# **scientific** reports



# **OPEN** Positron annihilation spectroscopy study of radiation-induced defects in W and Fe irradiated with neutrons with different spectra

O. V. Ogorodnikova<sup>1™</sup>, M. Majerle<sup>2</sup>, J. Čížek<sup>3</sup>, S. Simakov<sup>4</sup>, V. V. Gann<sup>5</sup>, P. Hruška<sup>3</sup>, J. Kameník<sup>2</sup>, J. Pospíšil<sup>6</sup>, M. Štefánik<sup>2</sup> & M. Vinš<sup>7</sup>

The paper presents new knowledge on primary defect formation in tungsten (W) and iron (Fe) irradiated by fission and high-energy neutrons at near-room temperature. Using a well-established method of positron-annihilation lifetime-spectroscopy (PALS), it was found that irradiation of W in the fission reactor and by high-energy neutrons from the p(35 MeV)-Be generator leads to the formation of small radiation-induced vacancy clusters with comparable mean size. In the case of Fe, smaller mean size of primary radiation-induced vacancy clusters was measured after irradiation with fission neutrons compared to irradiation with high-energy neutrons from the p(35 MeV)-Be generator. It was found that one of the reasons of the formation of the larger size of the defects with lower density in Fe is lower flux in the case of irradiation with high-energy neutrons from the p(35 MeV)-Be source. The second reason is enhanced defect agglomeration and recombination within the energetic displacement cascade at high energy primary knock-on-atoms (PKAs). This is consistent with the concept of the athermal recombination corrected (arc-dpa) model, although the measured dpa cross-section of both fission neutrons and wide-spectrum high-energy neutrons in W is between the conventional Norgett-Robinson-Torrens (NRT-dpa) and arc-dpa predictions. This means that the physics of the primary radiation effects in materials is still not fully known and requires further study through a combination of modeling and experimental efforts. The present data serve as a basis for the development of an improved concept of the displacement process.

Tungsten (W) is considered as an attractive material for use in advanced fission and fusion reactors because of its high melting point, excellent high temperature strength, good thermal conductivity, low physical sputtering yield, relatively good resistance against radiation swelling, and good resistance against corrosion. For these reasons, W is a leading candidate as a material that will be in direct contact with plasma in future fusion reactors, ITER and DEMO<sup>1,2</sup>. Reduced-activation ferritic-martensitic (RAFM) steels are considered as primary structural materials in advanced fission and fusion reactors<sup>3-6</sup>. To predict the behavior of materials under irradiation, it is important to understand primary defect formation.

The importance of controlling neutron-induced degradation of fission reactor materials has necessitated the study of radiation damage to metals over many decades. In future thermonuclear and advanced fission reactors, materials must withstand irradiation of high-energy neutrons. In the fusion reactor, materials will be irradiated with 14 MeV (in peak) neutrons generated by D-T fusion reaction. As a fusion neutron source does not exist yet,

<sup>1</sup>National Research Nuclear University "MEPHI" (Moscow Engineering Physics Institute), Kashirskoe sh. 31, Moscow, Russia. <sup>2</sup>Nuclear Physics Institute of the CAS, Řež 130, 250 68 Řež, Czech Republic. <sup>3</sup>Department of Low-Temperature Physics, Charles University, V Holešovičkách 2, 180 00 Prague, Czech Republic. <sup>4</sup>Institute for Neutron Physics and Reactor Technology, Karlsruhe Institute of Technology, Hermann-von-Helmholtz-Platz 1, 76344 Eggenstein-Leopoldshafen, Germany. 5National Science Centre "Kharkov Institute of Physics and Technology", Kharkov, Ukraine. <sup>6</sup>Department of Condensed Matter Physics, Charles University, Faculty of Mathematics and Physics, Ke Karlovu 5, 121 16 Prague 2, Czech Republic. <sup>7</sup>Research Centre Řež, Řež 130, 250 68 Řež, Czech Republic. <sup>™</sup>email: olga@plasma.mephi.ru

fission neutrons and charged particles are widely used to simulate fusion neutron-induced damage in materials, see, for example<sup>7-9</sup>. In early papers, the total density of radiation-induced defects in metals irradiated with electrons<sup>10</sup>, fission neutrons<sup>11,12</sup> and fast neutrons from d(30 MeV)-Be source<sup>13</sup> was measured using resistivity technique. However, data on the size distribution of radiation-induced defects were not reported. This is due to the fact that the resistivity experiments do not take into account agglomeration of primary radiation-induced defects into clusters of different sizes, although the size, shape and spatial distribution of defects can affect the material properties on a long-term time scale. Therefore, advanced microscopic studies are needed to understand what fraction of irradiated vacancies agglomerates into vacancy clusters, what is the morphology and size distribution of vacancy clusters, and what is the role of vacancy clusters in the deterioration of the macroscopic physical properties of irradiated materials.

A recent paper  $^{14}$  compared radiation-induced defects in W and iron (Fe) irradiated with high-energy protons and neutrons. Positron annihilation lifetime spectroscopy (PALS) was employed for characterization of size and concentration of radiation-induced defects  $^{15}$ . PALS is an effective technique for detecting and characterizing radiation-induced defects that are often below the resolution limit of transmission electron microscopy (TEM). It was shown that 22.5 MeV protons produce mono-vacancies in W but the neutrons from the p(35 MeV)-Be generator produce vacancy clusters with an average size of 3–5 vacancies during irradiation at ambient temperature up to a fluence of  $1.4 \times 10^{20}$  n/m² (corresponding to about 9 appm of the NRT-dpa). In the present paper, we extend the pioneer work  $^{14}$  by comparing the cluster size of vacancy-type defects formed in W and Fe after irradiation with fission and wide-spectrum high energy neutrons.

Experimental data on the total primary defect production under different types of irradiation can serve as a basis for comparison with models of the displacement process. The classical 'NRT' model developed in 1975 by Norgett, Robinson, and Torrens<sup>16,17</sup> is used to estimate the displacement per atom (dpa) produced by different types of particles. The number of primary knock-on atoms  $N_d$  in the irradiated material can be calculated using the NRT-dpa model as follows:

$$N_d(T) = \begin{cases} 0, & \text{if} \quad T < E_d \\ 1, & \text{if} \quad E_d < T < 2E_d/0.8 \\ 0.8T/(2E_d), & \text{if} \quad 2E_d/0.8 < T < \infty. \end{cases}$$
 (1)

In the above equation, T denotes the kinetic energy of reaction recoil which is transferred to the knocked atom by an elastic collision. The symbol  $E_d$  indicates the threshold of energy required to displace an atom from the lattice.

In general, the threshold displacement energy is a function of crystallographic orientation. However, the crystallographic-averaged  $E_d$  is used in the Eq. (1). The average threshold energy  $E_d$  for neutron-induced damage cross sections was selected to be 40 eV for Fe and 90 eV for W according to recommendations in Ref. Because the NRT-dpa model neglects ballistic in-cascade recombination effects, the experimental defect concentration can be lower than the calculated NRT-dpa value 19,20. The recently proposed athermal recombination-corrected (arc-dpa) model includes the defect generation efficiency,  $\xi(T)$ , and the third line of Eq. (1) is modified into the following form  $^{21}$ 

$$N_d = 0.8T\xi(T)/(2E_d). (2)$$

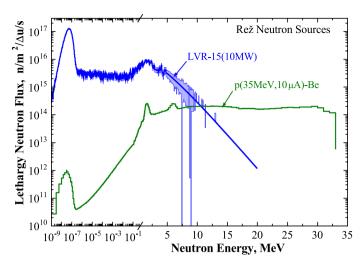
In the work<sup>14</sup>, it was shown that experimental data for neutron- and proton-irradiated Fe are better described by the arc-dpa model than the NRT-dpa model. Whereas experimental data for neutron- and proton-irradiated W are between NRT-dpa and arc-dpa predictions. In the present paper, we compare the arc-dpa and NRT-dpa predictions with experimental data of the primary radiation defects in W and Fe after irradiation with fission and energetic neutrons. This work highlights the potential of PALS technique for studying primary radiation damage, as well as for validation radiation damage models.

### Experimental

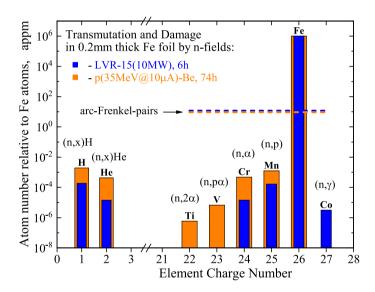
Cold-rolled W foils with purity of 99.97% produced by Plansee and ARMCO type Fe foils with purity of 99.8% produced by Goodfellow were mechanically polished to mirror-like state. Then W foils were recrystallized at 2000 K for 40 min in ultra-high vacuum with a base pressure lower than  $2\times 10^{-9}$  mBar. The Fe foils were annealed at 1173 K for one hour in vacuum with a base pressure of  $1\times 10^{-6}$  mBar. In the case of Fe, such heat treatment allows us to minimize the density of defects but conserves the  $\alpha$ -phase of bcc Fe. The size of samples was  $10\times 10$  mm² and their thickness was 100 and 200  $\mu$ m for W and Fe, respectively.

Wide-spectrum high energy neutron irradiation was carried out at a source of fast neutrons with continuous neutron spectra up to 33 MeV generated by a p(35 MeV) beam incident on a thick Be target at the U-120 M cyclotron of Nuclear Physics Institute (NPI CAS) in Řež (see Ref.  $^{22}$  for details). The thickness of the Be target was 8 mm, which means that the protons were stopped inside the target. The W and Fe foils were irradiated in air in the position of 15 mm from the front of the Be target. The average current of the proton beam was 10  $\mu$ A, which resulted in a neutron flux of about  $10^{15}$  m $^{-2}$  s $^{-1}$  at the current sample location. The irradiation was carried out at room temperature. More information about the irradiation procedure is given in Ref.  $^{14}$ .

Irradiation with fission neutrons was performed in the channels of H9/3 of the LVR-15 research reactor of the Research Centre Řež<sup>23</sup>. The neutron spectrum in the irradiation position was calculated by the neutron transport code MCNP6.1<sup>24</sup> using the current fuel rods distribution. The neutron flux was estimated to be  $\sim 2.9 \times 10^{17}$  m<sup>-2</sup> s<sup>-1</sup>. The fraction of fast neutrons with energies of E>0.1 MeV was calculated as 7.9% of the total neutron flux, meaning that the flux of fast neutrons in the fission neutron spectra was  $2.3 \times 10^{16}$  m<sup>-2</sup> s<sup>-1</sup>. This flux is about 20 times higher than the NPI CAS neutron flux from the p(35 MeV)-Be source.



**Figure 1.** The neutron spectra generated in the channel H9/3 of the LVR-15 reactor and in the distance of 15 mm from the thick Be target bombarded with 35 MeV protons from the U-120 cyclotron.



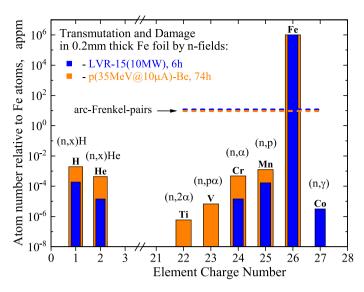
**Figure 2.** Calculated numbers of transmutants and displaced atoms (*arc*-Frenkel pairs) produced in W during irradiation in the LVR-15 reactor and p-Be source due to nuclear reactions.

The specimens were irradiated to a maximum fast neutron fluence of  $1.56 \times 10^{21}$  n/m² for W and  $5 \times 10^{20}$  n/m² for Fe, which corresponds to the displacement damage levels of  $3.7 \times 10^{-5}$  and  $3.6 \times 10^{-5}$  NRT-dpa for W and Fe, respectively. The temperature of the samples under irradiation was about 363–373 K. A comparison of the neutron spectra in the LVR-15 reactor and p(35 MeV)-Be neutron spectra is shown in Fig. 1.

The energy spectrum of neutrons in the reactor and neutrons produced by the p(35 MeV)-Be source are different. There is a significant fraction of thermal and epithermal neutrons in the reactor neutron spectrum. Thermal and epithermal neutrons do not have sufficient energy to produce a considerable concentration of vacancy-type defects. However, the thermal neutrons may cause transmutation via neutron capture reactions, whereas fast neutrons cause most of displaced atoms. Although the fraction of fast neutrons (E > 0.1 meV) in the total flux is 7.9%, this part of the spectrum contributes up to 90% of the total production of displacement damage.

We have estimated the nuclear transmutation of W and Fe into another elements for both neutron sources used in this work. For this purpose, the code FISPACT-II and JEFF-3.3 neutron data library<sup>25</sup> were used. The number of transmutants accumulated during the maximum irradiation time (6 h in the LVR-15 reactor and 74 h in the p(35 MeV)-Be source) relative to the W and Fe atoms is shown in Figs. 2 and 3, respectively. For both materials, the softer reactor neutron spectrum results in a higher concentration of high Z-elements by the  $(n,\gamma)$  reactions than the accelerator driven neutron source. In contrast, the neutrons from the p(35 MeV)-Be source produce more low-Z elements and hydrogen or helium gases than the neutrons from the LVR-15 reactor.

The total relative inventory of the solid build-up elements generated in W and Fe in the LVR-15 reactor was calculated to be  $4.1 \times 10^{-1}$  appm and  $1.8 \times 10^{-4}$  appm, respectively. Irradiation of targets with the p(35 MeV)-Be



**Figure 3.** Calculated numbers of transmutants and displaced atoms (*arc*-Frenkel pairs) produced in Fe during irradiation in the LVR-15 reactor and p-Be source due to nuclear reactions.

neutrons produces  $4.3\times10^{-4}$  appm of new solid elements in W and  $1.7\times10^{-3}$  appm in Fe. The ratio of the concentration of solid build-up generated in W and Fe irradiated by reactor neutrons, trans<sup>reactor</sup>, to the concentration formed by neutrons from the p(35 MeV)-Be source, trans<sup>p-Be</sup>, is equal to

$$trans^{reactor}/trans^{p-Be} = 4.1 \times 10^{-1}/4.3 \times 10^{-4} = 10^3$$
 (3)

in the case of W and

trans<sup>reactor</sup> / trans<sup>p-Be</sup> = 
$$1.8 \times 10^{-4} / 1.7 \times 10^{-3} = 10^{-1}$$
 (4)

in the case of Fe. The total concentration of solid build-up elements generated in W irradiated by reactor neutrons is significantly higher (about three orders of magnitude) than that in W irradiated by neutrons from the p(35 MeV)-Be source. In contrast, the concentration of solid transmutants in Fe due to the effects of reactor neutrons is lower compared to neutrons from the p(35 MeV)-Be source.

The calculated fractions of primary defects in W and Fe, i.e. Frenkel pairs of vacancies and interstitials survived in the PKA cascades are also plotted in Figs. 2 and 3. One can see that the total relative inventory of new build-up elements generated in W and Fe in the LVR-15 reactor and by wide-spectrum high energy neutrons from the p(35 MeV)-Be source is lower than the displacement damage predicted by the arc-dpa model. The ratio of the solid transmutants to the arc-Frenkel pairs reaches a maximum value of 17% in the case of W irradiation in the LVR-15 reactor due to the extremely high rate of rhenium production by thermal neutrons. Consequently, new elements produced by nuclear reactions during irradiation will have secondary impact on the radiation-induced defect evolution under current experimental conditions, such as decoration of defects or precipitation.

As it was mentioned above, the reactor flux of fast neutrons is about 20 times higher than the high-energy neutron flux from the p(35 MeV)-Be source. But there is a large fraction of high-energy neutrons in the range of 15–33 MeV in the NPI CAS neutron spectra from the p(35 MeV)-Be source. This fraction of high-energy neutrons is negligible in the fission neutron spectra (Fig. 1).

#### Results

The intrinsic and radiation-induced defects in W and Fe were studied by PALS. A digital spectrometer<sup>26</sup> with time resolution of 145 ps (FWHM  $^{22}$ Na) was employed for positron lifetime (LT) investigations. Positron source was made by deposition of 2  $\mu$ l of  $^{22}$ NaCl water solution (iThemba Labs) with activity of  $\approx$ 1.5 MBq on a 2  $\mu$ m thick Mylar foil<sup>27</sup>. The diameter of the positron source spot was  $\approx$ 1.5 mm and it was always positioned in the center of each sample measured. The details of PALS measurements can be found in Ref.<sup>14</sup>.

Results of decomposition of LT spectra are listed in Tables 1 and 2 for W and Fe samples, respectively.

Annealed non-irradiated W and Fe are characterized by single component PALS spectrum. The lifetime  $\tau_1$  of this component is  $(105\pm1)$  and  $(107\pm5)$  ps, for W and Fe, respectively (see Tables 1 and 2). These values agree well with the bulk positron lifetime for W  $^{28}$  and Fe $^{29}$ . Hence, the component with lifetime  $\tau_1$  represents a contribution of free positrons de-localized in the lattice. It means that the defect concentration in the annealed W and Fe is lower than 1 appm since virtually all positrons annihilate from the de-localized state in the lattice  $^{30-33}$ .

The PALS spectra of both W and Fe samples irradiated in the LVR-15 reactor with fission neutron spectrum to a fluence of  $2.12\times10^{21}$  n/m²  $(1.67\times10^{20}$  n/m² of fast neutrons with an energy of E>0.1 MeV) contain a new component with longer lifetime  $\tau_2$  =  $(190\pm5)$  ps for Fe and  $\tau$  =  $(244\pm3)$  ps for W (see Tables 1, 2). This component can be attributed to positrons trapped at radiation-induced defects. Comparing experimental lifetimes with

Sample	Description	τ <sub>1</sub> (ps)	I <sub>1</sub> (%)	τ <sub>2</sub> (ps)	I <sub>2</sub> (%)	C <sub>cl</sub> (appm)	N <sub>v</sub>	C <sub>v</sub> (appm)
WR	Recrystallized at 2000 K for 40 min	105(1)	100	-	-	-	-	-
WR_LVR1	$n^{0}$ -irradiated, $F = 1.66 \times 10^{20} \text{ m}^{-2}$	95(5)	86(1)	244(3)	14(1)	1.4(2)	3.1(2)	4.5(5)
WR_LVR2	$n^0$ -irradiated, $F = 2.1 \times 10^{20} \text{ m}^{-2}$	92(4)	84(1)	289(3)	16(1)	1.3(1)	5.0(2)	6.6(5)
WR_LVR3	$n^0$ -irradiated, $F = 5.1 \times 10^{20} \text{ m}^{-2}$	86(4)	74(1)	261(3)	26(1)	2.8(2)	3.8(2)	10.5(5)
WR_LVR4	n <sup>0</sup> -irradiated, F = 1.56 × 10 <sup>21</sup> m <sup>-2</sup>	70(5)	54(2)	245(5)	46(2)	7.0(5)	3.4(5)	24(1)

**Table 1.** Positron lifetimes  $\tau_i$  and relative intensities  $I_i$  of components measured by PALS in reference W samples and W samples irradiated with fission neutrons in the LVR-15 reactor at sample temperature of about 370 K. The fluence of fast neutrons (E>0.1 MeV), F, is also shown. The experimental errors expressed in units of the last significant digit are given in parentheses. The physical parameters calculated from PALS data:  $C_{cl}$  concentration of vacancy clusters,  $N_{v}$  average number of vacancies in a cluster,  $C_{v} = C_{cl} N_{v}$  total concentration of vacancies.

Sample	Description	τ <sub>1</sub> (ps)	I <sub>1</sub> (%)	τ <sub>2</sub> (ps)	I <sub>2</sub> (%)	C <sub>cl</sub> (appm)	N <sub>v</sub>	C <sub>v</sub> (appm)
Fe	Annealed at 1173 K for 1 h	107(5)	100	-	-	-	-	-
Fe_LVR1	$n^0$ -irradiated, $F = 1.66 \times 10^{20} \text{ m}^{-2}$	102(3)	90.4(5)	190(5)	9.6(5)	1.4(2)	1.4(2)	2.0(4)
Fe_LVR2	$n^{0}$ -irradiated, $F = 2.1 \times 10^{20} \text{ m}^{-2}$	98(2)	80(2)	195(4)	20(2)	2.7(1)	1.7(2)	4.6(5)
Fe_LVR3	$n^0$ -irradiated, $F = 5.1 \times 10^{20} \text{ m}^{-2}$	88(2)	68(1)	197(1)	32(1)	5.1(1)	1.8(2)	9.2(5)

**Table 2.** Positron lifetimes  $\tau_i$  and relative intensities  $I_i$  of components measured by PALS in reference Fe samples and Fe samples irradiated with fission neutrons in the LVR-15 reactor at sample temperature of about 370 K. The fluence of fast neutrons (E>0.1 MeV), F, is also shown. The physical parameters calculated from PALS data are listed in the table as well. The experimental errors expressed in units of the last significant digit are given in parentheses. Notation is the same as in Table 1.

results of ab-initio theoretical calculations  $^{32-35}$ , one can conclude that small vacancy clusters consisting on average of 1–2 and 4 vacancies were created by fission neutron irradiation in Fe and W, respectively. Dislocation-type defects were not detected neither in W nor in Fe up to the fluence of  $5 \times 10^{20}$  n/m<sup>2</sup>.

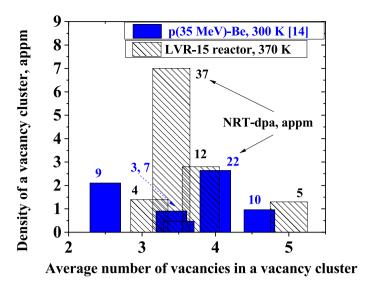
In general, the transmutation elements, resulting from the interaction of low-energy neutrons (present in the spectra of fission neutrons) with a solid, can decorate the radiation-induced defects. With a high ratio of thermal neutrons to fast neutrons, interstitial impurities as a result of transmutation can reduce the lifetime of positrons trapped in vacancy-type defects by decorating these defects<sup>36</sup>. Hence, if the concentration of transmutation products is comparable to dpa, the size of radiation-induced defects might be larger than the size obtained by comparing the experimental data with ab-initio theoretical calculations. However, for low fluences used in this study the effects of transmutation impurities are negligible since the concentration of transmutation products is substantially lower than dpa. Consequently, both fission and energetic neutron irradiations of W and Fe samples introduced predominantly small vacancy clusters. The driving force for the agglomeration of individual vacancies into vacancy clusters is a reduction of the surface energy. Agglomeration of radiation-induced vacancies is facilitated by the fact that neutron irradiation produces vacancies in cascades, i.e. located close to each other. Agglomeration of such vacancies into clusters is relatively easy, since it does not require diffusion to a long distance<sup>14</sup>.

The mean size of radiation-induced vacancy clusters in W after fission and high-energy p(35 MeV)-Be neutron irradiations is compared in Fig. 4. The NRT-dpa is indicated by labels in the figure. The temperature of samples was ~300 K and ~370 K during irradiation with neutrons from the p(35 MeV)-Be source and in the LVR-15 reactor, respectively. Thermally activated migration of vacancies in W is negligible at these temperatures<sup>2,37</sup>. Unlike low-Z materials, for example Fe, which require irradiation and subsequent measurement at cryogenic temperatures in order to neglect the impact of thermal effects on the defect recovery<sup>30</sup>, W has the advantage of high melting temperature and, therefore, migration of vacancy-type defects is insignificant even at 400 K. Since migration of interstitials occurs at significantly lower temperatures compared to vacancies, some vacancy-type defects in W were likely removed by recombination with migrating interstitials which are mobile well below room temperature.

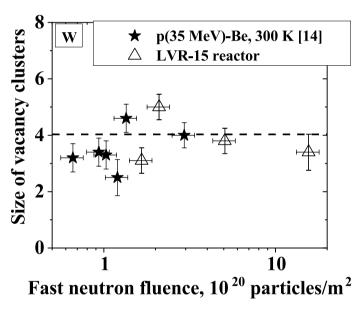
From Fig. 4, one can conclude that both fission neutrons from the LVR-15 reactor and high-energy neutrons from the p(35 MeV)-Be source create in W vacancy clusters containing on average 3–5 vacancies.

Figure 5 shows experimental data of the average size of vacancy clusters in  $\hat{W}$  induced by irradiation with neutrons from p(35 MeV)-Be source and neutrons in the LVR-15 reactor as a function of irradiation fluence. The average size of vacancy clusters for both types of irradiation is comparable up to the fluence of  $10^{21}$  n/m². This is because vacancies are immobile at the irradiation temperature 300–370 K and the fluences are too low for cascade overlap events. According to SRIM calculations, there are no cascade overlap events at such fluences  $^{14}$ . Moreover, the average size of vacancy clusters does not remarkably change with increasing fluence.

Vacancy-related defects in the Fe samples irradiated in the nuclear reactor are remarkably smaller than clusters created by p(35 MeV)-Be neutrons (Fig. 6). The density of radiation-induced defects increases with



**Figure 4.** Experimental data of the mean size of radiation-induced vacancy clusters in W and their density after irradiation in the LVR-15 reactor in comparison with high-energy p(35 MeV)-Be neutron irradiation 1<sup>14</sup> for each irradiation fluence indicated for the NRT-dpa values in appm.

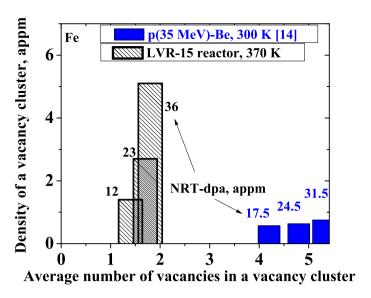


**Figure 5.** Experimental data of the mean size of vacancy clusters in W induced by irradiation with neutrons from p(35 MeV)-Be source<sup>14</sup> and neutrons in LVR-15 reactor as a function of the irradiation fluence. Dashed line is weighted average of the mean size of vacancy clusters.

increasing fluence/dpa. For Fe irradiated with fission neutrons, the mean size of vacancy clusters increases from 1–2 vacancies to 2 vacancies per cluster with NRT-dpa increasing from  $12\times10^{-6}$  to  $36\times10^{-6}$ . For Fe irradiated with high-energy neutrons from the p(35 MeV)-Be source, the mean size of vacancy clusters grows from 4 up to 5–6 vacancies per cluster with NRT-dpa increasing from  $17\times10^{-6}$  to  $31\times10^{-6}$ .

### Discussion

Cluster size after fission and high-energy neutron irradiation. As follows from PALS measurements, the irradiation of W with neutrons from both the p(35 MeV)-Be source and fission reactor creates in W small vacancy clusters of approximately the same size. Irradiation of Fe in the LVR-15 reactor creates vacancy clusters with (i) smaller size and (ii) higher concentration compared to irradiation with neutrons from the p(35 MeV)-Be source at the same dpa. In both irradiation spectra, the vacancy clusters in Fe appear to increase in the size and the density with increasing fluence. The increase in the size is evidence for vacancy flow to vacancy clusters produced in earlier stages of the irradiation.



**Figure 6.** Experimental data of the mean size of radiation-induced vacancy clusters in Fe and their density after irradiation in the LVR-15 reactor in comparison with high-energy p(35 MeV)-Be neutron irradiation <sup>14</sup> for each irradiation fluence indicated in NRT-dpa values in appm.

Note, that according to our SRIM simulations, the mean distance between displacements is in the order of 0.1  $\mu$ m even for the highest fluence used in the present work. Hence, cascades do not overlap with each other. Since vacancies are immobile in W at the irradiation temperatures and the maximum dose of  $\sim 3 \times 10^{-5}$  dpa precludes cascade overlap effects, flux (or dose rate) should not cause vacancy growth. Furthermore, flux would not have any effect on in-cascade local vacancy concentration. The present data also showed that the vacancy cluster size in W is independent of the fluence for conditions where cascade overlap can be neglected and thermally activated migration of vacancies does not occur. A similar size of vacancy clusters in W has been measured for all fluences studied.

The smaller size of radiation-induced defects in Fe with higher density after fission neutron irradiation compared to p(35 MeV)-Be neutrons can be attributed to (i) a high fraction of high-energy neutrons in the neutron spectra from the p(35 MeV)-Be source and (ii) flux effect caused by thermally activated migration of radiation-induced vacancies. High energy primary knock-on atoms (PKAs) transfer substantial kinetic energy to the host atoms, leading to displacement cascades that can be significantly greater than the defect migration enthalpies. As a consequence, both pronounced defect agglomeration and recombination during the cascade quench phase take place. In the case of Fe irradiated at room temperature, thermal effects play noticeable role in radiation-induced defect recombination and agglomeration. Migration of mono-vacancies was observed already at 220 K in electron-irradiated Fe (annealing stage III) and at 180 K in Fe irradiated with neutrons<sup>30</sup>. In our current experiments, the samples were irradiated in the temperature range of 300-373 K, which is far above the stage III. Therefore, vacancies are mobile at the temperature of irradiation. Radiation-induced vacancies that do not recombine with interstitials either disappear by diffusion to sinks at the grain boundaries and on the surface or can agglomerate into clusters that are immobile at the irradiation temperature. A migrating vacancy can be trapped in an already formed cluster increasing thereby its size. Consequently, contrary to W, in Fe samples the size of vacancy clusters increases with increasing fluence. Low flux leads to fewer number of radiation-induced vacancies created in the sample per unit time. This means that the probability that a vacancy disappears by diffusion into sinks or recombines with the interstitial is increased. This results in the formation of a smaller number of vacancy clusters with larger average size compared to high flux. As the flux increases, the concentration of point defects introduced per unit time increases as well. Because their thermal mobility remains unchanged, the probability that vacancies meet each other and form immobile cluster increases. Since these clusters are immobile at the irradiation temperature, they cannot merge with each other. As a consequence, a higher density of vacancy clusters with a smaller size is formed.

According to molecular dynamic (MD) calculations, the vacancy cluster size distribution in Fe shifts to larger size as the cascade energy increases from 10 to 50 keV $^{38}$ . The cascade energy of 10 and 50 keV corresponds to neutron energy of about 0.4 and 1 MeV, respectively. The conclusion of the MD calculations is supported by clearly separated clusters of vacancies by size for different cascade energies in the case of Fe, namely single vacancies and divacancies formed after irradiation with fission neutrons and vacancy clusters with 4–5 vacancies introduced by irradiation with a wide-spectrum of high-energy neutrons, see Fig. 6.

In the case of W, no clear effect of the cascade energy on the average vacancy size was reported in the MD calculations when the cascade energy increases from 1 to  $30~\text{keV}^{39}$ . However, the vacancy cluster fraction slightly increases as the cascade energy increases from 30 to 100~keV. The cascade energy of 30~keV and 100~keV corresponds to neutron energy of about 1 and 4 MeV, respectively. We did not observe any noticeable difference in

Type of spectrum: effective		Calculated arc-dp dpa), barn	oa (NRT-	Experim./Calcul arc-dpa	
energy	Experimental dpa, barn	ENDF/B-VIII.0 JEFF-3.3		(NRT-dpa)	
Tungsten					
U-235(n,f): 2.4 ± 1.3 MeV	121 ± 27 Guinan'82 (T < 10 K) <sup>13</sup> 156 ± 62 Klabunde'82 (T < 10 K) <sup>12</sup>	51 (184)	51 (184) 58 (221) 2.4±0.4 (		
LVR-15 reactor, 1.9 ± 1.0 MeV	205 ± 30 this work, (T ≈ 370 K)	50 (160)	53 (184)	3.9 ± 0.6 (1.11) <sup>a</sup>	
p(35 MeV)—Be: 15.7 ± 10.0 MeV	330 ± 15 <sup>14</sup> (T ≈ 300 K)	97 (371)	167 (659)	2.0 ± 0.1 (0.50) <sup>a</sup>	
D-T (RTNS-II): 14.9 ± 0.3 MeV	428 ± 97 Guinan'82 (T < 10 K) <sup>13</sup>	112 (438)	211 (877)	2.0 ± 0.2 (0.49) <sup>a</sup>	
Iron			•		
U-235(n,f): 2.4 ± 1.3 MeV	224±23 Horak'73 (T<10 K) <sup>45</sup> 264±44 Takamura'85 (T<10 K) <sup>46</sup> 260±43 Wallner'88 (T<10 K) <sup>47</sup>	262 (856)	253 (826)	1.00 ± 0.2 (0.33) <sup>b</sup>	
LVR-15 reactor, 2.2 ± 1.3 MeV	115 ± 20 this work, (T ≈ 370 K)	237 (729)	234 (714)	0.49 ± 0.08 (0.16) <sup>b</sup>	
p(35 MeV)—Be: 11.1 ± 9.5 MeV	220 ± 10 <sup>14</sup> (T ≈ 300 K)	546 (1749)	499 (1593)	0.44 ± 0.10 (0.14) <sup>b</sup>	
D-T (RTNS-II): 14.9 ± 0.3 MeV	-	797 (2543)	709 (2245)	-	

**Table 3.** Measured and calculated neutron-induced dpa cross-sections for W and Fe averaged in the neutron spectrum produced in the LVR-15 reactor and the p(35 MeV)—Be source. The calculations were performed using arc-dpa and NRT-dpa models with nuclear data from ENDF/B-VIII.0 and JEFF-3.3. The known previous measurements at cryogenic temperatures in fission reactors and with the D-T source are given for comparison. Comments: <sup>a</sup>ratio to JEFFF-3.3; <sup>b</sup>ratio to ENDF/B-VIII.0.

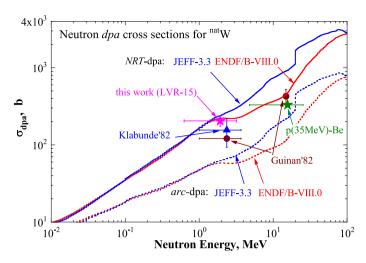
the average vacancy size between reactor neutrons and a wide-spectrum high-energy neutrons irradiations of W up to 37 appm NRT-dpa, see Figs. 4 and 5.

**Comparison with theory.** The NJOY-2016<sup>40</sup> was employed for calculation of the NRT- and arc-dpa cross sections for neutron irradiation. The code processes the evaluated cross section data and calculates the damage energy available for atom displacement from lattice site using the embedded NRT model. In order to calculate radiation damage within the arc-dpa approach, the primary defect survival function was incorporated into the NJOY-2016 code<sup>41</sup>. The primary defect survival function was constructed using available results of MD simulations<sup>21</sup>. Binary collision approximation (BCA) was used for the nuclear reaction recoil energies above 150–200 keV, where the results of MD simulations are not yet available<sup>42</sup>. Accurate cross-sections of the neutron reactions are crucial for the NRT- and arc- dpa calculations. The latest versions of the major evaluations of neutron cross-sections, namely, US Evaluated Nuclear Data File ENDF-VIII.0<sup>43</sup> and Joint Evaluated Fission and Fusion library JEFF-3.3<sup>44</sup>, were used in the present work. Table 3 shows the neutron-induced NRT-dpa and arc-dpa cross-sections for W and Fe calculated from the full nuclear reaction data.

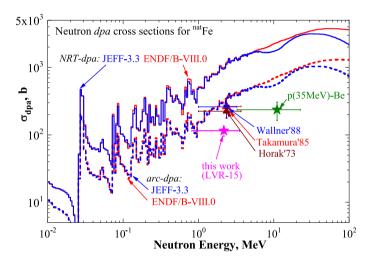
In Table 3 the theoretical cross-sections are compared with experimental values determined from PALS measurements by dividing the total concentration of vacancies,  $c_v$ , by the irradiation fluence. From inspection of the Table 3, one can conclude that the arc-dpa equals  $\approx 1/3$  of the NRT-dpa in the energy range of practical interest. In order to compare the calculated quantities with the neutron-induced cross-sections determined experimentally in the present work as well as in the available literature using fission reactors<sup>12,13,45-47</sup> and D-T generator<sup>13</sup>, the theoretical NRT- and arc-dpa cross-sections were folded with the neutron spectra of the corresponding facilities. It has to be mentioned that in contrast to Fe, the cross section calculated for W using nuclear data libraries ENDF/B-VIII.0 and JEFF-3.3 differs roughly in two times.

The calculated and experimental NRT- and arc-dpa neutron irradiation cross-sections are compared in Figs. 7 and 8 for W and Fe, respectively.

For W irradiated with fission neutrons, the experimental data are better described by the NRT-dpa model than the arc-dpa model. The measured dpa cross-section of high-energy neutrons from the p(35 MeV)-Be source in the case of  $W^{14}$  is in a reasonable agreement with either the NRT-dpa model using neutron reaction data from ENDF/B-VIII.0 library, or with the arc-dpa prediction using neutron reaction data from JEFF-3.3 library (Fig. 7). Considering also the experimental data from the available literature 12,13, one can conclude that the experimental neutron-induced cross-sections for W are straddling between the two models confirming the conclusion reported in Ref.<sup>14</sup>. Measured values for defect production efficiency in W may be underestimated because of self-interstitial defects, which are created as well as vacancies and are mobile already below room temperature. At low irradiation temperatures and low initial sink density, the recombination induced by the diffusion of interstitials is responsible for the density of vacancy-type of defects. Migrating interstitials may recombine with immobile vacancies or be trapped in a vacancy cluster, thus, reducing its size. Increasing the fluence, interstitials first find the sinks, which leads to a decrease in their concentration and a corresponding increase in the net vacancy concentration as observed experimentally. Therefore, because of migrating self-interstitial defects the discrepancy between measured and calculated dpa for W may be greater than indicated in Table 3. The general trend of radiation-induced defect recovery agrees well for both neutron and electron irradiations, especially with regard to a significant recovery stage below 25 K. The recovery of the electrical resistivity of W following low temperature electron irradiation was reported to be ~ 50-70% defect recovery after annealing



**Figure 7.** Experimental neutron-induced cross-sections for W measured in the present work after irradiation in the LVR-15 reactor at  $T \approx 370$  K and neutrons from the p(35 MeV)-Be source at  $T \approx 300$  K reported in Ref. <sup>14</sup>, as well as those that are known from the literature at T < 10 K, namely, Kladunde'82<sup>12</sup> and Guinan'82<sup>13</sup> (symbols with error bars). Calculated neutron-induced NRT-dpa (solid lines) and arc-dpa (dashed lines) cross sections for W using neutron reaction data from ENDF/B-VIII.0 and JEFF-3.3 are also shown for comparison.



**Figure 8.** Experimental neutron-induced cross-sections for Fe measured in the present work after irradiation in the LVR-15 reactor at  $T \approx 370$  K and neutrons from the p(35 MeV)-Be source at  $T \approx 300$  K reported in Ref.<sup>14</sup>, as well as those that are known from the literature at T < 10 K, namely, Horak'73<sup>45</sup>, Takamura'85<sup>46</sup>, and Wallner'88<sup>47</sup> (symbols with error bars). Calculated neutron-induced NRT-dpa (solid lines) and arc-dpa (dashed lines) cross sections for Fe using neutron reaction data from ENDF/B-VIII.0 and JEFF-3.3 are also shown for comparison.

through Stage I (up to 100 K)<sup>48,49</sup>. About 50% of initial radiation damage in thermal neutron-irradiated W after cryogenic irradiation was recovered by 300 K as reported in Ref.<sup>50</sup>. In the current study, no big difference between radiation-induced defect density in W irradiated at 300 K (determined by positron annihilation spectroscopy techniques) and prior defect production studies at 10 K (used electrical resistivity techniques) is observed. This can be due to various methods of measurements, various purity of W, irradiation conditions (damage rate versus annealing time), transmutation effects, etc. One possible reason may be that dissolved impurity atoms presented in our samples could suppress the radiation-induced defect recovery<sup>51</sup>.

Figure 8 shows the neutron-induced cross-sections determined experimentally in the present work for Fe irradiated with fission neutrons in the LVR-15 reactor at  $T \approx 370$  K. The data known from the literature are plotted in the figure as well. The experimental data of fission neutron irradiation of Fe at  $T < 10 \text{ K}^{45-47}$  are in a good agreement with the calculated spectrum averaged arc-dpa cross sections. In our previous publication<sup>14</sup>, the fast reactor spectrum averaged arc-dpa for Fe, measured by Horak and Blewitt<sup>45</sup>, was derived from the overview table published by P. Jung<sup>52</sup>. It resulted in the value of 136 barn, which is lower by a factor of two than other reactor measurement<sup>46,47</sup>. In contrast to this, the dpa value measured by the electrical resistivity change in Ref.<sup>45</sup> is 224 barn. Now, we use this value since it corresponds to the original author' data and well agrees with other reactor measurements<sup>46,47</sup>.

The arc-dpa model is in a good agreement with most of the experimental data at low irradiation temperatures of T < 10 K. It indicates that annealing of the hot recoils in cascade of collisions in Fe is the dominating factor of the recovery of primary radiation-induced defects. This proves the validity of the arc-dpa cross section calculated using the primary defect surviving function based on the results of the state-of-art MD simulations.

The cross-section of fission neutrons in the LVR-15 reactor measured in this work for Fe is lower than the arc-dpa prediction, similar to the data for neutrons from the p(35 MeV)-Be source. This is due to the thermal annealing of defects. Thermally activated recovery of defects in Fe that occurs already at ambient temperature reduces the radiation damage predicted by the arc-dpa model by a factor of about two. The concentration of radiation-induced defects is significantly reduced due to recombination effects occurring at the subsequent stages of annealing: I (below  $0.1 T_m$ )—recombination of close Frenkel pairs associated with self-interstitial atom motion, II—recombination of remote Frenkel pairs ( $T \approx 0.15 T_m$ ), III—migration of mono-vacancies into sinks and their agglomeration into clusters ( $T \approx 0.15-0.2 T_m$ ), where  $T_m$  is the melting temperature<sup>2,30,37,53-56</sup>. Therefore, not only athermal vacancy-interstitial recombination considered in the arc-dpa model, but also thermally activated diffusion of point defects to sinks contributes to a significant recovery of radiation-induced vacancies and interstitials<sup>2,20,30,45-47</sup>.

## **Conclusions**

We initiated a study of the effect of different neutron spectra on the cluster size of primary radiation-induced defects in bcc Fe and W. PALS technique has been applied to study the size and concentration of vacancy-type radiation-induced defects and to explore the validity of the damage models for fission neutron spectra and a wide range high energy neutron spectra.

With irradiation up to the fluence of about  $1 \times 10^{21}$  n/m², dislocation-type defects produced by irradiation were not detected neither in W nor in Fe, only vacancy-type defects were detected. It was found that irradiation of W with neutrons produced in a nuclear reactor and with high-energy neutrons from a p(35 MeV)-Be generator leads to the formation of radiation-induced vacancy clusters with comparable mean size of  $\approx 4$  vacancies.

Fe samples irradiated with neutrons from the p(35 MeV)-Be source contained vacancy clusters with a larger size and lower density compared to the samples irradiated with fission neutrons. One reason for this is higher flux in the case of fission neutron irradiation that leads to a higher density of vacancy clusters with a smaller size. The second reason for the larger clusters of vacancies with lower concentrations formed during high-energy neutron irradiation is the higher energy of PKAs in the neutron spectra of the p(35 MeV)-Be source compared to fission neutrons. High energy PKAs transfer substantial kinetic energy to the host atoms, resulting in an energetic displacement cascade. This enhances both defect agglomeration and recombination during the cascade quenching phase. As a consequence, the actual damage of samples may be less than expected from the NRT-dpa model. This is consistent with the concept of the athermal recombination corrected (arc-dpa) model. Moreover, thermally activated diffusion of defects even at 300 K leads to defect recombination, which significantly (by a factor of about two) reduces the concentration of radiation-induced defects predicted by the arc-dpa model. Thus, different neutron spectra and different fluxes can lead to different cluster sizes of radiation-induced defects, despite the same dpa. The sample temperature has a stronger effect on radiation-induced defect size than the irradiation fluence. Different cluster sizes, which are not taken into account in the dpa models, can invariably contribute to changes in the microstructure and, consequently, the physical properties of irradiated materials. This means that the physics of primary radiation effects in materials is still not fully known and requires further study through a combination of modeling and experimental efforts. The present data serve as a basis for developing an improved concept of the displacement process.

# Methods

- 1. Sample preparation Cold-rolled W foils with a thickness of 100  $\mu$ m and purity of 99.97% produced by Plansee and ARMCO type Fe foils with a thickness of 200  $\mu$ m and purity of 99.8% produced by Goodfellow were mechanically polished to mirror-like state. Then W foils were recrystallized at 2000 K for 40 min in ultrahigh vacuum with a base pressure lower than  $2\times10^{-9}$  mBar. The Fe foils were annealed at 1173 K for 1 h in vacuum with a base pressure of  $1\times10^{-6}$  mBar. In the case of Fe, such heat treatment allows us to minimize the density of defects but persist  $\alpha$ -phase of bcc Fe.
- 2. Irradiation with wide-spectrum high energy neutrons Wide-spectrum high energy neutron irradiation was carried out at the source of fast neutrons with continuous neutron spectra up to 35 MeV generated by a p(35 MeV) beam incident on a thick Be target at the U-120M cyclotron of Nuclear Physics Institute (NPI CAS) in Řež. The detailed description is given in Ref.<sup>22</sup>. The neutron flux was  $10^{15}$  n/m<sup>2</sup>s. The neutron irradiation was carried out at room temperature. The neutron fluence on the foils was  $0.4 \times 10^{20}$ ,  $1.0 \times 10^{20}$ ,  $1.4 \times 10^{20}$ , and  $1.8 \times 10^{20}$  n/m<sup>2</sup>.
- 3. Irradiations with fission neutrons Irradiation with fission neutrons has been performed in the channels of H9/3 of the LVR-15 research reactor of the Research Centre Řež. The detailed description is given in Ref. The neutron spectrum in the irradiation position was calculated by the neutron transport code MCNP6.1 using the current fuel rods distribution. The neutron flux was estimated to be  $\sim 2.9 \times 10^{17}$  m<sup>-2</sup> s<sup>-1</sup>. The fraction of fast neutrons with energies of E > 0.1 MeV was calculated as 7.9% of the total neutron flux, meaning that the flux of fast neutrons in the fission neutron spectra was  $2.3 \times 10^{16}$  m<sup>-2</sup> s<sup>-1</sup>. The temperature of the samples under irradiation was about 363-373 K. The fluence of fast neutrons on the foils was  $1.67 \times 10^{20}$ ,  $2.1 \times 10^{20}$ ,  $5.1 \times 10^{20}$  n/m², and  $1.56 \times 10^{21}$  n/m².
- 4. Defect characterization Positron annihilation lifetime spectroscopy (PALS) measurements and a computer simulation of PALS spectra were used for intrinsic and radiation-induced defects investigation. A digital

spectrometer with time resolution of 145 ps (FWHM  $^{22}Na)$  was employed for positron lifetime (LT) investigations. Positron source was made by deposition of 2 µl of  $^{22}NaCl$  water solution (iThemba Labs) with activity of  $\approx 1.5$  MBq on a 2 µm thick Mylar foil. The diameter of the positron source spot was  $\approx 1.5$  mm and it was always positioned in the center of each sample measured. At least  $10^7$  positron annihilation events were accumulated in LT spectra which were decomposed using a maximum likelihood based procedure. The source contribution consisted of two weak components which come from positrons annihilated in the source spot and the covering Mylar foil and exhibit lifetimes of  $\sim 368$  ps and  $\sim 1.5$  ns. Corresponding intensities of the source contribution components were  $\sim 6\%$  and  $\sim 1\%$  for Fe and  $\sim 10\%$  and  $\sim 1.7\%$  for W, respectively. The details of these PALS measurements can be found in Refs.  $^{26,27}$ .

- 5. *Nuclear transmutation calculations* The nuclear transmutation of W and Fe into another elements was calculated using the code FISPACT-II and JEFF-3.3 neutron data library.
- 6. The neutron induced NRT- and arc-dpa cross sections were calculated by the NJOY-2016 code using the evaluated neutron reaction data from the latest versions of the main evaluations ENDF-VIII.0 and JEFF-3.3. The lattice displacement energy E<sub>d</sub> was selected to be 40 eV for Fe and 90 eV for W. The primary defects (Frenkel pairs) survival function which impact on arc-dpa was taken for Fe and W from the Primary Radiation Group of the Organisation for Economic Co-operation and Development (OECD)<sup>21</sup> by fitting to the selected molecular dynamic (MD) simulations. Above the PKA energies of 150–200 keV, where the results of MD simulations are not presently available, the combination of the MD and binary collision approximation (BCA) calculations was used to compute defect survival efficiency. The displacement cross sections files are available on: https://www-nds.iaea.org/CRPdpa/, https://www.oecd-nea.org/dbdata/JEFF33/.

# Data availability

The authors declare that all data supporting the findings of this study are available from the authors on request.

Received: 7 March 2019; Accepted: 23 September 2020 Published online: 03 November 2020

#### References

- 1. Roth, J. et al. Recent analysis of key plasma wall interactions issues for ITER. J. Nucl. Mater. 390-391, 1-9 (2009).
- Ogorodnikova, O. V. & Sugiyama, K. Effect of radiation-induced damage on deuterium retention in tungsten, tungsten coatings and Eurofer. J. Nucl. Mater 442, 518–527 (2013).
- 3. Baluc, N. et al. Status of reduced activation ferritic/martensitic steel development. J. Nucl. Mater. 367-370, 33-41 (2007).
- 4. Hishinuma, A. *et al.* Current status and future R&D for reduced-activation ferritic/martensitic steels. *J. Nucl. Mater.* **258–263**, 193–204 (1998).
- Ueda, Y., Tobita, K. & Katoh, Y. PSI issues at plasma facing surfaces of blankets in fusion reactors. J. Nucl. Mater. 313–316, 32–41 (2003).
- Ogorodnikova, O. V., Raepsaet, X. & Futterer, M. A. Tritium permeation through the first wall of the EU-HCPB blanket. Fus. Eng. Des. 49-50, 921-926 (2000).
- Ogorodnikova, O. V. & Gann, V. Simulation of neutron-induced damage in tungsten by irradiation with energetic self-ions. J. Nucl. Mater. 460, 60–71 (2015).
- 8. Hatano, Y. et al. Deuterium trapping at defects created with neutron and ion irradiations in tungsten. Nucl. Fusion 53, 073006 (2013).
- 9. Zinkle, S. J. & Snead, L. L. Opportunities and limitations for ion beams in radiation effects studies: Bridging critical gaps between charged particle and neutron irradiations. Scr. Mater. 143, 154–160 (2018).
- 10. Jung, P. & Lucki, G. Damage production by fast electrons in dilute alloys of vanadium, niobium and molybdenum. *Radiat. Effects* **26**, 99–103 (1975).
- 11. Coltman, R. R., Klabunde, C. E. & Williams, J. M. Rates of defect production by fission neutrons in metals at 4.7 K. J. Nucl. Mater. 99, 284–293 (1981).
- 12. Klabunde, C. E. & Coltman, R. R. Fission neutron damage rates and efficiencies in several metals. *J. Nucl. Mater.* **108–109**, 183–193 (1982).
- 13. Guinan, M. W. & Kinney, J. H. Resistivity damage rates in fusion-neutron irradiated metals at 4.2 K. *J. Nucl. Mater.* **108–109**, 95–103 (1982).
- Ogorodnikova, O. V. et al. Verification of the theory of primary radiation damage by comparison with experimental data. J. Nucl. Mater 525, 22–31 (2019).
- 15. Eldrup, M., Li, M., Snead, L. L. & Zinkle, S. J. Characterization of defect accumulation in neutron-irradiated Mo by positron annihilation spectroscopy. *Nucl. Instrum. Methods Phys. Res. Sect. B* 266, 3602–3606 (2008).
- Norgett, M. J., Robinson, M. T. & Torrens, I. M. A proposed method of calculating displacement fluence rates. *Nucl. Eng. Des.* 33, 50–54 (1975).
- 17. Robinson, M. T. Basic physics of radiation damage production. J. Nucl. Mater. 216, 1–28 (1994).
- Standard Practice for Neutron Radiation Damage Simulation by Charge-Particle Irradiation, E521-96, Annual Book of ASTM Standards, vol. 12.02, American Society for Testing and Materials, Philadelphia, 1996. Reapproved 2009.
- 19. Averback, R. S., Benedek, R. & Merkle, K. L. Ion irradiation studies of the damage function of copper and silver. *Phys. Rev. B* 18, 4156–4171 (1978).
- 20. Zinkle, S. J. & Singh, B. N. Analysis of displacement damage and defect production under cascade damage conditions. *J. Nucl. Mater.* **199**, 173–191 (1993).
- Nordlund, K. et al. Improving atomic displacement and replacement calculations with physically realistic damage models. Nat. Commun. 9, 1084 (2018).
- 22. Stefanik, M. et al. High-flux white neutron source based on p(35)-Be reactions for activation experiments at NPI. Radiat. Phys. Chem. 104, 306–309 (2014).
- 23. https://cvrez.cz/en/infrastructure/research-reactor-lvr-15/ (2020)
- 24. Goorley, J. T., et al., 'Initial MCNP6 Release Overview—MCNP6 version 1.0', Los Alamos National Laboratory report LA-UR-13-22934 (2013).
- 25. Fleming, M., Stainer, T., Gilbert, M. (eds) The FISPACT-II User Manual. Report UKAEA-R(18)001 (2018).

- Bečvář, F., Čížek, J., Procházka, I. & Janotová, J. The asset of ultra-fast digitizers for positron-lifetime spectroscopy. Nucl. Instrum. Method. Phys. Res. A 539, 372–385 (2005).
- 27. Bečvář, F. et al. A high-resolution BaF2 positron-lifetime spectrometer and experience with its long-term exploitation. Nucl. Instrum. Method Phys. Res. A 443, 557–577 (2000).
- 28. Ziegler, R. & Schaefer, H. E. Vacancy formation in molybdenum and tungsten investigated by positron lifetime measurements. *Mater. Sci. Forum* **15–18**, 145–148 (1987).
- 29. Čížek, J., Procházka, I., Kočík, J. & Keilová, E. Positron-lifetime study of reactor pressure vessel steels. *Phys. Status Solidi A* 178, 651–661 (2000).
- 30. Vehanen, A., Hautojärvi, P., Johansson, J., Yli-Kaupilla, J. & Moser, P. Vacancies and carbon impurities in  $\alpha$  iron: Electron irradiation. *Phys. Rev. B* 25, 762–780 (1982).
- 31. Puska, M. J., Sob, M., Brauer, G., Korhonen, T. Positron annihilation characteristics in perfect and imperfect transition metal carbides and nitrides. *J. Phys. IV France* **05**, C1-135–C1-142 (1995).
- 32. Troev, T., Popov, E., Staikov, P., Nankov, N. & Yoshiie, T. Positron simulations of defects in tungsten containing hydrogen and helium. *Nucl. Instrum. Method. Phys. Res. B* 267, 535–541 (2009).
- 33. Staikov, P. & Djourelov, N. Simulations of <1 0 0> edge and ½ <1 1 1> screw dislocations in α-iron and tungsten and positron lifetime calculations. *Phys. B* **413**, 59–63 (2013).
- 34. Puska, M. J. & Nieminen, R. M. Defect spectroscopy with positrons: A general calculation method. *J. Phys. F Met. Phys.* 13, 333–346 (1983)
- Kuramoto, E., Tsutsumi, T., Ueno, K., Ohmura, M. & Kamimura, Y. Positron lifetime calculations on vacancy clusters and dislocations in Ni and Fe. Comput. Mater. Sci. 14, 28–35 (1999).
- 36. Hautojärvi, P., Johansson, J., Vehanen, A., Yli-Kauppila, J. & Moser, P. Vacancy-carbon interaction in iron. *Phys. Rev. Lett.* 44, 1326–1329 (1980).
- 37. Keys, L. K. & Moteff, J. Neutron irradiation and defect recovery of tungsten. J. Nucl. Mater. 34, 260-280 (1970).
- 38. Stoller, R. E. J. Nucl. Mater. 276, 22-32 (2000).
- 39. Setyawan, W. et al. J. Nucl. Mater. 462, 329-337 (2015).
- 40. Kahler, A.C. (ed.) The NJOY Nuclear Data Processing System, Version 2016", Report LA-UR-17-20093, Los Alamos National Lab (2018).
- 41. Simakov, S. P., Fischer, U., Koning, A. J., Konobeyev, AYu. & Rochman, D. A. Iron NRT- and arc-displacement cross sections and their covariances. *Nucl. Mater. Energy* 15, 244–248 (2018).
- Konobeyev, A. Y., Fischer, U., Korovin, Y. A., Simakov, S. P., IOTA-2017. A code for the simulation of ion transport in materials. KIT Scientific Working Papers No. 63, Karlsruhe (2017).
- 43. Brown, D. A. et al. ENDF/B-VIII.0: 'The 8th major release of the nuclear reaction data library with CIELO-project cross sections, new standards and thermal scattering data. Nucl. Data Sheets 148, 1–142 (2018).
- 44. Plompen, A.J.M., Cabellos, O., De Saint Jean, C. et al. The joint evaluated fission and fusion nuclear data library. Eur. Phys. J. A 56, 181 (2020). https://www.oecd-nea.org/dbdata/jeff/jeff33/index.html.
- 45. Horak, J. A. & Blewitt, T. M. Isochronal recovery of fast neutron irradiated metals. J. Nucl. Mater. 49, 161-180 (1973).
- 46. Takamura, S., Aruba, T. & Nakato, K. Fission-neutron displacement cross sections in metals. J. Nucl. Mater. 136, 159-163 (1985).
- 47. Wallner, G. et al. Defect production rates in metals by reactor neutron irradiation at 4.6 K. J. Nucl. Mater. 152, 146-153 (1988).
- 48. Coltman, R. R., Klabunde, C. E. & Redman, J. K. Survey of thermal-neutron damage in pure metals. Phys. Rev. 156, 715-734 (1967).
- 49. Vajda, P. Anisotropy of electron radiation damage in metal crystals. Rev. Mod. Phys. 49, 481–521 (1977)
- 50. Maury, F., Biget, M., Vajda, P., Lucasson, A. & Lucasson, P. Frenkel pair creation and stage I recovery in W crystals irradiated near threshold. *Radiat. Effects* 38, 53–65 (1978).
- 51. Faber, K. In Proc. Ill Intern. Symp. Reinststoffe in Hisseneohaft and Teahnik, Dresden (1970).
- 52. Jung, P. Atomic displacement functions of cubic metals. J. Nucl. Mater. 117, 70-77 (1983).
- 53. van Bueren, H. Z. Metallkunde 46, 272 (1955).
- 54. Zinkle, S. J. & Snead, L. L. Ann. Rev. Mater. Res. 44, 241 (2014).
- 55. Ogorodnikova, O. V., Ciupiński, L., Grzonka, J., Gasparyan, Yu. & Efimov, V. Annealing of radiation-induced damage in tungsten under and after irradiation with 20 MeV self-ions. *J. Nucl. Mater.* **451**, 379–386 (2014).
- Ogorodnikova, O. V. et al. Annealing of radiation-induced defects in tungsten: positron annihilation spectroscopy study. J. Nucl. Mater. 517, 148–151 (2019).

### Acknowledgements

We are grateful to V. Efimov for annealing of W samples. Thermal annealing of Fe samples was performed in MGML (www.mgml.eu), which is supported within the program of Czech Research Infrastructures (project no. LM2018096). Irradiations were carried out at the infrastructure of the NPI CAS Řež and CVŘ through the projects LM2015056 and LM2015074 (Ministry of Education, Youth and Sports of the Czech Republic). Support by the Technology Agency of the Czech Republic (project TK01030153) is highly appreciated.

# **Author contributions**

O.V.O. proposed the high-energy proton and neutron irradiation experiments and the PALS method of defect investigation, performed sample preparation and drafted the manuscript, M.M. designed and coordinated the irradiations, performed calculations of transmutation productions using the code FISPACT-II, J.K. prepared and supervised the irradiation in the LVR-15 reactor, M.S. conducted neutron irradiations, V.V.G. provided critical interpretation, J.C. coordinated the PALS measurements and performed PALS data evaluation and interpretation, P.H. provided assistance in the PALS measurements, S.S. performed theoretical calculations, J.P. performed thermal annealing of the Fe foils, M.V. performed characterization of the neutron spectrum with MCNP6.1 simulation. All authors contributed in the data analysis, discussion and the final manuscript preparation.

#### Competing interests

The authors declare no competing interests.

# Additional information

Correspondence and requests for materials should be addressed to O.V.O.

Reprints and permissions information is available at www.nature.com/reprints.

**Publisher's note** Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.

Open Access This article is licensed under a Creative Commons Attribution 4.0 International License, which permits use, sharing, adaptation, distribution and reproduction in any medium or format, as long as you give appropriate credit to the original author(s) and the source, provide a link to the Creative Commons licence, and indicate if changes were made. The images or other third party material in this article are included in the article's Creative Commons licence, unless indicated otherwise in a credit line to the material. If material is not included in the article's Creative Commons licence and your intended use is not permitted by statutory regulation or exceeds the permitted use, you will need to obtain permission directly from the copyright holder. To view a copy of this licence, visit <a href="http://creativecommons.org/licenses/by/4.0/">http://creativecommons.org/licenses/by/4.0/</a>.

© The Author(s) 2020