scientific reports

OPEN

Check for updates

Study on the energy evolution mechanism of coal and rock with impact tendency under different strain rates

Kun Zhang[⊠], Yichen Zhang, Sen Zhang, Jianxi Ren, Liang Zhang, Renjie Zhang & Yuanquan Cui

To explore the strain rate effect of deformation and failure of impact prone coal rock, uniaxial compression tests and triaxial compression tests with different strain rates were carried out. The mechanical properties and impact tendency of impact-prone coal rock were studied, and the energy evolution law and pre-peak energy self-promotion-inhibition mechanism of impact-prone coal rock were obtained. The results show that with the increase of strain rate, the peak strength of coal rock under uniaxial compression decreases gradually, and the peak strength of coal rock under triaxial compression increases first and then decreases, and the impact tendency of coal rock increases first and then decreases. The energy evolution of coal rock under uniaxial compression is mainly divided into four stages: initial energy damage, energy hardening, energy softening and failure. With the increase of strain rate, the total energy and elasticity at the peak point of coal rock under uniaxial compression decrease gradually, and the total energy, elastic energy and dissipation energy at the peak point under triaxial compression increase first and then decrease. The elastic energy promotion coefficient of impact-prone coal rock is much larger than the inhibition coefficient, and the increase of strain rate will promote the generation of elastic energy inside coal rock. The research results can provide reference for the prevention and early warning of dynamic disasters of coal and rock mass with impact tendency.

In recent years, with the further development of deep coal mining, the frequency and scale of rock burst disasters in coal mines have increased significantly. The internal structure of coal rock is highly complex, and the mechanical properties are affected by the external loading rate¹, which induces dynamic disasters such as rock burst. Especially for coal rock with burst tendency, it is necessary to pay attention to its mechanical characteristics and failure modes. Therefore, it is of great significance for coal mine safety mining and disaster prevention to explore the influence of different loading rates on rock burst tendency.

The mechanical properties of coal rock are not only affected by the external stress state, but also related to the loading rate. This is because the change of loading rate will change the mechanical properties of the material. Therefore, the mechanical effect of rock mass under different loading rates is an important research topic in rock engineering². Chong³ and Lajtal⁴ carried out indoor rock triaxial compression tests on rocks with strain rates of $10^{-4} \text{ s}^{-1} - 10^{-1} \text{ s}^{-1}$ and $3.5 \times 10^{-8} \text{ s}^{-1} - 2.5 \times 10^{-5} \text{ s}^{-1}$, respectively, indicating that the compressive strength of rocks is positively correlated with the loading rate. However, with the in-depth analysis of the mechanical properties of rock under different loading rates by many scholars, it is found that the relationship between loading rate and rock strength is not a single positive correlation, but there is a corresponding 'critical rate' (If the loading rate is less than the critical rate, the strength of the rock will gradually increase with the increase of the loading rate is greater than the critical rate, the strength of the rock gradually decreases with the increase of the loading rate b. Swan et al.⁵ revealed the effect of loading rate on the triaxial compression mechanical properties of saturated shale when the strain rate was in the range of $10^{-4} - 240 \text{ min}^{-1}$, and proposed the corresponding critical rate of 0.1 min⁻¹. In addition, Zhang et al.⁶ also analyzed that the peak strength and elastic modulus of limestone increased sharply in the range of $5 \times 10^{-3} - 5 \times 10^{-3} \text{ mm/s}$ and decreased in the range of $5 \times 10^{-3} - 5 \times 10^{-1} \text{ mm/s}$ through uniaxial compression test of limestone. The damage of rock under different

School of Architecture and Civil Engineering, Xi'an University of Science and Technology, Xi'an 710054, China. email: zhangkun0833@qq.com loading rates can be described not only by mechanical characteristics, but also by rock failure characteristics^{7–10}, acoustic emission monitoring^{11,12}, energy evolution characteristics^{13,14}. Because the evolution law of internal energy of rock will directly reflect the damage and failure of rock under the influence of loading rate, the influence of different loading rates on rock damage and failure can be explained from the perspective of rock energy evolution.

The damage of rock is an energy-driven unstable state. Analyzing the deformation and failure mechanism of rock from the perspective of energy can better understand the nature of its failure. Many scholars have carried out experimental and theoretical studies on the energy evolution mechanism of rock deformation and failure process^{15–17}, indicating that the change of loading conditions will affect the energy density inside the rock. According to the uniaxial compression test and triaxial compression test of rock, scholars have studied the rock energy characteristics at the pre-peak stage or a certain characteristic point (peak stress point, yield stress point) of rock^{18–20}, and used the rock energy release rate to reflect the damage degree of rock. Based on the theory of rock energy dissipation, Xie et al.²¹ defined the concepts of releasable strain energy and unit dissipated energy, and proposed the strength criterion of rock. Aiming at the problem of dynamic failure in rock engineering, scholars have studied the energy dissipation of rock under impact and dynamic load, and analyzed that the degree of fragmentation of rock^{22,23} is positively correlated with the energy absorption per unit volume. The reason of rock unloading failure in rock triaxial unloading test is that the elastic energy accumulated by rock before unloading is released in large quantities, which leads to crack propagation^{24,25}. Therefore, the failure of rock is related to the release of elastic energy. At the same time, according to the characteristics of nonlinear evolution of rock energy in the process of deformation and failure, Meng²⁶ analyzed the nonlinear energy evolution mechanism of rock under lithology and loading rate, while Wang et al.²⁷ analyzed the nonlinear energy evolution mechanism of limestone under uniaxial compression based on nonlinear dynamics and rock energy evolution theory, and established an energy self-promotion-inhibition model.

In summary, scholars have made a lot of achievements in the study of mechanical properties and energy evolution of rock under different loading rates. However, there are few studies on the energy evolution mechanism of coal rock under different strain rates, especially on the impact-prone coal rock. Therefore, through uniaxial compression test and triaxial compression test of impact-prone coal rock under different strain rates, the mechanical parameters and impact tendency of deformation and failure of impact-prone coal rock under different strain rates are studied, and the energy evolution mechanism and self-promotion-inhibition mechanism of deformation and failure of impact-prone coal rock under different strain rates are analyzed. The research results can provide reference for the prevention and early warning of dynamic disasters of coal and rock mass with impact tendency.

Test scheme and mechanical characteristics analysis

Test scheme. The test coal samples were taken from Binchang mining area, and the general/normal physical parameters are shown in Table 1. The collected coal blocks were processed into standard cylinders (diameter D=50 mm, height H=100 mm) by core drilling machine, cutting machine, and grinding machine to ensure that the flatness deviation of the two ends of the sample was controlled in the range of 0–0.05 mm. In order to eliminate the discreteness of the sample, the density and ultrasonic longitudinal wave velocity of the sample were screened. The impact tendency of coal rock refers to the characteristics of high accumulation of deformation energy and impact failure in coal rock mass²⁸. The impact tendency of coal rock is analyzed by laboratory rock mechanics test²⁹. The uniaxial compressive strength of coal rock is 13.33 MPa, the elastic energy index is 6.85, the impact energy index is 5.71, and the dynamic failure time is 649 ms. Therefore, it can be determined that the sample is a strong impact tendency coal rock.

DTAW-8000 rock high pressure dynamic testing machine can be applied to rock uniaxial compression test and triaxial compression test. The whole test is controlled by computer program. The loading rate is 0.001–7 mm/s, the stress rate is 0.01–300 kN/m, the maximum loading force can reach 8000 kN, and the host stiffness is 6 GN/m. The test device is shown in Fig. 1.

In order to analyze the influence of strain rate on the mechanical characteristics and energy dissipation mechanism of coal rock, uniaxial compression test and triaxial compression test were carried out respectively. The strain rates of coal rock were $1 \times 10^{-5} s^{-1}$, $1 \times 10^{-4} s^{-1}$ and $1 \times 10^{-3} s^{-1}$ respectively. Due to the more complex occurrence conditions of deep-buried coal seams, it is more authentic to study the triaxial compression coal and rock under different strain rates with similar characteristics of deep-buried engineering mining. Therefore, according to the buried depth of the coal sample, the confining pressure of the triaxial compression test is taken as 8, 12, 16 MPa, and then the influence of different strain rates on the coal and rock under the triaxial compression state is studied. In order to reduce the friction force of the contact surface between the press devices and the coal sample and reduce the end effect of the rock, a layer of vaseline with a thickness of less than 1 mm was applied to the contact surface. When the sample was installed, the sample data was measured in real time by force and displacement sensors.

Mechanical characteristics analysis. As shown in Table 2, it can be seen that the mechanical parameters of coal rock under different strain rates under uniaxial compression and triaxial compression are different, but

Buried depth of coal rock/m	Density /g cm ⁻³	Porosity /%	Water content/%	Longitudinal wave velocity/km s ⁻¹
700	48.55-49.89	5.8-13.4	2.4-5.7	2.16-2.72

 Table 1. General/normal physical parameters of coal rock.

.....



Figure 1. Test device diagram.

			Peak strength		Elastic modulus		
Test	Confining pressure/MPa	Strain rate/s ⁻¹	Numerical value/MPa	Reduction rate/%	Numerical value/GPa	Reduction rate/%	Peak strain %
	0	1×10^{-5}	13.33		3.29		0.45
Uniaxial compression	0	1×10^{-4}	7.39	44.5	2.05	37.6	0.53
	0	1×10^{-3}	4.88	33.9	1.45	29.2	0.47
Triaxial compression	8	1×10^{-5}	22.16		3.42		0.65
	8	1×10^{-4}	33.08	-49.2	3.67	-7.3	1.13
	8	1×10^{-3}	17.84	45.9	3.16	13.8	0.57
	12	1×10^{-5}	26.28		3.51		0.82
	12	1×10^{-4}	40.21	-53.1	3.99	-13.6	1.51
	12	1×10^{-3}	22.21	44.7	3.46	13.2	0.68
	16	1×10^{-5}	51.45		4.98		1.32
	16	1×10^{-4}	60.83	-18.2	5.34	-7.2	1.88
	16	1×10^{-3}	40.21	33.9	4.62	13.4	0.93

Table 2. Test results of coal rock under different strain rates.

.....

the mechanical characteristics of coal rock under different strain rates under triaxial compression are similar. Because the strain rate has the same influence on the mechanical characteristics of coal rock under different confining pressures, this paper will analyze the mechanical properties and energy evolution characteristics of coal rock under uniaxial and triaxial conditions (confining pressure is 12 MPa). The reduction rate in the table is the reduction ratio of rock mechanics parameters at high strain rate to the peak strength or elastic modulus of rock at low strain rate. The peak strain is the axial strain at the peak point of the rock stress-strain curve.

As shown in Fig. 2, the strain rate will affect the strength and deformation characteristics of the sample, which is mainly reflected in the peak strength, elastic modulus, and peak strain of the sample. Under uniaxial compression, with the increase of strain rate, the peak strength and elastic modulus of coal rock decrease, but the reduction rate gradually slows down, and the peak strain increases first and then decreases. When the strain rate is 1×10^{-5} s⁻¹, the post-peak stress-strain curve of coal and rock produces a 'sudden decreasing' stress drop, which has a small residual stress. When the strain rate is 1×10^{-4} s⁻¹ and 1×10^{-3} s⁻¹, the initial cracks close rapidly, and the whole coal rock is unstable and destroyed, which appears obvious brittle characteristics. Under triaxial compression, the peak strength, elastic modulus, and peak strain of coal rock increase first and then decrease with the increase of the loading rates. Among them, the compaction stage of coal rock gradually decreases, the elastic and plastic stages are prolonged, and the final failure has certain ductility characteristics, indicating that the confining pressure weakens the initial fracture and other structures on the strength of coal rock.

Impact tendency analysis of coal rock under different strain rates. The stress environment in the mining area was the external condition that induced rock burst disasters, and the impact tendency of coal rock mass was the essential factor. The change of advance speed of mining would affect the loading mode and stress path of coal rock, and further impact its failure mode. In order to investigate the effect of strain rate on the impact tendency of coal rock, this paper uses the brittleness index modification index (BIM) to analyse the impact tendency of coal rock under different strain rates.

BIM index is to simplify the unloading curve to a straight line passing through the peak point with E50 as the slope, which is expressed as the ratio of the total energy E stored in the coal rock to the elastic energy Ee.



Figure 2. Triaxial stress-strain curves of coal rock under different strain rates.

When the elastic energy stored in the coal rock approached the total energy, the value of BIM was close to 1. At this time, the energy input from the outside was stored as elastic energy, and the coal rock energy was released instantly after the peak, and rock burst occurred. Therefore, the larger the BIM value, the lower the impact tendency of coal rock. M.Aubertin³⁰ divided the impact tendency according to the BIM value, as shown in Table 3.

Table 4 lists the BIM values of coal rock at different strain rates. With the increase of strain rate, the BIM value decreases first and then increases. When the strain rate is 1×10^{-5} s⁻¹, the impact tendency evaluation of coal rock is medium. When the strain rate increases to 1×10^{-4} s⁻¹, the impact tendency evaluation of coal rock is high. When the strain rate is 1×10^{-3} s⁻¹, the impact tendency evaluation of coal rock is different strain rate is 1×10^{-3} s⁻¹, the impact tendency evaluation of coal rock is high. When the strain rate, and increases first and then decreases. With the increase of strain rate, the accumulation ability of elastic energy of coal rock increases first and then decreases. It shows that the impact tendency of coal rock will increase first and then decrease with the increase of strain rate, and then change the elastic energy accumulation ability of coal rock.

Energy evolution law of coal rock with burst tendency

Energy dissipation theory of rock. The deformation and failure of coal rock are accompanied by four energy conversion forms: energy input, energy accumulation, energy dissipation and energy release. The total energy input from the outside is mainly converted into elastic energy and dissipative energy^{31,32}. Elastic strain energy is the energy stored in the process of reversible deformation of coal rock mass, which eventually leads to the deformation and failure of coal rock by accumulating energy. The dissipated energy is the energy lost by coal and rock during irreversible deformation (plastic deformation, damage, friction, and thermal radiation).

BIM	Burst tendency
$1.00 \le BIM \le 1.20$	High
$1.20 < BIM \le 1.50$	Medium
BIM > 1.50	Low

Table 3. Impact tendency evaluation based on BIM.

Strain rate /s ⁻¹	$A_1/kJ m^{-3}$	$A_2/kJ m^{-3}$	BIM
1×10^{-5}	25.72	34.87	1.35
1×10^{-4}	15.87	16.89	1.06
1×10^{-3}	7.61	13.86	1.82

Table 4. BIM index of coal and rock at different strain rates.

The process of energy dissipation is a dynamic process of continuous development, extension, derivation, weakening and disappearance of the internal structure of coal rock^{20,33}. According to the first law of thermodynamics.

$$E = E_e + E_d \tag{1}$$

where E is the total strain energy input from the outside, kJ/m^3 ; Ee is the elastic strain energy during coal rock deformation, kJ/m^3 ; Ed is the dissipated energy during coal rock deformation, kJ/m^3 . Figure 3 shows the relationship between dissipated energy and elastic strain energy in coal rock.

According to the energy analysis of the coal rock, the energy in each part of the coal rock is:

$$E = \int_{0}^{\varepsilon_{1}} \sigma_{1} d\varepsilon_{1} + \int_{0}^{\varepsilon_{2}} \sigma_{2} d\varepsilon_{2} + \int_{0}^{\varepsilon_{3}} \sigma_{3} d\varepsilon_{3}$$
(2)

$$E_e = \frac{1}{2}\sigma_1\varepsilon_1^e + \frac{1}{2}\sigma_1\varepsilon_2^e + \frac{1}{2}\sigma_3\varepsilon_3^e$$
(3)

where σ_1 , σ_2 and σ_3 are the principal stresses of coal rock; ϵ_1^{e} , ϵ_2^{e} and ϵ_3^{e} are the elastic strains along the principal stress direction.

Under the condition of uniaxial compression, σ_2 and σ_3 are both 0, so the total strain energy and elastic strain energy of coal rock are simplified as:

$$E = \int \sigma_1 d\varepsilon_1 = \sum_{i=1}^n \frac{1}{2} (\sigma_{1i+1} + \sigma_{1i}) (\varepsilon_{1i+1} - \varepsilon_{1i})$$

$$\tag{4}$$

$$E_e = \frac{1}{2}\sigma_1\varepsilon_1^e = \frac{\sigma_1^2}{2E_u} \tag{5}$$

where σ_{1i} and ϵ_{1i} are the stress and strain values on the principal stress–strain curve. In the calculation of elastic strain energy per unit of coal rock, the elastic mod-ulus E_0 can approximately replace $E_u^{34,35}$. The error caused by the replacement is generally within 5%³⁶. Thus, the elastic strain energy E_e can be approximately given by

$$E_e \approx \frac{\sigma_1^2}{2E_0} \tag{6}$$

Under the conventional triaxial condition, it is assumed that the coal rock mass is isotropic, and the circumferential elastic strain energy is relatively small and negligible compared with the axial elastic strain energy³⁷. Therefore, the elastic strain energy in coal rock can be calculated according to Formula (6). The total strain energy E in coal is:

$$E = \sum_{i=1}^{n} \frac{1}{2} (\sigma_{1i} + \sigma_{1i-1}) (\varepsilon_{1i} - \varepsilon_{1i-1}) - 2 \sum_{i=1}^{n} \sigma_3 (\varepsilon_{3i} - \varepsilon_{3i-1}).$$
(7)



Figure 3. Relationship between dissipated energy and elastic strain energy in coal rock.

.....

Energy evolution law. Based on the theory of rock energy dissipation, the experimental data are substituted into Formulae (1) (4) (6) (7) to calculate the total energy E, elastic energy E_e , dissipated energy E_d , elastic energy ratio and dissipated energy ratio in the deformation and failure of coal rock under uniaxial compression and triaxial compression. The energy evolution curves of coal rock with impact tendency under different strain rates are shown in Fig. 5.

It can be seen from Fig. 4a-c that the total energy, elastic energy, and dissipation energy show different evolution characteristics during the deformation and failure process of impact-prone coal rock under uniaxial



(a) 1×10^{-5} s⁻¹ strain rate ($\sigma_3 = 0$ MPa)



(c) 1×10^{-3} s⁻¹ strain rate ($\sigma_3 = 0$ MPa)



(e) $1\times 10^{\text{-3}} \text{ s}^{\text{-1}}$ strain rate (σ_3 = 12 MPa)



(b) $1 \times 10^{-4} \text{ s}^{-1}$ strain rate ($\sigma_3 = 0 \text{ MPa}$)



(d) 1×10^{-3} s⁻¹ strain rate ($\sigma_3 = 12$ MPa)



(f) $1\times 10^{\text{-3}}~\text{s}^{\text{-1}}$ strain rate (σ_3 = 12 MPa)

Figure 4. Energy evolution curves of coal rock under different strain rates.





Figure 5. Internal energy ratio curve of uniaxial compression coal rock under different strain rates.

compression. The elastic energy increases nonlinearly before the peak value. When the energy storage limit is reached, the elastic energy stored in the coal rock is suddenly released due to the failure of coal rock. The dissipation energy increases slowly in the process of initial fracture compaction. The dissipation energy in the elastic stage is in a stable state, and the dissipation energy in the plastic stage will continue to increase until the dissipation energy of coal rock failure increases suddenly. Due to the large strain rate at high strain rate of 1×10^{-3} s⁻¹, the internal structure of coal rock is not completely destroyed, and it still has a certain bearing capacity after the peak. With the further development of deformation and failure, the internal structure of coal rock is damaged, and coal rock produces obvious plastic deformation.

As shown in Fig. 4d–f, compared with the energy evolution of coal rock under uniaxial compression, the change trend of total energy, elastic energy, and dissipation energy of coal rock under triaxial compression is similar. However, due to the action of confining pressure, the initial cracks in coal rock are quickly compacted and the new cracks expand rapidly, so the duration of coal rock compaction stage and elastic stage is very short. After entering the plastic stage, with the increase of load, the dissipated energy in coal rock is much higher than the elastic energy. Therefore, the energy dissipation curves of coal and rock with different strain rates under uniaxial compression are only divided into stages in this paper.

The proportion of elastic energy and dissipated energy in the deformation and failure process of coal rock with impact tendency reflects the internal energy structure of coal rock. As shown in Fig. 5, the elastic energy ratio curve of coal rock with different strain rates under uniaxial compression is 'S' type. Therefore, according to the energy ratio of coal rock with different strain rates under uniaxial compression, the energy evolution of coal rock with impact tendency can be divided into four stages: initial energy damage stage, energy hardening stage, energy softening stage and failure stage.

Initial energy damage stage (from O to A). The dissipation energy increases nonlinearly with the increase of deformation, and the proportion of dissipation energy Ed in coal rock is greater than that of elastic energy Ee, which is mainly caused by the closure and friction of microcracks in coal rock. The total energy and elastic

energy also increase with the increase of deformation, and with the closure of micro cracks, the growth rate of elastic energy increases gradually, and finally the coal rock enters the next stage (energy hardening stage) after the dissipation energy is equal to the elastic energy.

Energy hardening stage (from A to B). After the micro-fractures in coal rock are completely closed, the total energy and elastic energy increase with the same trend with the increase of coal rock deformation, and the growth rate is greater than the dissipation energy growth curve. The dissipation energy curve is approximately horizontal, and the elastic performance is greater than the dissipation energy in the whole process (the proportion of elastic energy Ee is greater than the proportion of dissipation energy Ed). The total energy input at this stage is basically stored in the coal rock, and the elastic properties of the coal rock are continuously accumulated, and the energy dissipation is less.

Energy softening stage (from B to C). As the proportion of elastic energy in coal rock reaches the peak, the total energy and elastic energy in coal rock increase with the increase of deformation, but the growth rate of elastic energy decreases gradually. At this stage, part of the total energy input continues to be stored in the form of elastic energy, and part of it is rapidly released by friction, expansion, and new cracks. Therefore, the growth rate of dissipated energy is gradually increasing (the proportion of dissipated energy increases). The deformation ability of coal rock is obviously enhanced, and new microcracks are generated and extended inside the coal rock. The generation of these cracks is bound to cause more energy dissipation.

Failure stage (after point C). When the peak strength is reached, the rock enters the failure stage. At this stage, the dissipation energy evolution curve increases sharply, while the elastic energy evolution curve decreases sharply. This is due to the rapid expansion and penetration of internal cracks in coal rock, resulting in the loss of bearing capacity of coal rock, and the elastic energy accumulated in coal rock is quickly released in the form of dissipated energy, resulting in a sharp increase in the dissipation energy curve.

Under uniaxial compression, when the strain rate is 1×10^{-4} s⁻¹ (Fig. 5), the dissipated energy in the energy hardening stage (AB stage) increases slowly first and then gradually stabilizes. The possible reason was that there were new cracks in the coal rock at the early stage of energy hardening, causing an increase in the dissipated energy, and the dissipated energy became stable after the cracks were closed. As a result, the proportion of dissipated energy in energy hardening stage (A to B) in Fig. 5 B rose dramatically. In Reference³⁸, the energy evolution of rock is divided into three stages ac-cording to the energy ratio characteristics. In this paper, by contrast, the energy evolution was divided into four stages: initial energy damage stage, energy hardening stage, energy softening stage, and failure stage. This helps to better reflect the internal energy mechanism of burst-prone coal rock under different strain rates.

Analysis of peak point energy index under different strain rates. The strain rate will affect the energy index of the peak point of the impact tendency coal rock. As shown in Table 5, with the increase of strain rate, the total energy and elastic energy of coal rock at peak point under uniaxial compression continue to decrease. This is because there are many cracks in the impact-prone coal rock itself. With the increase of strain rate, the stress concentration at the crack is more obvious, which leads to the expansion and penetration of more cracks. The energy required for specimen failure is decreasing, and the elastic energy stored in coal rock will also decrease. The proportion of elastic energy at the peak point of coal rock increases first and then decreases with the increase of strain rate.

Compared with uniaxial compression, the energy index of coal peak point varies with different strain rates under triaxial compression. With the increase of strain rate, the total energy, elastic energy, and dissipated energy of at the peak point of coal increase first and then decrease. It shows that when the strain rate reaches 1×10^{-4} s⁻¹, the coal rock burst risk is the highest in the coal rock mass with high buried depth.

Energy self-promotion-inhibition mechanism of burst-prone coal rock

The external input energy is transformed into elastic energy accumulated inside the rock mass. This effect is known as strain hardening effect. Accordingly, what suppresses this effect is the strain softening effect. There are two mechanisms (energy accumulation mechanism and energy dissipation mechanism) in the pre-peak energy

Confining pressure/MPa	Strain rate/s ⁻¹	Total energy /kJ m ⁻³	Elastic energy/kJ m ⁻³	Proportion of elastic energy/%	Dissipated energy/kJ m ⁻³	Proportion of dissipated energy/%
0	1×10^{-5}	34.87	23.42	67.16	11.45	32.84
	1×10^{-4}	16.89	14.12	83.59	2.77	16.40
	1×10^{-3}	13.86	8.52	61.47	5.33	38.43
12	1×10^{-5}	341.8	117.1	34.25	224.8	65.75
	1×10^{-4}	874.3	188.4	21.55	685.8	78.45
	1×10^{-3}	287.6	71.26	24.78	216.3	75.22

 Table 5. Energy index of coal rock peak point at different strain rates.

.....

conversion process of burst-prone coal rocks, which are driven by the pre-peak strain hardening deformation mechanism of coal rock³⁹. According to the analysis of microscopic deformation mechanism of rock⁴⁰, the total energy of the rock at time t is U, at which there are m types of strain hardening effects and n types of strain softening effects. The energy transferred by each effect at time t is U_i and U_k, respectively, the total mechanical energy input from the outside is U_c, and the energy released from the rock is U_t.

$$U = \sum_{i=1}^{m} U_i + \sum_{k=1}^{n} U_k$$
(8)

Assuming that there was only one strain hardening effect and strain softening effect in the microscopic deformation process, then they two effects can be expressed as

$$\frac{dU_i}{d_t} = [\mathbf{a}_{i0}(U_c - U_{i0}) - \mathbf{a}_i U_i + \mathbf{a}_{ik} U_k] U_i$$
(9)

$$\frac{dU_k}{d_t} = [\mathbf{b}_{k0}(U_i - U_{k0}) - (b_{k1} - b_{k2})U_k - \mathbf{b}_{k3}U_t]U_k$$
(10)

where U_{i0} is the lowest activation energy of the i-th hardening mechanism; U_{k0} is the lowest activation energy of the k-th softening mechanism; a_{i0} is the promotion coefficient of strain hardening; ai is the inhibition coefficient of the i-th strain hardening mechanism; a_{ik} is the coefficient of converting U_i into heat energy and internal energy; b_{k1} is the self-competition coefficient of the k-th strain softening mechanism; b_{k2} is the self-promotion coefficient of the k-th strain softening mechanism; b_{k3} is the energy diffusion coefficient.

The strain hardening mechanism converted the external input energy into elastic energy, but the accumulation of a large amount of elastic energy was also affected by the self-inhibition effect. Since the temperature of the indoor test changed slowly, it is assumed that the thermal energy loss in the coal specimen was not considered. So Eq. (9) can be rewritten as:

$$\frac{dU_e}{d_t} = [a_{e0}(U_{ec} - U_{i0}) - a_e U_e]U_e$$
(11)

where U_e is the elastic energy, U_{i0} is the activation value of elastic energy, U_{ec} is the energy input from the outside to promote the accumulation of elastic energy, a_{e0} is the promotion activation coefficient, and a_e is the inhibition coefficient. Therefore, the elastic energy of coal rock mass can be expressed as

$$U_e = \frac{b}{a_e + e^{a_e k - bt}} \tag{12}$$

where $b = a_{e0}(U_{ec} - U_{i0})$, and k is a constant.

Equation 12 is the self-promotion-inhibition evolution model of pre-peak energy of burst-prone coal rock. By fitting the pre-peak elastic energy of the burst-prone coal rock under different strain rates, the elastic energy inhibition coefficient as and the promotion coefficient k can be obtained, so as to analyze the elastic energy variation characteristics of the burst-prone coal rock under different strain rates. The uniaxial and triaxial compression test data of coal rock under different strain rates $(1 \times 10^{-5} \text{ s}^{-1}, 1 \times 10^{-4} \text{ s}^{-1} \text{ and } 1 \times 10^{-3} \text{ s}^{-1})$ are fitted according to the model in Eq. 12. Thus, the nonlinear fitting curve of pre-peak elastic energy is obtained, as showed in Fig. 6. The corresponding elastic energy fitting parameters as and b are shown in Table 6.

According to the fitting parameter R^2 , the self-promotion-inhibition evolution model of pre-peak energy of coal rock fits well with the experimental results, which can truly reflect the self-promotion-inhibition evolution process of pre-peak energy of coal rock. Herein, a_e is the inhibition coefficient of elastic energy, and b is the promotion coefficient of elastic energy.

It can be seen from Fig. 6 that the promotion effect of elastic properties in coal rock is greater than the inhibition effect of elastic energy. Therefore, the elastic energy accumulates rapidly in coal rock, which further leads to the failure of coal rock. When the strain rate is 1×10^{-5} s⁻¹, the internal elastic strain energy of coal rock accumulates slowly in the rock sample, so the inhibition effect and promotion effect of elastic energy generation in coal rock will gradually increase, and the faster elastic energy accumulation will lead to the enhancement of elastic energy inhibition effect. Therefore, the elastic energy promotion coefficient and inhibition coefficient is greater than that of promotion coefficient.

In summary, the pre-peak elastic energy promotion coefficient of impact prone coal rock is greater than the inhibition coefficient. With the increase of strain rate, the elastic energy promotion coefficient and inhibition coefficient of coal rock mass also increase, and the promotion coefficient increases greatly, indicating that the increase of strain rate will promote the generation of elastic energy inside coal rock.

Conclusions

In this paper, the uniaxial compression test and triaxial compression test of coal rock with burst tendency are used to study the mechanical properties of coal rock with burst tendency under different strain rates, the change law of burst tendency, the law of energy evolution and the self-promotion-inhibition mechanism of pre-peak energy. The main conclusions are as follows:





Figure 6. Fitting curves of elastic energy of coal rock under different strain	rates.
--	--------

	Inhibition coefficient (a_e)		ent (a_e)	Promotion coeffici		
Confining pressure/MPa	Strain rate/s ⁻¹	Numerical value	Amplification	Numerical value	Amplification	R^2
0	1×10^{-5}	2.04		51.25		0.997
	1×10^{-4}	27.86	12.65	495.5	8.66	0.997
	1×10^{-3}	741.78	25.62	6124.2	11.35	0.992
12	1×10^{-5}	0.13		24.3		0.998
	1×10^{-4}	0.86	5.61	128.2	4.27	0.998
	1×10 ⁻³	61.52	303.6	4446.2	33.68	0.992

Table 6. Coal rock fitting parameters under different strain rates.

1. The peak strength and elastic modulus of coal rock with impact tendency in uniaxial compression test decrease with the increase of strain rate, while the peak strength and elastic modulus of coal rock in triaxial compression test increase first and then decrease with the increase of strain rate. According to the impact tendency energy index BIM, it is determined that the impact tendency of coal rock under uniaxial compression will increase first and then decrease with the increase of strain rate.

- 2. In the uniaxial compression test, according to the change law of the energy proportion of the coal rock with impact tendency, the evolution of the load energy of the coal rock with impact tendency is divided into four stages: initial energy damage stage, energy hardening stage, energy softening stage and failure stage.
- 3. The conversion rate of dissipated energy in coal rock with impact tendency at peak point is positively correlated with strain rate. Under uniaxial compression, the total energy and elastic energy of coal rock with peak impact tendency decrease with the increase of strain rate, and the change of strain rate will affect the elastic energy accumulation force of coal rock. In addition, with the increase of strain rate under triaxial compression, the total energy of coal rock at the peak point increase first and then decrease, which shows that the impact tendency of coal rock has the highest impact risk when the strain rate is 1×10^{-4} s⁻¹ under confining pressure.
- 4. A pre-peak energy self-promotion-inhibition evolution model of impact prone coal rock is established. The elastic energy promotion coefficient of impact prone coal rock is much larger than the inhibition coefficient. With the increase of strain rate, the promotion coefficient and inhibition coefficient of coal rock elastic energy will gradually increase, and the promotion coefficient will increase greatly. Therefore, the increase of strain rate will promote the generation of elastic energy inside coal rock.

Data availability

The data used to support the findings of this study are available from the corresponding author upon request.

Received: 16 May 2023; Accepted: 22 August 2023 Published online: 23 August 2023

References

- Chen, S. J., Yin, D. W., Jiang, N., Wang, F. & Guo, W. J. Simulation study on effects of loading rate on uniaxial compression failure of composite rock-coal layer. *Geomech. Eng.* 17, 333–342 (2019).
- 2. Huang, B. X. & Liu, J. W. The effect of loading rate on the behavior of samples composed of coal and rock. *Int. J. Rock Mech. Min. Sci.* 61, 23–30 (2013).
- Chong, K. P., Hoyt, P. M., Smith, J. W. & Paulsen, B. Y. Effects of strain rate on oil shale fracturing. Int. J. Rock Mech. Min. Sci. Geomech. Abstr. 17, 35–43 (1980).
- 4. Lajtai, E. Z., Scott-Duncan, E. J. & Carter, B. J. The effect of strain rate on rock strength. Rock Mech. Rock Eng. 24, 99–109 (1991).
- Swan, G., Cook, J., Bruce, S. & Meehan, R. Strain rate effects in Kimmeridge bay shale. Int. J. Rock Mech. Min. Sci. Geomech. Abstr. 26, 135–149 (1989).
- Zhang, L. Y. & Mao, X. B. Experimental study of the mechanical effects of loading rates on limestone at high Temperature. Rock Soil Mech. 31, 3511–3515 (2010).
- 7. Backers, T., Fardin, N., Dresen, G. & Stephansson, O. Effect of loading rate on mode I fracture toughness, roughness and micromechanics of sandstone. *Int. J. Rock Mech. Min. Sci.* **40**, 425–433 (2003).
- 8. Liu, X. W. et al. Experimental and numerical study on failure characteristics and mechanism of coal under different quasi-static loading rates. *Theor. Appl. Fract. Mech.* **121**, 103478 (2022).
- 9. Yu, L. Q. et al. Experimental and numerical simulation study on crack propagation of fractured fine sandstone under the influence of loading rate. J. China Coal Soc. 46, 3488–3501 (2021).
- 10. Ren, J. X. *et al.* Study on the mechanical properties of saturated red sandstone under freeze-thaw conditions. *Environ. Earth Sci.* **81**, 1–20 (2022).
- 11. Zhai, M. Y., Xu, C., Xue, L., Cui, Y. & Dong, J. Y. Loading rate dependence of staged damage behaviors of granite under uniaxial compression: Insights from acoustic emission characteristics. *Theor. Appl. Fract. Mech.* **122**, 103633 (2022).
- 12. Zhang, K. *et al.* Study on characteristics of acoustic emission b value of coal rock with outburst-proneness under coupled static and dynamic loads. *Shock Vib.* **2023**, 2400632 (2023).
- 13. Sun, F. Y., Fan, J. Q., Guo, J. Q. & Liu, X. L. Experimental and numerical investigation of energy evolution characteristic of granite considering the loading rate effect. *Adv. Mater. Sci. Eng.* **2022**, 8260107 (2022).
- 14. Lai, X. P. *et al.* Mechanical behavior characteristics and energy evolution law of coal samples under the influence of loading rate—a case study of deep mining in wudong coal mine. *Minerals* **12**, 1032–1032 (2022).
- Hai, P., Han, L. J., Zhang, M. W., Meng, Q. B. & Zhang, Z. Z. Experimental research on rock energy evolution under uniaxial cyclic loading and unloading compression. *Geotech. Test. J.* 41, 20170233–20170233 (2018).
- Gao, F., Cao, S. P., Zhou, K. P., Lin, Y. & Zhu, L. Y. Damage characteristics and energy-dissipation mechanism of frozen-thawed sandstone subjected to loading. J. Technol. Sci. 169, 102920 (2020).
- Guo, H. J. et al. A study on the effects of loading axial pressure rate on coal mechanical properties and energy evolution law. Geofluids 2022, 5593173 (2022).
- Peng, R. D. *et al.* Energy dissipation and release during coal failure under conventional triaxial compression. *Rock Mech. Rock Eng.* 48, 509–526 (2015).
- 19. Zhou, X. P. Triaxial compressive behavior of rock with mesoscopic heterogeneous behavior: Strain energy density factor approach. *Theor. Appl. Fract. Mech.* **45**, 46–63 (2006).
- Steffler, E. D., Epstein, J. S. & Conley, E. G. Energy partitioning for a crack under remote shear and compression. Int. J. Fract. 120, 563–580 (2003).
- 21. Xie, H. P., Li, L. Y., Ju, Y., Peng, R. D. & Yang, Y. M. Energy analysis for damage and catastrophic failure of rocks. *Sci. China Technol. Sci.* 54, 199–209 (2011).
- Li, X. B., Lok, T. S. & Zhao, J. Dynamic characteristics of granite subjected to intermediate loading rate. Rock Mech. Rock Eng. 38, 21–39 (2005).
- Zhang, Z. X., Kou, S. Q., Jiang, L. G. & Lindqvist, P. A. Effects of loading rate on rock fracture: Fracture characteristics and energy partitioning. *Int. J. Rock Mech. Min. Sci.* 37, 745–762 (2000).
- Li, Y. Z., Huang, D. & Li, X. A, "Strain rate dependency of coarse crystal marble under uniaxial compression: Strength, deformation and strain energy. *Rock Mech. Rock Eng.* 4, 1153–1164 (2014).
- Hua, A. & You, M. Q. Rock failure due to energy release during unloading and application to underground rock burst control. *Tunn. Undergr. Space Technol.* 16, 241–246 (2001).
- Meng, Q. B., Zhang, M. W., Zhang, Z. Z., Han, L. J. & Pu, H. Research on non-linear characteristics of rock energy evolution under uniaxial cyclic loading and unloading conditions. *Environ. Earth Sci.* 78, 1–20 (2019).

- Wang, G. L. et al. Analysis of nonlinear energy evolution in fractured limestone under uniaxial compression. Theor. Appl. Fract. Mech. 120, 103387 (2022).
- 28. Kidybiński, A. Bursting liability indices of coal. Int. J. Rock Mech. Min. Sci. Geomech. Abstr. 18, 295-304 (1981).
- 29. Zhang, K. *et al.* Fracture behaviors of prefabricated fractured coal rock under graded static-dynamic coupled loading. J. Xi'an Univ. Sci. Technol. 42, 546–554 (2022).
- Aubertin, M., Gili, D. E. & Simon, R. On the use of the brittleness index modified(BIM) to estimate the post-peak behavior of rocks. *Rock Mech.* 12, 945–952 (1994).
- Zhang, Z. Z. & Gao, F. Experimental investigation on the energy evolution of dry and water-saturated red sandstones. Int. J. Min. Sci. Technol. 25, 383–388 (2015).
- 32. Wang, G. L., Gao, T. C., Sun, F., Wen, X. X. & Zhang, L. Study on the Meso-Energy Damage Evolution Mechanism of Single-Joint Sandstone under Uniaxial and Biaxial Compression. *Adv. Mater. Sci. Eng.* **2021**, 5245402 (2021).
- Sujatha, V. & Chandra Kishen, J. M. Energy release rate due to friction at bimaterial interface in dams. J. Eng. Mech. 129, 793–800 (2003).
- 34. Gerstle, K. H. Advanced mechanics of materials. J. Struct. Eng. 127, 598-598 (2001).
- Mikhalyuk, A. V. & Zakharov, V. V. Dissipation of dynamic-loading energy in quasi-elastic deformation processes in rocks. J. Appl. Mech. Tech. Phys. 38, 312–318 (1997).
- 36. Huang, D., Huang, R. Q. & Zhang, Y. X. Experimental investigations on static loading rate effects on mechanical properties and energy mechanism of coarse crystal grain-marble under uniaxial compression. *Chin. J. Rock Mech. Eng.* **31**, 245–255 (2012).
- Ma, Z. Q., Jiang, Y. D., Li, Y. W., Yang, Y. M. & Li, H. T. Experimental research on influence of loading rate and confining pressure on energy evolution of coal. *Chin. J. Geotech. Eng.* 38, 2114–2121 (2016).
- Chen, Z. Q., He, C., Ma, G. Y., Xu, G. W. & Ma, C. C. Energy damage evolution mechanism of rock and its application to brittleness evaluation. Rock Mech. Rock Eng. 52, 1265–1274 (2019).
- Labuz, J. F. & Dai, S. T. Residual strength and fracture energy from plane-strain testing. J. Geotech. Geoenviron. Eng. 128, 882–889 (2000).
- 40. An, X. X. *et al.* Nonlinear energy evolution characteristics of diorite examined by triaxial loading–unloading and acoustic emission tests. *Materials* **15**, 6434–6434 (2022).

Acknowledgements

This study was supported by the Natural Science Foundation of china (12072259), and the Science and Joint fund project-enterprise-Shaanxi coal joint fund project (2019JLP-01).

Author contributions

Conceptualization, Y.Z., K.Z. and L.Z.; Writing—review and editing, K.Z. and L.Z. Project admin-istration, J.R. and K.Z.; Data curation, S.Z.; Writing—original draft preparation, Y.Z. Visualization, Y.Z., R.Z. and S.Z.; Formal analysis, K.Z. and Y.Z.; methodology, J.R. and L.Z.; Validation, Y.Z., L.Z. and K.Z.; Resources, S.Z.; Supervision, J.R.; Investigation, K.Z., Y.C. and Y.Z.; Software, S.Z. and Y.Z. All authors have read and agreed to the published version of the manuscript.

Funding

Authors should state how the research and publication of their article was funded, by naming financially supporting bodies followed by any associated grant numbers in square brackets.

Competing interests

The authors declare no competing interests.

Additional information

Correspondence and requests for materials should be addressed to K.Z.

Reprints and permissions information is available at www.nature.com/reprints.

Publisher's note Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.

Open Access This article is licensed under a Creative Commons Attribution 4.0 International License, which permits use, sharing, adaptation, distribution and reproduction in any medium or format, as long as you give appropriate credit to the original author(s) and the source, provide a link to the Creative Commons licence, and indicate if changes were made. The images or other third party material in this article are included in the article's Creative Commons licence, unless indicated otherwise in a credit line to the material. If material is not included in the article's Creative Commons licence and your intended use is not permitted by statutory regulation or exceeds the permitted use, you will need to obtain permission directly from the copyright holder. To view a copy of this licence, visit http://creativecommons.org/licenses/by/4.0/.

© The Author(s) 2023