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OPEN Fractionation of carbon and hydrogen isotopes of TSR-altered gas products under closed system pyrolysis

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Thermochemical sulfate reduction (TSR) is common in marine carbonate gas reservoirs, leading to complicated isotope characteristics of TSR-altered gas. This study aims to better understand how TSR affects the geochemical and isotopic compositions of alkanes in pyrolysis products. Pyrolysis of TSR were conducted with crude oil, nonane (C_{o}) and methylnaphthalene (MN) in the presence of MqSO₄ solution at temperatures of 350 °C, 360 °C, and 370 °C for different durations of 4–219 h in a closed system. Results show that carbon and hydrogen isotope compositions of alkane gas resulting from TSR (pyrolysis with crude oil and MgSO₄) became heavier with increasing carbon number, i.e., $\delta^{13}C_1 < \delta^{13}C_2 < \delta^{13}C_3$ and $\delta^2H - C_1 < \delta^2H - C_2 < \delta^2H - C_3$. Compared with the $\delta^{13}C_1$, $\delta^{13}C_2$ and $\delta^{13}C_3$ increased in a much wider range as heating continued. Carbon and hydrogen isotopes of alkane gas produced by TSR became heavier with increasing gas souring index. Values for $\delta^{13}C_1 - \delta^{13}C_2$ and $\delta^2H - C_1 - \delta^2H - C_2$ typically decreased as oil and Co underwent thermal cracking. Comparative experiments using Co in the presence of MqSO₄ produced partially reversed carbon isotope series ($\delta^{13}C_1 > \delta^{13}C_3$), which, for the first time, confirmed the ability of TSR to cause isotopic reversal from pyrolysis. The residual heavy alkanes gradually became ¹³C-enriched during TSR, which increased δ^{13} C, values and changed the partially reversed isotope sequence to a positive sequence ($\delta^{13}C_1 < \delta^{13}C_2$). The discovery of a partial reversal of the carbon isotope series of alkane gases through pyrolysis will further deepen the understanding of TSR-altered natural gas.

 H_2S is a harmful gas usually generated in deep marine carbonate gas reservoirs¹⁻⁶, which poses significant challenges for the safe production of natural gas. High concentrations of H₂S in gas reservoirs are mainly produced by thermochemical sulfate reduction (TSR)^{1,7-11}, during which sulfate is reduced by organic matters and/or hydrocarbons to H₂S and CO₂. In general, hydrocarbons with higher carbon number will react more readily with sulfate¹²⁻¹⁴. The reaction equations can be expressed as follows:

> $SO_4^{2-} + CH_4 \rightarrow CO_3^{2-} + H_2S + 2H_2O$ $3SO_4^{2-} + 4C_2H_6 \rightarrow CO_3^{2-} + 3H_2S + 4CH_4 + CO_2 + H_2O_3$ $3SO_4^{2-} + 2C_3H_8 \rightarrow 3CO_3^{2-} + 3H_2S + 2CH_4 + CO_2 + H_2O_3$ $3SO_4^{2-} + 4C_4H_{10} + H_2O \rightarrow 5CO_3^{2-} + 5H_2S + 8CH_4 + 3CO_2$

The effect of TSR has been studied extensively by characterising natural gas components, stable isotopes such as carbon, hydrogen, and sulfur, as well as inclusions and sulfur-bearing minerals^{9,15-30}. Cai et al.^{23,24} concluded

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that CH₄ can be oxidised when the dryness coefficient is greater than 0.97 and presented fractionation equations for TSR in the presence of methane and ethane^{27, 28}. Machel et al.⁴ proposed an initiation temperature of 100-140 °C for TSR, and Worden et al.³¹ thought that the initiation temperature for TSR was 140 °C. Amrani et al.²⁹ and Meshoulam et al.³²systematically investigated the isotopic composition of sulfur compounds during TSR and proposed that the composition of sulfur isotopes may reflect the degree of TSR. Hao et al.¹, Liu et al.^{20,21} and Cai et al.²⁷ characterised geochemical properties of marine gas in the Sichuan Basin, China, and found that heavy hydrocarbons were preferentially involved in the TSR reaction compared with CH₄, which can increase the dryness coefficient of natural gas. TSR was also found to gradually cause partial carbon isotope reversal of the positive alkane gas series²⁰. Liu et al.²¹ discovered that hydrogen isotope fractionation for CH₄ generated by TSR via hydrogen isotope exchange between water and hydrocarbons was greater than that for CH4 directly generated from kerogen. Although a carbon isotope fractionation model for alkane gas in H₂S-bearing gas reservoirs, such as the commonly observed pattern of the carbon isotope series of CH_4 and C_2H_6 that changes from positive to reversed and then back to positive^{1, 20, 33}, has been established, the hydrogen isotope fractionation of alkane gas has not been explored by laboratory pyrolysis. Liu et al.³⁴ proposed that the rock salt and/or brine may play an important role for the occurrence of TSR based on the formation mechanism of H₂S-enriched gas reservoirs in the Sichuan Basin, China. Cross et al.³⁵ reported, based on laboratory simulations, that temperature was the key factor for the occurrence of TSR, whereas pressure had a minor impact. Pan et al.¹² conducted a hightemperature, long-time, step-by-step thermal cracking simulation with organic matter and Fe₂O₃, MgSO₄, and a mixture of both. They found that CH_4 was produced by TSR in the presence of heavy hydrocarbons and that isotope fractionation became more pronounced with increasing carbon number. Based on a thermal cracking simulation, Zhang et al.^{36,37} proposed that the initiation temperature for TSR was affected by the chemical composition of crude oil, and low molar ratios of water and $MgSO_4$ were favorable to the reaction. $MgSO_4$ affects pH, which in turn increases the concentration of the active sulfate species $HSO_4^{-38,39}$. TSR eventually oxidised CH_4 into carbon dioxide¹⁹⁻²¹. Zhao et al.⁴⁰ experimentally simulated the TSR reaction with crude oil, bitumen, and different kinds of kerogen under presence of anhydrite and MgSO₄, and found that TSR preferentially modified low molecular hydrocarbons, and type III kerogen was least reactive during the TSR process.

However, most of these laboratory simulations of TSR have focused on the chemical composition, and carbon isotope composition of the pyrolysis^{12, 36–41}. The effects of oil cracking and TSR on the hydrogen isotopic composition of alkane gas have rarely been studied⁴². In addition, participation of water in the reaction and involvement of hydrogen from other sources, e.g. water, can result in a hydrogen isotope fractionation of alkane gas that may differ from its carbon isotope fractionation²¹.

In this paper, crude oil, nonane (C_9H_{20} , C_9), and methylnaphthalene ($C_{11}H_{10}$, MN) were used to simulate TSR alteration at different thermal stages. The chemical and carbon isotopic composition of gaseous products from thermal cracking and TSR of crude oil were analysed to elucidate the impact of TSR. In addition, this is the first study that considered the impact of the presence of water during TSR alteration on the hydrogen isotope fractionation of alkane gas. Therefore, the effects of thermal cracking and TSR on the fractionation of carbon and hydrogen isotopes of alkane gas were studied to explore the isotopic evolution of carbon and hydrogen caused by TSR, aiming to provide experimental evidence to better understand the isotopic composition and variation of gases in H₂S-bearing reservoirs.

Methods

Samples. Crude oil sample used in the simulation experiments were collected from the TK772 well within the Ordovician Yingshan Formation $(O_{1-2}y)$ in the No.7 District of the Tahe Oilfield, Tarim Basin, western China, at a depth of 5,557.5–5,591.5 m. The content of saturated hydrocarbons, aromatic hydrocarbons, non-hydrocarbons, asphaltene, and sulfur of the crude oil were measured as 25.28%, 28.66%, 12.23%, 17.26%, and 2.46%, respectively, with a carbon isotope composition of – 32.8‰ (the hydrogen isotopic composition was not measured). The purities of C₉ (C₉H₂₀, nonane) and MN (C₁₁H₁₀, methylnaphthalene) were 99.99%. The reaction reagents and experimental buffer in this paper were manufactured by the Aladdin Reagent Shanghai Co., Ltd.

Experimental procedures and product analyses. It has been reported that the most suitable temperature for TSR of crude oil in a closed system is approximately 360 °C and that heating time and pH are important factors affecting the occurrence of TSR^{10,36}. To simulate the evolution of reaction products during thermal cracking and TSR, as well as the change in isotopic composition caused by TSR, crude oil samples were heated at a temperature of 360 °C for 4, 10, 24, 40, 72, and 219 h. For each condition, the experiment was conducted with crude oil only, and a mixture of crude oil, buffer and MgSO4. In the pyrolysis system, we added a mixed salt solution (including 5.61 g MgCl₂, 10.01 g NaCl and 100 ml distilled water, 350 mg solution per gold capsule) to the gold capsule. A mixture of silica and talc (1:1, about 60 mg per gold capsule) was used as a buffer to maintain a relatively stable pH of approximately 3-5. To determine the effects of temperature on TSR, experiments were also conducted using a solution of crude oil, buffer, and MgSO₄ at temperatures of 350 °C and 370 °C. For each experiment, about 10 mg of crude oil, MgSO₄ solution, and buffer were combined in a gold capsule (60 mm in length, 6 mm in diameter) under argon gas. The gold capsules were placed in different autoclaves that were connected to each other. The pressure of the experimental system was maintained at 50 MPa to simulate the conditions under which most TSR occurs. After the reaction temperature was increased from room temperature (18 °C) to 200 °C at a rate of 20 °C/h, it was kept constant at 200 °C for half an hour to stabilise the system temperature. The temperature was then increased to the target temperature at a rate of 20 °C/h, and held constant for the pre-set reaction time. The gold capsules were then taken out of the autoclaves and quenched. Fluctuations of temperature and pressure in the autoclaves were 0.5 °C and 1 MPa, respectively. To compare and analyse the

	n No	Time (h)	Easy-Ro (%)	Yield of main products (ml/g)							Chemical composition of main products (%)						C1/		
Reaction condition				CH4	C2H6	C ₃ H ₈	C4H10	C5H12	H ₂	CO ₂	H ₂ S	CH4	C ₂ H ₆	C ₃ H ₈	C4H10	C5H12	CO ₂	H ₂ S	C ₁₋₅ (%)
360 °C oil	M-8	4	0.80	1	0.36	0.23	0.08	0.01	0.06	0.75	-	39.84	14.31	9.11	3.25	0.49	29.83	n.d	59.46
	M-9	10	0.90	3.53	1.45	1.05	0.46	0.1	0.23	0.98	-	45.1	18.53	13.39	5.92	1.29	12.52	n.d	53.54
	M-10	24	1.00	8.2	3.47	2.52	1.18	0.3	0.25	1.39	-	47.33	20.02	14.54	6.8	1.71	8	n.d	52.36
	M-11	40	1.10	14.47	6.27	4.86	2.71	0.93	0.28	1.92	-	46.01	19.92	15.44	8.62	2.95	6.1	n.d	49.51
	M-12	72	1.19	24.06	10.08	7.66	4.25	1.52	0.3	1.99	0.22	48.02	20.12	15.28	8.48	3.04	3.97	0.43	50.58
	M-13	219	1.40	38.09	16.07	13.14	8.27	3.59	0.5	2.51	1.08	45.75	19.3	15.79	9.93	4.31	3.01	1.29	48.12
360 °C oil+MgSO4+buffer	M-15	4	0.80	9.94	2.76	2.1	0.94	0.29	0.23	41.38	47.92	9.41	2.61	1.99	0.89	0.28	39.19	45.38	61.99
	M-16	10	0.90	27.75	6.41	2.5	0.74	0.2	0.17	35.24	131.95	13.54	3.13	1.22	0.36	0.1	17.19	64.38	73.79
	M-17	24	1.00	34.71	4.04	0.3	0.1	0.03	0.14	112.59	308.11	7.55	0.88	0.07	0.02	0.01	24.47	66.98	88.51
	M-18	40	1.10	38.17	1.54	0.08	0.02	-	0.15	135.34	357.66	7.16	0.29	0.02	n.d	n.d	25.39	67.11	95.85
	M-19	72	1.19	40.52	0.18	0.01	-	-	0.12	179.99	378.63	6.76	0.03	n.d	n.d	n.d	30.03	63.16	99.56
	M-20	219	1.40	34.32	0.03	-	-	-	0.14	190.38	307.6	6.44	0.01	n.d	n.d	n.d	35.75	57.77	99.84
350 °C oil + MgSO ₄ + buffer	M-31	7.5	0.80	0.99	0.26	0.17	0.07	0.04	0.05	15.02	2.33	5.23	1.37	0.88	0.37	0.21	79.3	12.32	64.89
	M-32	19.5	0.90	9.03	1.83	1.11	0.33	0.09	0.09	29.67	47.46	10.08	2.05	1.24	0.37	0.1	33.11	52.96	72.83
	M-33	42	1.00	23.91	6.52	2.75	0.59	0.08	0.1	158.03	420.05	3.91	1.06	0.45	0.1	0.01	25.82	68.63	70.71
	M-34	79.5	1.10	35.35	7.23	3.11	0.43	0.02	0.08	193.52	487.53	4.86	0.99	0.43	0.06	n.d	26.61	67.03	76.66
	M-35	172	1.23	37.04	2.89	0.08	0.03	-	0.07	201.12	546.65	4.7	0.37	0.01	n.d	n.d	25.53	69.38	92.52
360 °C oil + MgSO ₄ + buffer	M-36	4	0.80	1.05	0.28	0.16	0.05	0.01	0.07	11.69	0.31	7.71	2.05	1.2	0.37	0.08	85.68	2.29	67.57
	M-37	10	0.90	7.21	1.38	0.79	0.2	0.05	0.16	20.22	32.07	11.61	2.22	1.27	0.32	0.08	32.57	51.66	74.90
	M-38	24	1.00	26.31	5.52	2.47	0.57	0.09	0.2	188.31	373.92	4.4	0.92	0.41	0.1	0.02	31.52	62.59	75.21
	M-39	40	1.10	37.19	7.8	2.41	0.55	0.09	0.16	246.62	512.89	4.6	0.97	0.3	0.07	0.01	30.53	63.5	77.31
	M-40	72	1.19	42.29	4.6	0.14	0.03	-	0.06	277.72	626.79	4.44	0.48	0.01	n.d	n.d	29.18	65.86	90.06
370 °C oil + MgSO ₄ + buffer	M-41	2	0.80	1.21	0.32	0.21	0.05	0.02	0.13	21	2.01	4.86	1.29	0.86	0.22	0.07	83.98	8.05	66.58
	M-42	5.5	0.90	9.58	1.76	1.09	0.31	0.09	0.24	34.98	60.66	8.81	1.62	1	0.29	0.08	32.17	55.79	74.66
	M-43	11	1.00	26.52	5.16	1.7	0.47	0.12	0.16	57.31	239.09	8.02	1.56	0.52	0.14	0.04	17.34	72.33	78.02
	M-44	21	1.10	45.5	8.6	1.75	0.27	-	0.09	298.86	619.37	4.67	0.88	0.18	0.03	n.d	30.67	63.56	81.08
	M-45	44	1.23	48.71	4.49	0.05	-	-	0.04	336.84	656.69	4.65	0.43	n.d	n.d	n.d	32.18	62.73	91.54
360 °C C ₉ + MgSO ₄ + buffer	M-46	4	0.80	0.06	0.04	0.03	-	-	-	9.21	0.07	0.63	0.47	0.29	0.06	0.02	97.64	0.78	42.86
	M-47	10	0.90	1.13	0.41	0.25	0.07	0.02	0.12	10.32	1.71	8.02	2.9	1.79	0.54	0.13	73.48	12.16	59.94
	M-48	24	1.00	30.49	8.54	5.09	2.22	0.46	0.31	183.24	311.71	5.62	1.58	0.94	0.41	0.09	33.8	57.5	65.05
	M-49	40	1.10	70.2	22.99	9.18	3.45	1.07	0.35	374.65	666.62	6.11	2	0.8	0.3	0.09	32.62	58.04	65.70
	M-50	72	1.19	73.5	25.78	11.4	4.86	1.73	2.27	485.42	781.79	5.3	1.86	0.82	0.35	0.12	35	56.37	62.72
360 °C MN+MgSO ₄ +buffer	M-51	10	0.90	0.03	0.01	0.01	-	-	-	5.43	-	0.49	0.13	0.09	n.d	n.d	99.29	n.d	69.01
	M-52	24	1.00	0.02	0.01	-	-	-	-	2.8	-	0.58	0.19	0.12	n.d	n.d	99.11	n.d	65.17
	M-53	40	1.10	0.06	0.01	0.01	-	-	-	12.53	-	0.44	0.08	0.05	n.d	n.d	99.43	n.d	77.19
	M-54	72	1.19	0.06	0.01	-	-	-	-	8.46	1.66	0.57	0.07	0.03	n.d	n.d	83.04	16.29	85.07
	M-55	219	1.40	0.33	0.01	-	-	-	-	74.67	29.66	0.31	0.01	n.d	n.d	n.d	71.33	28.34	96.88

Table 1. Yields and chemical compositions of main products of the thermal cracking simulation experiments.

effects of TSR, experiments were also conducted on nonane (C_9) and methylnaphthalene (MN) at 360 °C following the same procedures. The amount of C_9 and MN added in the experiments were both about 10 mg.

The chemical compositions of gas products were analysed using an Agilent 6890 N gas chromatograph equipped with a PoraPLOT Q column (30 mm $\times 0.25$ mm $\times 0.25$ µm). Helium was used as the carrier gas. The oven temperature was programmed as follows: an initial temperature of 50 °C for 2 min, raised to 180 °C at the rate of 4 °C/min, and held constant at 180 °C for 15 min. Deviation between replicate analyses was less than 1%. The stable carbon isotopic composition was analysed with an Isochrom II GC-IRMS isotope ratio mass spectrometer equipped with a PoraPLOT Q column. Helium was used as the carrier gas. The oven temperature program was started at 50 °C, held for 3 min, raised to 150 °C at a rate of 15 °C/min, and held at 150 °C for 8 min. Each sample was analysed twice with a deviation between the analyses of less than 0.3‰. Stable hydrogen isotope analyses were conducted with a Finningan Delta^{Plus} XL isotope ratio mass spectrometer equipped with a Dim-type column. The oven temperature was programmed as follows: an initial temperature of 40 °C held for 8 min, raised to 110 °C at a rate of 3 °C/min, then held at 110 °C for 2 min. Each analysis was conducted twice, with a deviation between the analysis are listed in Tables 1 and 2.

Results

Yields of reaction products under different conditions. The yields of all gaseous alkanes produced from thermal cracking of crude oil at 360 °C increased with longer heating time, with CH_4 exhibited the highest yields of 1.00–8.09 ml/g. The yields of H_2S , CO_2 and H_2 also increased with increasing reaction time, but no H_2S was detected in the first 40 h (Table 1). During thermal cracking of a mixture of crude oil, MgSO₄, and buffer

			δ ¹³ C (%	o, VPDB)	δ ² H (‰, VSMOW)			
Reaction condition	No	Time (h)	CO ₂	CH ₄	C ₂ H ₆	C ₃ H ₈	CH ₄	C ₂ H ₆	C ₃ H ₈
	M-9	10	n.d	- 55.8	- 37.2	- 35.6	-272	- 203	-173
	M-10	24	- 22.6	-51.3	- 35.9	- 34.5	-274	-204	-174
360 °C oil	M-11	40	-25.6	-51.5	- 36.9	- 35.5	-277	-202	-181
	M-12	72	-24.4	-49.1	- 35.7	- 34.7	-278	-209	-184
	M-13	219	-28.5	-48.4	- 36.8	- 35.2	-262	- 207	-173
	M-32	19.5	- 20.7	- 42.7	- 35.9	- 33.5	-237	- 169	-141
250 °C ail MacO , huffer	M-33	42	-23.4	-40.9	- 33.6	-29.8	-232	-159	- 126
550° C $611 + MgSO_4 + buller$	M-34	79.5	-24.6	- 39.2	-31.3	-24.9	-242	-140	-129
	M-35	172	-25.0	- 37.0	-21.2	n.d	-216	-101	n.d
	M-37	10	- 15.7	-41.3	- 34.3	- 33.1	-226	-174	-136
260.86 -1 - M. 60 - 1 - 6-	M-38	24	-23.1	- 36.9	- 32.9	- 30.4	-227	-153	-114
360 °C oii + MgSO ₄ + burner	M-39	40	-25.1	- 36.7	-31.8	-26.5	-224	-134	-105
	M-40	72	-25.6	- 36.3	-23.7	n.d	-214	-102	n.d
	M-42	5.5	- 19.0	- 38.8	- 34.1	- 32.8	-228	- 173	-130
270 °C - 1 - M-CO - 1 - 6-	M-43	11	-22.9	- 38.1	- 33.6	-31.8	-231	-153	-112
$3/0^{\circ}$ C oii + MgSO ₄ + burner	M-44	21	-25.0	- 35.0	- 29.8	-23.4	-216	-122	-102
	M-45	44	-25.8	-33.7	-21.8	n.d	- 199	-106	n.d
	M-46	4	-2.1	n.d	n.d	n.d	n.d	n.d	n.d
	M-47	10	-10.5	n.d	n.d	n.d	n.d	n.d	n.d
360 °C C_9 + MgSO ₄ + buffer	M-48	24	-23.3	-29.2	- 31.6	- 30.1	-216	-184	-158
	M-49	40	-24.8	-29.3	-28.5	- 26.9	-213	-152	-139
	M-50	72	- 25.8	- 29.1	-27.6	-26.2	-211	-132	-123
	M-51	10	- 2.5	n.d	n.d	n.d	n.d	n.d	n.d
	M-52	24	-5.7	n.d	n.d	n.d	n.d	n.d	n.d
360 °C MN + MgSO ₄ + buffer	M-53	40	-7.7	n.d	n.d	n.d	n.d	n.d	n.d
	M-54	72	-11.8	n.d	n.d	n.d	n.d	n.d	n.d
	M-55	219	-17.5	n.d	n.d	n.d	n.d	n.d	n.d

Table 2. Carbon and hydrogen isotope compositions of the products of the thermal cracking simulationexperiments. Note: n.d. no detection.

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at 360 °C (M15–M20), yields of CH_4 and C_2H_6 increased at first and then decreased as the reaction continued. The yield of CH_4 was in the range of 9.94–40.52 ml/g. The yields of C_3H_8 , C_4H_{10} , and other heavy gaseous hydrocarbon products gradually decreased with longer heating time. The yield of H_2S increased at first and then decreased in the range of 47.92–378.63 ml/g. The CO_2 yield increased from 41.38 to 190.38 ml/g with time. The yield of H_2 decreased from 0.23 to 0.12 ml/g (Table 1) with increasing heating time. These results suggest that the presence of sulfate significantly increased the yields of H_2S and CO_2 .

Compositions of main reaction products under different conditions. During thermal cracking of crude oil at 360 °C, the relative content of alkane gases generally increased with longer heating time, while some decreased as the heating time was increased to 219 h (Table 1). The relative content of CH_4 in the gaseous reaction products ranged from 39.84 to 48.02%, while that of CO_2 exhibited a decreasing trend with increasing heating time. Only trace amounts of H_2S were detected after a heating time of 72 h and 219 h (Table 1). Similarly, it was found that during thermal cracking of a mixture of crude oil, MgSO₄, and buffer at 360 °C (M15–M20), the relative content of CH_4 and C_2H_6 first increased and then decreased as the reaction continued. The relative content of CH_4 varied between 6.44% and 13.54%. Concentration of heavy hydrocarbon gases, including C_3H_8 and C_4H_{10} , decreased with longer heating time. The relative content of H_2S and CO_2 produced from thermal cracking of crude oil increased because of TSR. Thermal cracking (M46–M55) of C_9 and MN in the presence of sulfate also produced high amounts of CO_2 and low amounts of alkane gases (Table 1). To facilitate a comparison with other research and gas geochemical characteristics under actual geological conditions, we modelled the Easy%Ro (Table 1).

Isotopic composition of main reaction products produced under different conditions. Carbon and hydrogen isotopic compositions gaseous reaction products resulting from thermal cracking of various hydrocarbons under a range of experimental conditions are summarised in Table 2 above.



Figure 1. Variations of the yield of major products from thermal cracking of crude oil only (light blue line) and those in the presence of $MgSO_4$ (red line) at the temperature of 360 °C: CH_4 (**a**), H_2 (**b**), CO_2 (**c**), and H_2S (**d**).



Figure 2. The plot of CH_4/CO_2 versus $(CO_2 + H_2S)/(CO_2 + H_2S + \Sigma C_{1-5})$ during thermal cracking of crude oil and TSR.

Discussion

Yields and relative contents of TRS reaction products. Yield of CH₄, CO₂, and H₂S from direct thermal cracking of crude oil are significantly lower than those resulting from cracking of a crude oil and $MgSO_4$ solution under similar experimental conditions (Table 1). Increased yields of gaseous products might be attributed to the involvement of sulfur in the reaction, which may also trigger TSR^{37,38}, converting heavier hydrocarbons into CH₄, CO₂, and H₂S¹². Since the activity energy for alteration of hydrocarbons TSR is lower than that for thermal cracking³⁸, gas yields from the crude oil and MgSO₄ solution is higher than those for thermal cracking of crude oil alone under the same pyrolysis conditions (temperature and time). Compared to the increase of CH_4 yield during thermal cracking of crude oil, the CH_4 yield during thermal cracking of crude oil and $MgSO_4$ rapidly increased in the first 72 h at 360 °C, and then slightly decreased (Fig. 1a), which may be related to the oxidation of methane to H_2S and CO_2 during $TSR^{12,27}$. The H_2 yield from thermal cracking of crude oil gradually increased with time up to 219 h, but the H_2 yield from crude oil and MgSO₄ decreased from 0.23 ml/g to 0.15 ml/g until 72 h, and remained almost constant at less than 0.15 ml/g as the reaction continued (Fig. 1b). This observation suggests that TSR may have a very limited effect on H_2 formation during pyrolysis. During the reaction of crude oil and MgSO₄, the yield of H_2S and CO₂ increased rapidly before until 72 h (Fig. 1c, d), after which the CO₂ yield remained almost constant as the H₂S yield decreased slightly. Because the presence of a $MgSO_4$ solution introduces sulfur and oxygen into the pyrolysis system, the yield of H_2S and CO_2 increased^{12,37}. After 72 h, the yield of CH_4 and H_2S slightly decreased (Fig. 1a, d), indicating that the TSR process consumed



Figure 3. The plot of reaction time versus $\delta^{13}C_{CO2}$ of gaseous products from simulation experiments of different mixtures at various temperatures.

these components to some extent and led to the production of CO_2 and sulfur^{27,40,43}. The dryness coefficient (C_1 / C_{1-5}) of the gas formed by thermal cracking of crude oil is low, while the dryness coefficient of gas formed during pyrolysis with TSR is higher, accompanied by an increased CH₄ content (Table 1), which further indicates that oxidation of heavy hydrocarbons by TSR will generate CH₄^{12,40,43}.

Because the source gas of CO₂ and H₂S is produced during the TSR process, the ratios of CH₄/CO₂ and $(CO_2 + H_2S)/(CO_2 + H_2S + \Sigma C_{1-5})$ were used to investigate variations of the chemical composition of gas altered by TSR. As shown in Fig. 2, ratios of $(CO_2 + H_2S)/(CO_2 + H_2S + \Sigma C_{1-5})$ sharply decrease with increasing CH₄/CO₂ ratios. The ratio of CH₄/CO₂ for crude oil, C₉, and MN with MgSO₄ is less than 1.0, while the ratio of CH₄/CO₂ for thermal cracking of crude oil, the same ratios for C₉ and MN with MgSO₄ are less than 1.0, and the ratio of $(CO_2 + H_2S)/(CO_2 + H_2S + \Sigma C_{1-5})$ for crude oil, the same ratios for C₉ and MN with MgSO₄ are less than 1.0, and the ratio of $(CO_2 + H_2S)/(CO_2 + H_2S + \Sigma C_{1-5})$ decreases as the CH₄/CO₂ ratio increases. Compared to the wide range of ratios for pyrolysis of crude oil and MgSO₄, the ratio of CH₄/CO₂ and $(CO_2 + H_2S)/(CO_2 + H_2S + \Sigma C_{1-5})$ for C₉ or MN with MgSO₄ shows a smaller range (Fig. 2b). These variations of CH₄/CO₂ and $(CO_2 + H_2S)/(CO_2 + H_2S + \Sigma C_{1-5})$ for crude oil and different degrees of TSR alteration during pyrolysis are similar to those caused by thermal cracking and TSR alteration of natural gas in gas reservoirs^{1, 20,21}. Thermal cracking of crude oil produced more CH₄, while TSR increased the yield of CO₂ and H₂S. The content of CH₄ in alkane gas further increased with increased thermal cracking. In contrast, the CO₂ and H₂S contents varied at different stages of TSR. Based on the properties of H₂S-bearing natural gas and previous simulation results^{1,6,12,23,40}, variations in gas produced by TSR pyrolysis are similar to those of H₂S-bearing natural gas and previous simulation results^{1,6,12,23,40}, variations in gas produced by TSR.

Fractionation characteristics of carbon and hydrogen isotopes during TSR. The carbon isotopic composition of produced CO₂ from crude oil, C₉, and MN with MgSO₄ at different temperature is negatively correlated with heating time. The $\delta^{13}C_{CO2}$ value gradually decreased from -2.1% (C₉, 360 °C, 4 h) to -28.5% (crude oil, 360 °C, 219 h) (Table 2, Fig. 3). The carbon isotopic composition of CO₂ from crude oil, C₉, and MN with MgSO₄ became significantly lighter over time until about 20 h heating time. After that, the $\delta^{13}C_{CO2}$ value for crude oil and C₉ with MgSO₄ remained mostly constant, which is similar to what happens during thermal cracking of crude oil. The decrease of $\delta^{13}C_{CO2}$ values during the first 20 h can be attributed to a greater fractionation of carbon isotopes at the onset of TSR¹². After 20 h, the carbon isotope fractionation gradually reached a balance between CO₂ and CH₄. Although the $\delta^{13}C_{CO2}$ value for CO₂ produced from MN with MgSO₄ decreased with heating time, CO₂ was relatively more enriched in ¹³C when compared to crude oil, C₉, and MgSO₄. In addition to having a heavy carbon isotopic composition, MN was also the most easily oxidised component during TSR. Due to the addition of MgSO₄ to MN, MN was quickly oxidised by TSR and converted to gas with CO₂ as the main component. Concentrations of heavy hydrocarbon gases were below the detection limit of the instruments. In summary, the transformation of crude oil, C₉, and MN by TSR converts ¹²C-rich hydrocarbons to ¹²C-enriched CO₂, which might be converted to ¹²C-rich calcite and precipitated in gas reservoirs^{9,21}.

The δ^{13} C value of gas produced from crude oil, C₉, and MN with MgSO₄ at different temperature and heating times is shown in Fig. 4. With increasing carbon numbers, the carbon isotopes of alkane gas from thermal cracking of crude oil at a pyrolysis temperature of 360 °C became heavier in the order of δ^{13} C₁ < δ^{13} C₂ < δ^{13} C₃.

The $\delta^{13}C_1$ values gradually increased over a relatively large range, while both $\delta^{13}C_2$ and $\delta^{13}C_3$ increased in a more narrow range as heating time increased (Fig. 4a). The carbon isotopic composition of alkane gas produced from crude oil and MN with MgSO₄ also became heavier with increasing carbon number in the order of $\delta^{13}C_1 < \delta^{13}C_2 < \delta^{13}C_3$. However, at the same temperature, with the addition of MgSO₄ solution, $\delta^{13}C_1$ gradually increased in a relatively narrow range, while both $\delta^{13}C_2$ and $\delta^{13}C_3$ showed larger increase as the reaction proceeded (Fig. 4b–d). It is obvious that the $\delta^{13}C_1$ of alkane gas produced in the presence of a MgSO₄ solution is higher than that produced during comparative experiments without MgSO₄. In a single thermal system, the $\delta^{13}C_1$ of alkane gas from thermal cracking of crude oil gradually becomes higher with increasing carbon number, and is linearly correlated with the reciprocal of the carbon number (1/n)⁴⁴. The reduction in the variation of $\delta^{13}C_1$



Figure 4. The δ^{13} C values of products from simulation experiments with crude oil at 360 °C (**a**), a mixture of crude oil and MgSO₄ at temperatures of 350 °C (**b**), 360 °C (**c**), 370 °C (**d**), and a mixture of C₉ and MgSO₄ at 360 °C (**e**).

values produced by TSR alteration indicates that these hydrocarbons are rapidly oxidised to CH_4 with a $\delta^{13}C_1$ value similar to the source material. The TSR process leads to a ^{13}C increase in CH_4 , producing a carbon isotopic composition more similar to that of crude oil (-32.8%). In contrast, CO_2 becomes gradually enriched in ^{12}C due to equilibrium fractionation of carbon isotopes between CO_2 and CH_4 . Overall, the variation of $\delta^{13}C_1$ is significantly smaller in the presence of MgSO₄, during TSR of crude oil, similar to that of H_2 S-bearing alkane gas in the Sichuan Basin, where natural gas shows a heavy carbon isotopic composition of CH_4^{20} . The carbon isotope composition of CO_2 formed in the presence of TSR is lighter than that formed in the absence of TSR, because TSR will oxidise a large portion of the hydrocarbons, leading to more intense $\delta^{13}C_{CO2}$ fractionation. Therefore, $\delta^{13}C_{CO2}$ values related to crude oil cracking are relatively heavier, while $\delta^{13}C_{CO2}$ will be relatively enriched in ^{12}C during pyrolysis (with TSR) in the presence of a MgSO₄ solution (Table 2).

Our experiments show for the first time that the carbon isotopic composition of gas produced from C_9 with MgSO₄ became partially reversed to $\delta^{13}C_1 > \delta^{13}C_2 < \delta^{13}C_3$ after a heating time of 24 h. The CH₄ produced from C_9 with MgSO₄ shows an extremely small variation in $\delta^{13}C_1$ values. The variation of $\delta^{13}C_2$ became larger than that of $\delta^{13}C_3$ with longer reaction time (Fig. 4e). This partial reversal of the carbon isotope series of alkane gas is similar to that of H₂S-bearing alkane gas in the Sichuan Basin, Ordos Basin, and other locations^{1,1,6,23}. Therefore, it is likely that the partial reversal of the carbon isotope series of alkane gas reservoirs happens when light hydrocarbons are altered by TSR. The isotopic composition of reaction products of pyrolysis with MN could not be detected due to the low content of alkane gases.

Figure 5 shows the variation of δ^2 H–C_n in alkane gases produced from crude oil at 360 °C, from a mix of crude oil and MgSO₄ at 350, 360, and 370 °C, as well as from a mix of C₉ and MgSO₄ at 360 °C. Similar to the δ^{13} C values, the hydrogen isotopic composition of alkane products from crude oil and a mixture of crude oil and MgSO₄ became heavier with increasing carbon number under all conditions, i.e. δ^2 H–C₁ < δ^2 H–C₂ < δ^2 H–C₃. The δ^2 H–C₁ values gradually increased in a relatively large range, and both δ^2 H–C₂ and δ^2 H–C₃ increased in a narrower range as heating time increased (Fig. 5a). The δ^2 H–C₁ value for a mix of crude oil and MgSO₄ gradually increased over time, but in a relatively small range for each temperature. The δ^2 H–C₂ and δ^2 H–C₃ values also



Figure 5. The δ^2 H–C_n of gaseous products from simulation experiments with crude oil at 360 °C (**a**), a mixture of crude oil and MgSO₄ at the temperature 350 °C (**b**), 360 °C (**c**), and 370 °C (**d**), as well as a mixture of C₉ and MgSO₄ at 360 °C (**e**).

increased with heating time, but in a much larger range compared with that of $\delta^2 H-C_1$ (Fig. 5b–d). The variation of $\delta^2 H-C_2$ is slightly larger than that of $\delta^2 H-C_3$. The $\delta^2 H-C_1$ values remained almost constant during the TSR alteration of C₉, while the $\delta^2 H-C_2$ values show much larger variations. The $\delta^2 H-C_3$ show the largest variations, but a reversed trend of the hydrogen isotopic composition of alkane gas was not observed during pyrolysis (Fig. 5e). These results indicate that the TSR can reduce the variation of $\delta^2 H-C_1$, possibly due to the similar hydrogen isotopic composition of the reaction product (C₁ gas) and that of the precursor and/or the involvement of hydrogen derived from water²¹. The $\delta^2 H-C_n$ fractionation could not be accurately calculated because of a lack of the hydrogen isotopic composition of H₂ and H₂S. However, TSR of crude oil in the presence of MgSO₄ greatly reduced the variation of $\delta^2 H-C_1$, which is consistent with the characteristics of H₂S-bearing alkane gas in the reservoirs of the Sichuan Basin, China⁴⁵. In general, hydrogen isotope fractionation during pyrolysis system may be more complicated than fractionation of carbon isotopes, because hydrogen contributes both to formation of alkane gas and H₂, while also providing hydrogen during pyrolysis²¹.

These results suggest that TSR can alter both the carbon and hydrogen isotopic composition of gaseous alkane products, and even lead to a reversed trend of the carbon isotope series of CH_4 and C_2H_6 for a mix of C_9 and MgSO₄ as the source material. This can result in similar isotopic compositions to those of H₂S-bearing natural gas⁴⁵. Liu et al.²⁰ investigated carbonate gas systems in the Sichuan Basin of China and found different amounts of acid gases (CO₂ and H₂S) in all marine strata. Both positive carbon isotope series and partially reversed sequence of alkanes were found. The positive carbon isotope series formed during production of sour gases was caused by TSR alteration that preferentially reacted with ¹²C-bearing heavy hydrocarbons. Therefore, the carbon isotope sequence was again converted to be positive series.

In this study, we found that the TSR process played a significant role in the pyrolysis of C_9 and MN with a MgSO₄ solution, which lead to production of mainly H₂S and CO₂. TSR is more sensitive to MN, which makes it possible that MN can be completely oxidised into CO₂ and H₂S (Table 1). The smallest variation of both carbon and hydrogen isotopic compositions was observed for CH₄, and was closest to that of the precursor. The heavier carbon isotopic composition of the precursor and C₂H₆ produced from thermal cracking initially led to a reversed







Figure 7. The plot of $H_2S/(H_2S + \Sigma C_{1-5})$ versus $\delta^{13}C_{CO2}$ of simulation products.



Figure 8. The plot of $H_2S/(H_2S + \Sigma C_{1-5})$ versus $\delta^{13}C_1(\mathbf{a})$, $\delta^{13}C_2(\mathbf{b})$, $\delta^{13}C_3(\mathbf{c})$, $\delta^{13}C_1 - \delta^{13}C_2(\mathbf{d})$ of alkane gas products from simulation experiments under different conditions.



Figure 9. The plot of $H_2S/(H_2S + \Sigma C_{1-5})$ versus $\delta^2H - C_1(\mathbf{a})$, $\delta^2H - C_2(\mathbf{b})$, $\delta^2H - C_3(\mathbf{c})$ and $\delta^2H - C_1 - \delta^2H - C_2(\mathbf{d})$ of alkane gas products from simulation experiments under different conditions.



Figure 10. The plot of $\delta^{13}C_1 - \delta^{13}C_2$ versus $\delta^2H - C_1 - \delta^2H - C_2$ of alkane gas products from simulation experiments under different conditions.

carbon isotope series of the alkane gas (Table 2, M-48). However, the temperature of our experiments (360 °C) was much higher than that in natural geological environments. Therefore, heavy hydrocarbons enriched in ¹²C tended to become unstable, and were subject to thermal cracking, which led to isotope fractionation. ¹³C was enriched in the residual heavy hydrocarbons, and the effect of fractionation was larger than that for CH_4 during TSR, changing the carbon isotope sequence back to positive.

Gas souring index (GSI) and carbon and hydrogen isotope fractionation of alkane gas. Because H_2S can be produced during TSR, the gas souring index (GSI), i.e., $H_2S/(H_2S + \Sigma C_{1-5})$, has been used as an indicator for the occurrence and degree of TSR⁴⁶. The variation of the GSI at different stages of TSR can be established by statistical analysis of H_2S -bearing natural gas samples⁴⁵. To reproduce the variation of molecular and isotopic compositions of H_2S -bearing natural gas during TSR, the GSI and carbon and hydrogen isotope fractionation mechanism of alkane gas were studied during pyrolysis at different temperatures with various heating times.

During thermal cracking of crude oil, a very small amount of H_2S with minor CO_2 was produced, indicating that no TSR occurred during direct thermal cracking of crude oil. In contrast, the CO_2 yield gradually increased with a larger GSI (>0.6) for TSR involving a mixture of crude oil and MgSO₄ solution, and increased rapidly with further increasing GSI (Fig. 6), which is similar to the relationship between GSI and CO_2 content of H_2S -bearing natural gas²⁰. The $\delta^{13}C_{CO2}$ values remained nearly constant but gradually decreased with increasing GSI during thermal cracking due to the presence of TSR (Fig. 7). This phenomenon can be attributed to TSR,



Figure 11. The plot of $\delta^{13}C_1$ versus $\delta^{13}C_2$ (**a**), $\delta^{13}C_2$ and $\delta^{13}C_3$ (**b**) and $\delta^{13}C_1$ and $\delta^{13}C_{CO2}$ (**c**) of alkane gas products from simulation experiments under different conditions.



 δ^{2} H-C₁ (‰)



which preferentially incorporates ¹²C from hydrocarbons into CO₂ leading to ¹²C-enrichment with increasing TSR intensity⁴⁴.

Figure 8 shows the relationship between the gas souring index and $\delta^{13}C_1$, $\delta^{13}C_2$, and $\delta^{13}C_3$. The direct thermal cracking of crude oil produced only a small amount of H₂S due to low sulfur content of the crude oil, resulting in a GSI of less than 0.1. The GSI significantly increased with the addition of $MgSO_4$ solution to the crude oil to above 0.6 under different conditions. Meanwhile, the carbon isotopic composition of alkane gas became larger with increasing TSR intensity, i.e., longer reaction time (Fig. 8). The carbon isotopic composition of the alkane gas revealed that the $\delta^{13}C_1$ variation of CH₄ produced in the presence of MgSO₄ was much lower than that of C_2H_6 . The carbon isotope composition changed more significantly with the increasing GSI and longer heating time. Therefore, during TSR, the variation of $\delta^{13}C_1$ became smaller, compared with that of $\delta^{13}C_2$ and $\delta^{13}C_3$. The $\delta^{13}C_1 - \delta^{13}C_2$ difference became higher with increasing GSI, which is completely different from that of natural gas formed by direct thermal cracking of crude oil. During thermal cracking of crude oil, the carbon isotope composition of gaseous products gradually becomes more similar with increasing carbon number⁴⁵.

The δ^2 H-C_n values of alkane gas show a variation similar to the δ^{13} C_n values, with increasing GSI during the TSR process. The range of δ^2 H–C₁ values is fairly low, while that of δ^2 H–C₂ is higher, especially for the TSR of C_9 whose $\delta^2 H - C_1$ remained almost constant (Fig. 9). Similar to the carbon isotopic composition, the δ^2 H–C₁– δ^2 H–C₂ difference increased as the gas souring index became larger, indicating that TSR can lower δ^2 H–C₁ values and increase those of δ^2 H–C₂, producing an abnormal hydrogen isotope composition of alkane gas, which is only characteristic of thermal cracking of crude oil. Both $\delta^{13}C_1 - \delta^{13}C_2$ and $\delta^2H - C_1 - \delta^2H - C_2$ became lower with increasing TSR intensity. However, in the case of oil cracking, $\delta^{13}C_1 - \delta^{13}C_2$ and $\delta^2H - C_1 - \delta^2H - C_2$ show the opposite trend with increasing TSR (Fig. 10). This observation may be caused by the small variation of the



Figure 13. The plot of $\delta^{13}C_1$ versus δ^2H-C_1 of alkane gas products from simulation experiments under different conditions.

 $\delta^{13}C_1$ and δ^2H-C_1 produced by TSR, which is similar to the isotopic composition of the precursor. The carbon and hydrogen isotopic composition of C_2H_6 was more heavily affected by the thermal cracking than oxidisation by TSR. Therefore, the variation of its carbon and hydrogen isotope compositions is higher. In addition, the difference in the carbon and hydrogen isotopic composition between CH₄ and C_2H_6 gradually increased with a larger GSI.

Although TSR alteration decreased the variation of both carbon and hydrogen isotope compositions of CH₄, as compared with products from direct thermal cracking of crude oil, $\delta^{13}C_2$ became larger with increasing $\delta^{13}C_1$. The $\delta^{13}C_2$ versus $\delta^{13}C_1$ plot (Fig. 11a), and $\delta^{13}C_2$ versus $\delta^{13}C_3$ plot (Fig. 11b), showed positive correlations, with the latter having a higher correlation. The $\delta^{13}C_1$ and $\delta^{13}C_{CO2}$ values are negatively correlated (Fig. 11c), possibly because the carbon isotopic composition of CO₂ produced by TSR is enriched in ¹²C³⁴. For CH₄, C₂H₆, and C₃H₈, δ^2 H–C₁ and δ^2 H–C₂ are positively correlated with temperature and heating time. δ^2 H–C₂ values increase with increasing δ^2 H–C₁ values. The positive correlation between δ^2 H–C₂ and δ^2 H–C₃ is even more significant (Fig. 12). Based on these results, it can be concluded that the oxidation of hydrocarbons by TSR is accompanied by thermal cracking of crude oil, resulting in distinct patterns among the δ^2 H values of alkane gases. Although TSR effect can lead to smaller variations of carbon and hydrogen isotope compositions of CH₄ compared with C₂H₆ and C₃H₈, δ^2 H–C₁ values increased with increasing $\delta^{13}C_1$ values (Fig. 13), suggesting that direct thermal cracking of crude oil also produced CH₄. However, the CH₄ produced during pyrolysis of C₉ should be primarily produced by TSR.

All TSR simulation experiments of crude oil, C_9 and MN under different conditions suggest that the TSR alteration produces CH_4 with similar carbon and hydrogen isotopic compositions to those of its precursor and reduced variations of isotopic compositions. The difference between CH_4 and C_2H_6 in carbon isotope and hydrogen isotopic composition increases with increasing TSR intensity, while the carbon and hydrogen isotopic composition of C_2H_6 and C_3H_8 became heavier and shows smaller differences with increasing temperature, similar to the results from thermal cracking of crude oil. The production of alkane gas with similar chemical and isotope compositions to H_2 S-bearing natural gas during these experiments, suggest that TSR can alter the carbon and hydrogen isotopic composition of alkane gas $^{(0,2)}$. In addition, a partially reversed carbon isotope series of alkane gas ($\delta^{13}C_1 > \delta^{13}C_2 < \delta^{13}C_3$) was observed, which further confirms the above conclusion. 12 C-enriched CO₂ was mainly produced from the oxidation of hydrocarbons by TSR. However, dissolution of CO₂ and precipitation of carbonate minerals in aqueous fluids can complicate the carbon isotopic composition in the marine carbonate reservoir⁴⁵.

Conclusions

Pyrolysis of TSR was carried out using different organic matter (crude oil, nonane and methylnaphthalene), and the characteristics of carbon and hydrogen isotopes, as well as the composition and yields of the reaction products were analysed. The following main conclusions can be drawn:

(1) The carbon and hydrogen isotopic composition of alkane gas generally becomes heavier with increasing carbon number, i.e., $\delta^{13}C_1 < \delta^{13}C_2 < \delta^{13}C_3$ and $\delta^2H-C_1 < \delta^2H-C_2 < \delta^2H-C_3$. At the same temperature, the carbon and hydrogen isotopic composition of CH₄ gradually became larger with longer reaction time. The carbon and hydrogen isotopic composition of C₂H₆ and C₃H₈ also became heavier as the reaction continued, but the variation was significantly larger than that for CH₄. The variation of the carbon and hydrogen isotopic composition of C₃H₈. Rapid oxidation of source material by TSR produced CH₄ with a small variation in carbon and hydrogen isotopic values, revealing that this process can alter the carbon and hydrogen isotopic composition of CH₄, making it similar to those of the original precursor material. (2) The partially reversed carbon isotope series observed in alkane gas in natural gas. As the reaction continued, ¹³C became enriched in residual heavy hydrocarbon gas, which altered the commonly observed

order of $\delta^{13}C_1 > \delta^{13}C_2$ to a positive carbon isotope series ($\delta^{13}C_1 < \delta^{13}C_2$). For the first time, we confirmed the ability of TSR to alter the isotopic composition of alkanes, causing isotope reversal during TSR pyrolysis. (3) Under conditions of TSR, hydrogen isotopes of alkane gases form a positive isotope series ($\delta^2H-C_1 < \delta^2H-C_2 < \delta^2H-C_3$). Isotope fractionation is large, especially for ethane and propane, presumably due to the low molecular weight of hydrogen.

(4) During pyrolysis, oil cracking and TSR result in different $\delta^{13}C_1 - \delta^{13}C_2$ and $\delta^2H - C_1 - \delta^2H - C_2$ evolutionary trends. While $\delta^{13}C_1 - \delta^{13}C_2$ and $\delta^2H - C_1 - \delta^2H - C_2$ became smaller with increasing intensity of TSR, $\delta^{13}C_1 - \delta^{13}C_2$ and $\delta^2H - C_1 - \delta^2H - C_2$ became larger with increasing intensity of oil cracking.

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Author contributions

Q.L., W.P. and X.W. wrote the main manuscript text. Q.M., D.Z. and Z.J. reviewed the manuscript, and put forward some constructive suggestions.

Competing interests

The authors declare no competing interests.

Additional information

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