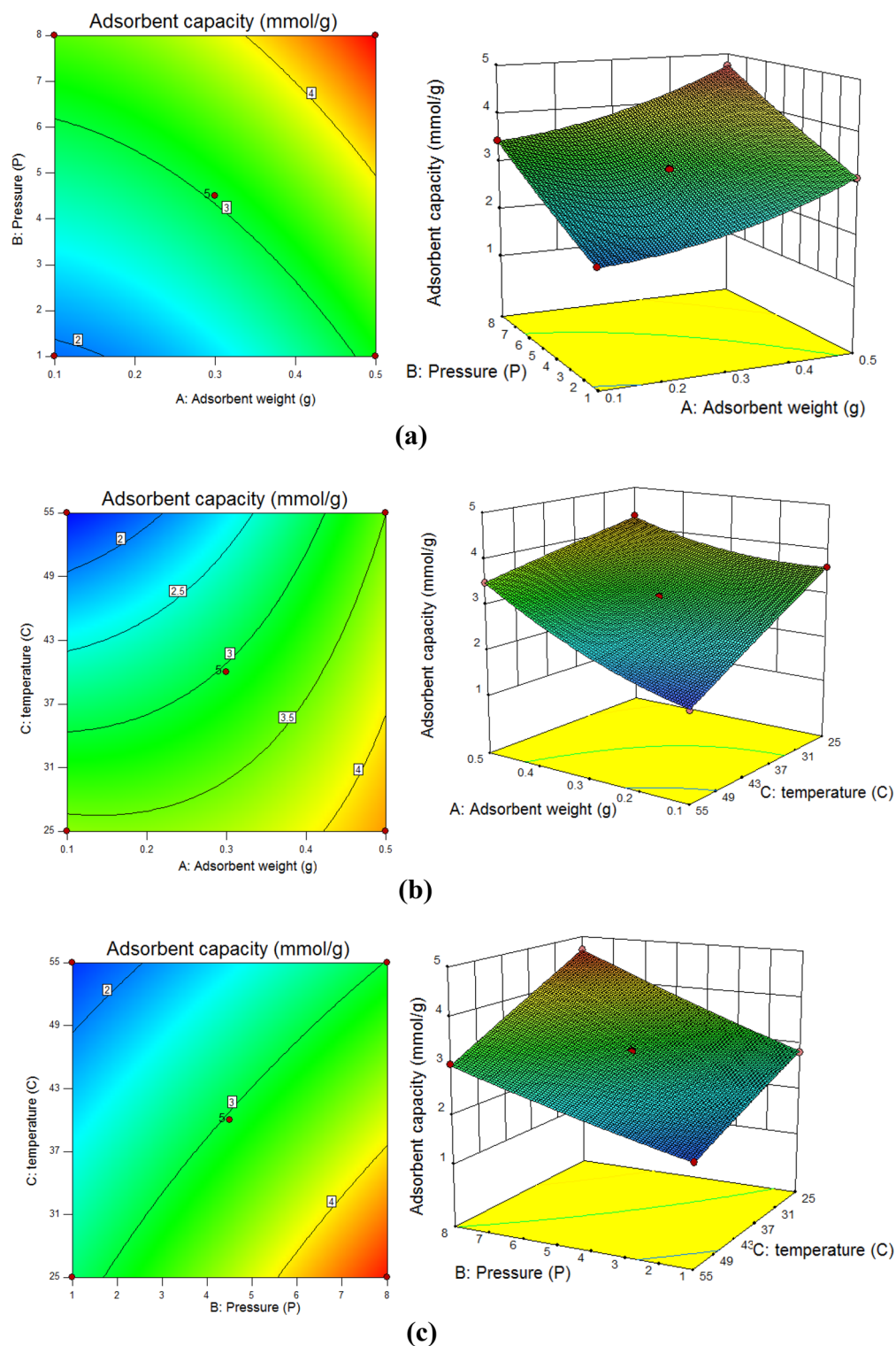
Source	Some of Squares	Df	Mean square	F value	$p$ -Value Prob > F	
Model	12.56	9	1.40	1404.32	<0.0001	Significant
A-Adsorbent weight	3.20	1	3.20	3221.16	<0.0001	Significant
B-Pressure	4.88	1	4.88	4914.41	<0.0001	Significant
C-temperature	3.80	1	3.80	3819.57	<0.0001	Significant
AB	4.900E-003	1	4.900E-003	4.93	0.0618	Not-significant
AC	0.36	1	0.36	362.33	<0.0001	Significant
BC	0.087	1	0.087	87.59	<0.0001	Significant
A <sup>2</sup>	0.21	1	0.21	214.06	<0.0001	Significant
B <sup>2</sup>	9.400E-003	1	9.400E-003	9.46	0.0179	
C <sup>2</sup>	6.845E-004	1	6.845E-004	0.69	0.4339	
Residual	6.955E-003	7	9.936E-004			
Lack of Fit	3.675E-003	3	1.225E-003	1.49	0.3442	Not significant
Pure error	3.280E-003	4	8.200E-004			
Cor total	12.56	16				
R <sup>2</sup>	0.9994		Std. dev	0.032		
Pre-R <sup>2</sup>	0.9949		Mean	3.16		
Adj-R <sup>2</sup>	0.9987		C.V%	1.00		

**Table 6.** ANOVA for Response Surface Quadratic model. Where A, B and C are coded form of independent factors. Interaction terms are AC, BC, and AB, and squared terms of factors are described by A<sup>2</sup>, B<sup>2</sup> and C<sup>2</sup>.

CO<sub>2</sub> adsorption capacity is the quadratic terms of adsorbent weight ( $F = 3221.16$ ), pressure ( $F = 4914.41$ ), and temperature ( $3819.57$ ). The interaction effect between factors, however, has less impact on the adsorption process.

#### The effect of independent factors

Figure 11 shows the interaction between independent factors. Figure 11a shows the interaction between adsorbent weights (A) and pressure (B), while temperature (C) is considered constant. According to the results, by



**Figure 11.** The interaction between (a) adsorbent weight and pressure factors, (b) adsorbent weight and temperature factors, and (c) pressure and temperature factors.

increasing the adsorbent weight to 0.4 g and pressure to 7.88 bar, the CO<sub>2</sub> adsorption capacity was raised to 4.80 mmol/g. That is because the interaction between active sites of solid adsorbent and CO<sub>2</sub> molecules increased significantly. Therefore, the yield of CO<sub>2</sub> adsorption capacity improved<sup>65</sup>. The growing active sites decrease adequate space for CO<sub>2</sub> capture, therefore, both agglomeration and closure of pores are observed<sup>66</sup>. According to the mentioned reasons 0.4 g adsorbent weight was chosen.

Figure 11b illustrates the interaction between adsorbent weight (A) and temperature (C). It shows that, by increasing temperature and adsorbent weight to 27 C and 0.4 g, CO<sub>2</sub> adsorption capacity improved to 4.80 mmol/g. This phenomenon happened since CO<sub>2</sub> adsorption is exothermic in nature, by increasing temperature the interaction between active sites and gas molecules augments, because of this molecular interaction grows and accessible and effective active sites on the surface of adsorption decline<sup>67</sup>. The highest adsorption capacity observed at lowest temperature<sup>59</sup>. In this study optimum temperature selected was 27 °C.

Figure 11c displayed the interaction between temperature (C) and pressure (B). According to the experimental results, a rising pressure factor from 1 to 7.88 bar causes CO<sub>2</sub> capacity to improves to 4.80 mmol/g. Khajeh and Ghaemi<sup>68,69</sup> reported that molecular movement and rate of reaction increase in high pressure. They reported that the adsorbents with different pore sizes show various behavior. Consequently, the optimum pressure was chosen at 7.88 bar.

#### Model variation and condition optimization

The RSM-BBD as a numerical method was applied for optimization of operating conditions in the selected range factors by considering the standard error<sup>28</sup>. The precision between the purposed solutions and actual results was determined by the optimal solutions. The optimum conditions was obtained at adsorbent weight of 0.4 g, pressure of 7.88 bar, and temperature of 27 C. Under the optimum conditions, the highest CO<sub>2</sub> capture was 4.80 mmol/g.

#### Adsorbent regeneration

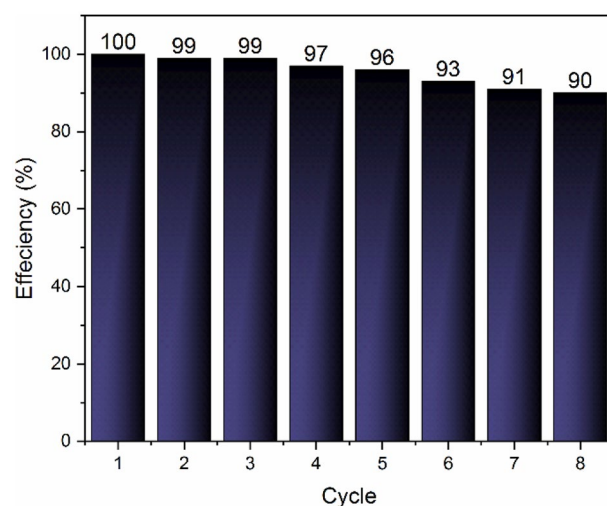
As an economical view, the regeneration of solid adsorbents is very important. The regeneration process is performed by three methods such as changing both of them resulting in a hybrid regeneration (VTSA/PTSA), changing the temperature (temperature swing; TSA), and changing the pressure (vacuum/pressure swing; VSA/PSA)<sup>70,71</sup>. In this study, the TSA method was used for regeneration of Pg@GO. At the end of each cycle, Pg@GO as a solid adsorbent was separated and regenerated in the oven at 40 °C for 10 h. As can be seen in Fig. 12, the adsorption capacity declined from 100 to 90% after 8 cycles. Because Pg@GO is economical and high-value adsorbent, it can be used in industrial gas adsorption applications.

#### Comparison of the absorbent results with other absorbents

Table 7 compares the adsorption capacity of Pg@GO used in this research with other research that used GO as an adsorbent for CO<sub>2</sub> capture. According to the results, it is clear that Pg@GO can adsorb CO<sub>2</sub> at 7.88 bar and 300 C with the maximum capacity of 4.80 mmol/g. As Pg@GO has many active sites, it can adsorb CO<sub>2</sub> molecules in the presence of low amount of solid adsorbent (0.4 g). At the end of the CO<sub>2</sub> adsorption process, Pg@GO recycled eight times without decreasing the adsorption capacity.

#### Conclusion

Carbon dioxide is one of the greenhouse gases that is produced via burning fossil fuels, and it has a negative impact on the environment. Pg@GO was synthesized as a solid adsorbent for CO<sub>2</sub> capture. The RSM-BBD method was used to optimize operation conditions. The maximum CO<sub>2</sub> adsorption capacity was 4.80 mmol/g at 0.40 g adsorbent weight, 300 K, and 7.88 bar. The Freundlich isotherm model has a good agreement with



**Figure 12.** Recycling performance of Pg@GO for CO<sub>2</sub> capture.

Solid adsorbents	P (bar)	T (°C)	CO <sub>2</sub> capacity (mmol/g)	References
KOH@GO-Fe <sub>3</sub> O <sub>4</sub>	9	298	6.812	11
GO-TiO <sub>2</sub> -Ag <sub>2</sub> O-Arg	10	273	1250	72
GO-TiO <sub>2</sub> -Ag <sub>2</sub> O	10	273	1185	72
polyethylenimine@GO	1	298	0.747	73
PEI-GO@ZIF-8	1	273	4.190	74
TiO <sub>2</sub> @GO	1	323	1.880	75
This study	7.88	300	4.800	–

**Table 7.** Comparison of operation condition and CO<sub>2</sub> adsorption capacity.

experimental data. Hence, the adsorption process is heterogeneous. According to kinetic model results, the Elovich model was able to describe CO<sub>2</sub> adsorption data because of the highest R<sup>2</sup> value and showed the interaction between CO<sub>2</sub> molecules and the adsorbent's surface is chemisorption. The negative value of  $\Delta G^\circ$  in the thermodynamic study proved that the process was exothermic and spontaneous. The regeneration of Pg@GO was tested in optimum conditions. The solid adsorbent was able to be reused eight times without a significant loss on the CO<sub>2</sub> adsorption capacity.

### Data availability

The data used and analyzed during the current study is available from the corresponding author on reasonable request.

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### References

- Feng, X. *et al.* MnyCo<sub>3</sub>-γO<sub>x</sub> bimetallic oxide prepared by ultrasonic technology for significantly improved catalytic performance in the reduction of NO<sub>x</sub> with NH<sub>3</sub>. *Fuel* **352**, 129159 (2023).
- Li, Z. *et al.* Ionic liquid hybrid metal-organic frameworks for efficient adsorption and selective separation of ammonia at high temperature. *Chem Eng J* **464**, 142728 (2023).
- Ghaemi, A. & Behroozi, A. H. Comparison of hydroxide-based adsorbents of Mg(OH)<sub>2</sub> and Ca(OH)<sub>2</sub> for CO<sub>2</sub> capture: Utilization of response surface methodology, kinetic, and isotherm modeling. *Greenh. Gases Sci. Technol.* **10**(5), 948–964 (2020).
- Pashaei, H., Ghaemi, A. & Nasiri, M. Modeling and experimental study on the solubility and mass transfer of CO<sub>2</sub> into aqueous DEA solution using a stirrer bubble column. *RSC Adv.* **6**(109), 108075–108092 (2016).
- Gao, S. *et al.* Ingenious artificial leaf based on covalent organic framework membranes for boosting CO<sub>2</sub> photoreduction. *J. Am. Chem. Soc.* **145**(17), 9520–9529 (2023).
- Liu, Y. *et al.* Ultrasound-assisted amine functionalized graphene oxide for enhanced CO<sub>2</sub> adsorption. *Fuel* **247**, 10–18 (2019).
- Chen, L. *et al.* Reinforced AZ91D magnesium alloy with thixomolding process facilitated dispersion of graphene nanoplatelets and enhanced interfacial interactions. *Mater. Sci. Eng. A* **804**, 140793 (2021).
- Biswas, K. Ultrasonication mediated Iron-doped reduced graphene oxide nano-sheets exhibiting unique physico-chemical properties and biomedical applications. *Mater. Chem. Phys.* **291**, 126687 (2022).
- Cai, J. *et al.* Molecular mechanisms of CO<sub>2</sub> adsorption in diamine-cross-linked graphene oxide. *Chem. Mater.* **31**(10), 3729–3735 (2019).
- Hermanová, S. *et al.* Graphene oxide immobilized enzymes show high thermal and solvent stability. *Nanoscale* **7**(13), 5852–5858 (2015).
- Helmi, M. *et al.* Synthesis and characterization of KOH@Graphene oxide-Fe<sub>3</sub>O<sub>4</sub> as a magnetic composite adsorbent for CO<sub>2</sub> capture. *J. Phys. Chem. Solids* **178**, 111338 (2023).
- Kagdada, H. L. *et al.* First principles study on small ZrAln and HfAln clusters: structural, stability, electronic states and CO<sub>2</sub> adsorption. *Mater. Chem. Phys.* **239**, 122264 (2020).
- Liu, X. *et al.* Metal-organic framework nanocrystals derived hollow porous materials: synthetic strategies and emerging applications. *The Innovation* **3**, 100281 (2022).
- Zhang, Y. *et al.* Application of MOFs and COFs for photocatalysis in CO<sub>2</sub> reduction, H<sub>2</sub> generation, and environmental treatment. *EnergyChem* **4**, 100078 (2022).
- Chandra, V. *et al.* Highly selective CO<sub>2</sub> capture on N-doped carbon produced by chemical activation of polypyrrole functionalized graphene sheets. *Chem. Commun.* **48**(5), 735–737 (2012).
- Politakos, N. *et al.* Graphene-based monolithic nanostructures for CO<sub>2</sub> capture. *Ind. Eng. Chem. Res.* **59**(18), 8612–8621 (2020).
- Song, Y. *et al.* Amino-functionalized graphene oxide blend with monoethanolamine for efficient carbon dioxide capture. *J. Alloys Compd.* **704**, 245–253 (2017).
- Verma, A. *et al.* Bio-based sustainable aerogels: New sensation in CO<sub>2</sub> capture. *Current Res. Green Sustain. Chem.* **3**, 100027 (2020).
- Cappa, C., Lucisano, M. & Mariotti, M. Influence of Psyllium, sugar beet fibre and water on gluten-free dough properties and bread quality. *Carbohydr. Polym.* **98**(2), 1657–1666 (2013).
- Farahani, Z. K. *et al.* Functional beverage based on alginate/insoluble fraction of Persian gum, WPI and PPC beads loaded with jujube extract: physicochemical, rheometry and sensory properties. *Int. J. Food Sci. Technol.* **57**(1), 499–505 (2022).
- Wang, G. *et al.* Facile synthesis and characterization of graphene nanosheets. *J. Phys. Chem. C* **112**(22), 8192–8195 (2008).
- Karbalaei Mohammad, N. *et al.* Experimental investigation and modeling of CO<sub>2</sub> adsorption using modified activated carbon. *Iran. J. Chem. Chem. Eng. (IJCCE)* **39**(1), 177–192 (2020).
- Mays, T. A new classification of pore sizes. *Studies in Surface Science and Catalysis, 2007.* 160 (Characterization of Porous Solids VII) 57–62.
- Alhajabdalla, M. *et al.* Application of response surface methodology and Box-Behnken design for the optimization of the stability of fibrous dispersion used in drilling and completion operations. *ACS Omega* **6**(4), 2513–2525 (2021).

25. Masoumi, H., Ghaemi, A. & Gannadzadeh Gilani, H. Synthesis of polystyrene-based hyper-cross-linked polymers for Cd(II) ions removal from aqueous solutions: Experimental and RSM modeling. *J. Hazard. Mater.* **416**, 125923 (2021).
26. Xie, H. *et al.* Study the parametric effect of pulling pattern on cherry tomato harvesting using RSM-BBD techniques. *Agriculture* <https://doi.org/10.3390/agriculture11090815> (2021).
27. Helmi, M., Sobati, M. A. & Hemmati, A. Biodiesel production from mastic oil via electrolytic transesterification: optimization using response surface methodology and engine test. *Environ. Sci. Pollut. Res.* **30**(47), 104100–104115 (2023).
28. Helmi, M., Tahvildari, K., & Hemmati, A. Parametric optimization of biodiesel synthesis from *Capparis spinosa* oil using NaOH/NaX as nanoheterogeneous catalyst by response surface methodology. *Braz. J. Chem. Eng.* **38**, 61–75 (2020).
29. Mir, M. & Haripriya, S. Assessment of physical and structural characteristics of almond gum. *Int. J. Biol. Macromol.* **93**, 476 (2016).
30. Deng, J.-H. *et al.* Simultaneous removal of Cd(II) and ionic dyes from aqueous solution using magnetic graphene oxide nanocomposite as an adsorbent. *Chem. Eng. J.* **226**, 189–200 (2013).
31. Gils, P. *et al.* Designing of new acrylic based macroporous superabsorbent polymer hydrogel and its suitability for drug delivery. *Int. J. Pharm. Pharm. Sci.* **1**, 43 (2009).
32. Li, Y. *et al.* 3-D magnetic graphene oxide-magnetite poly(vinyl alcohol) nanocomposite substrates for immobilizing enzyme. *Polymer* **149**, 13–22 (2018).
33. Farivar, F. *et al.* Thermogravimetric analysis (TGA) of graphene materials: Effect of particle size of graphene. *Graphene Oxide Graphite Therm. Parameters C* **7**(2), 41 (2021).
34. Nadarajan, A. *et al.* One-pot synthesis of covalently functionalized reduced graphene oxide–polyaniline nanocomposite for supercapacitor applications. *Clean Technol. Environ. Policy* **20**, 2025 (2018).
35. Ain, Q.-U., Farooq, M. U. & Jalees, M. I. Application of magnetic graphene oxide for water purification: Heavy metals removal and disinfection. *J. Water Process Eng.* **33**, 101044 (2020).
36. Ramos Ferrer, P. *et al.* Nanostructured porous graphene and its composites for energy storage applications. *Nano Converg.* **4**(1), 29 (2017).
37. Naikoo, G. A. *et al.* Chapter 20 Development of electrode materials for high-performance supercapacitors. In *Emerging Nanotechnologies for Renewable Energy* (eds Ahmed, W. *et al.*) 545–557 (Elsevier, 2021).
38. Ghasempour, Z., *et al.*, Characterization and optimization of persian gum/whey protein bionanocomposite films containing betanin nanoliposomes for food packaging utilization (2021).
39. Chaurasia, S. R., Dange, R. & Bhanage, B. M. Graphene oxide as a carbo-catalyst for the synthesis of tri-substituted 1,3,5-triazines using biguanides and alcohols. *Catal. Commun.* **137**, 105933 (2020).
40. Dabestani, M. *et al.* Persian gum: A comprehensive review on its physicochemical and functional properties. *Food Hydrocoll.* **78**, 92–99 (2018).
41. Rezaei, A., Nasirpour, A. & Tavanai, H. Fractionation and some physicochemical properties of almond gum (*Amygdalus communis* L.) exudates. *Food Hydrocoll.* **60**, 461–469 (2016).
42. Ahmadi-Dehnoei, A. & Ghasemirad, S. Introducing water-redispersible powderable acrylic adhesives using Persian gum. *Ind. Crops Prod.* **173**, 114083 (2021).
43. Helmi, M. *et al.* Phosphomolybdic acid/graphene oxide as novel green catalyst using for biodiesel production from waste cooking oil via electrolysis method: Optimization using with response surface methodology (RSM). *Fuel* **287**, 119528 (2020).
44. Zhao, Y. *et al.* Insight into the mechanism of CO<sub>2</sub> adsorption on Cu–BTC and its composites with graphite oxide or aminated graphite oxide. *Chem. Eng. J.* **239**, 399–407 (2014).
45. Khajeh, M. & Ghaemi, A. Exploiting response surface methodology for experimental modeling and optimization of CO<sub>2</sub> adsorption onto NaOH-modified nanoclay montmorillonite. *J. Environ. Chem. Eng.* **8**(2), 103663 (2020).
46. Najafi, P., Ramezanipour Penchah, H. & Ghaemi, A. Synthesis and characterization of Benzyl chloride-based hypercrosslinked polymers and its amine-modification as an adsorbent for CO<sub>2</sub> capture. *Environ. Technol. Innov.* **23**, 101746 (2021).
47. Fashi, F., Ghaemi, A. & Moradi, P. Piperazine-modified activated alumina as a novel promising candidate for CO<sub>2</sub> capture: Experimental and modeling. *Greenh. Gases Sci. Technol.* **9**(1), 37–51 (2019).
48. Al-Ghouti, M. A. & Da'ana, D. A. Guidelines for the use and interpretation of adsorption isotherm models: A review. *J. Hazard. Mater.* **393**, 122383 (2020).
49. Tiwari, D. *et al.* Dynamic CO<sub>2</sub> capture by carbon adsorbents: Kinetics, isotherm and thermodynamic studies. *Sep. Purif. Technol.* **181**, 107–122 (2017).
50. Serafin, J. *et al.* Management of surgical mask waste to activated carbons for CO<sub>2</sub> capture. *J. CO<sub>2</sub> Utilization* **59**, 101970 (2022).
51. Ho, Y. S. & McKay, G. A comparison of chemisorption kinetic models applied to pollutant removal on various sorbents. *Process Saf. Environ. Prot.* **76**(4), 332–340 (1998).
52. Zhao, G. *et al.* Sorption of heavy metal ions from aqueous solutions: A review. *Open Colloid Sci. J.* **4**(1), 19–31 (2010).
53. Ho, Y.-S. Isotherms for the sorption of lead onto peat: Comparison of linear and non-linear methods. *Pol. J. Environ. Stud.* **15**(1), 81 (2006).
54. Ritchie, A. G. Alternative to the Elovich equation for the kinetics of adsorption of gases on solids. *J. Chem. Soc. Faraday Trans. 1 Phys. Chem. Condens. Phases* **73**, 1650–1653 (1977).
55. Weber, W. J. Jr. & Morris, J. C. Kinetics of adsorption on carbon from solution. *J. Sanit. Eng. Div.* **89**(2), 31–59 (1963).
56. Pashaei, H. *et al.* Experimental investigation of the effect of nano heavy metal oxide particles in piperazine solution on CO<sub>2</sub> absorption using a stirrer bubble column. *Energy Fuels* **32**(2), 2037–2052 (2018).
57. Vafaeinia, M. *et al.* Oxygen and nitrogen enriched pectin-derived micro-meso porous carbon for CO<sub>2</sub> uptake. *RSC Adv.* **12**(1), 546–560 (2022).
58. Raganati, F. *et al.* Isotherms and thermodynamics of CO<sub>2</sub> adsorption on a novel carbon-magnetite composite sorbent. *Chem. Eng. Res. Design* **134**, 540–552 (2018).
59. Taheri, F. S. *et al.* High CO<sub>2</sub> adsorption on amine-functionalized improved mesoporous silica nanotube as an eco-friendly nanocomposite. *Energy Fuels* **33**(6), 5384–5397 (2019).
60. Rashidi, N. A., Yusup, S. & Borhan, A. Isotherm and thermodynamic analysis of carbon dioxide on activated carbon. *Procedia Eng.* **148**, 630–637 (2016).
61. Sulaiman, N. F. *et al.* In depth investigation of bi-functional, Cu/Zn/γ-Al<sub>2</sub>O<sub>3</sub> catalyst in biodiesel production from low-grade cooking oil: Optimization using response surface methodology. *Renew. Energy* **135**, 408–416 (2019).
62. Tan, Y. H. *et al.* Application of RSM and Taguchi methods for optimizing the transesterification of waste cooking oil catalyzed by solid ostrich and chicken-eggshell derived CaO. *Renew. Energy* **114**, 437–447 (2017).
63. *Introduction to mathematical statistics*. STAT 415 Course; Available from <https://online.stat.psu.edu/stat415/lesson/13/13.2>.
64. Tan, Y. H. *et al.* Biodiesel production from used cooking oil using green solid catalyst derived from calcined fusion waste chicken and fish bones. *Renew. Energy* **139**, 696–706 (2019).
65. Behroozi, A. H. *et al.* Electrolyte solution of MDEA–PZ–TMS for CO<sub>2</sub> absorption; response surface methodology and equilibrium modeling. *Environ. Technol. Innov.* **23**, 101619 (2021).
66. Taheri, F. S., Ghaemi, A. & Maleki, A. High efficiency and eco-friendly TEPA-functionalized adsorbent with enhanced porosity for CO<sub>2</sub> capture. *Energy Fuels* **33**(11), 11465–11476 (2019).
67. Mashhadimoslem, H. *et al.* Biomass derived hierarchical porous carbon for high-performance O<sub>2</sub>/N<sub>2</sub> adsorption; a new green self-activation approach. *RSC Adv.* **11**(57), 36125–36142 (2021).

68. Helmi, M. *et al.* Synthesis, characterization and performance evaluation of NaOH@ Chitosan-Fe<sub>3</sub>O<sub>4</sub> as an adsorbent for CO<sub>2</sub> capture. *Fuel* **338**, 127300 (2023).
69. Khajeh, M. & Ghaemi, A. Strontium hydroxide-modified nanoclay montmorillonite for CO<sub>2</sub> capture: response surface methodology and adsorption mechanism. *Int. J. Environ. Analyt. Chem.* **103**, 1–26 (2021).
70. Dhoke, C. *et al.* Review on reactor configurations for adsorption-based CO<sub>2</sub> capture. *Ind. Eng. Chem. Res.* **60**(10), 3779–3798 (2021).
71. Raganati, F., Miccio, F. & Ammendola, P. Adsorption of carbon dioxide for post-combustion capture: A review. *Energy Fuels* **35**(16), 12845–12868 (2021).
72. Nosrati, A. *et al.* Effective CO<sub>2</sub> capture and selective photocatalytic conversion into CH<sub>3</sub>OH by hierarchical nanostructured GO–TiO<sub>2</sub>–Ag<sub>2</sub>O and GO–TiO<sub>2</sub>–Ag<sub>2</sub>O–Arg. *ACS Omega* **8**(4), 3981–3991 (2023).
73. Shin, G.-J., Rhee, K. & Park, S.-J. Improvement of CO<sub>2</sub> capture by graphite oxide in presence of polyethylenimine. *Int. J. Hydrog. Energy* **41**(32), 14351–14359 (2016).
74. Huang, A. & Feng, B. Facile synthesis of PEI-GO@ZIF-8 hybrid material for CO<sub>2</sub> capture. *Int. J. Hydrog. Energy* **43**(4), 2224–2231 (2018).
75. Chowdhury, S., Parshetti, G. K. & Balasubramanian, R. Post-combustion CO<sub>2</sub> capture using mesoporous TiO<sub>2</sub>/graphene oxide nanocomposites. *Chem. Eng. J.* **263**, 374–384 (2015).

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### Competing interests

The authors declare no competing interests.

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