

Addendum to: Understanding environmental trade-offs and resource demand of direct air capture technologies through comparative life-cycle assessment

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In this Addendum, we clarify the assumptions made when constructing the product system for the high-temperature aqueous solution (HT-Aq) direct air capture (DAC) unit.

The HT-Aq DAC product system uses information published by Carbon Engineering, but we made several distinct changes to that system—in particular, in the calcination step—resulting in a simplified hypothetical new product system. Carbon Engineering’s DAC prototype includes an oxy-fuel-fired circulating fluid bed calciner that uses an in-bed combustion process to convert calcium carbonate (CaCO₃) pellets into CO₂ and CaO. Such a calciner design allows for the co-capture of CO₂ streams emitted during the processing of CaCO₃ and the heat supply via combustion of natural gas inside the calciner. This co-capture of fuel-related carbon reduces the carbon emissions from the combustion of natural gas in the calciner and comes at the expense of additional demand for CO₂ compression, liquefaction, transport and storage.

Table 1 | Calculation of the carbon capture efficiency (CCE) for HT-Aq DAC with co-capture of combustion-related CO₂. The case without co-capture is reported in the paper.

System type:	HT-Aq DAC without co-capture	HT-Aq DAC with co-capture	Formula/source
Variable (unit, symbol)			
Atmospheric CO ₂ captured (t, a)	1.00	1.00	By definition
Fuel CO ₂ released during combustion (t, b)	0.28	0.33	HT-Aq DAC without co-capture: main paper and Supplementary Data 1, Co-capture case: Keith et al. (2018) ¹ , Figure 2: 112 t CO ₂ captured per hour, 13.4 t CH ₄ burned per hour, stoichiometry gives 0.329 t CO ₂ (combustion) per t CO ₂ captured
Amount of methane required (t, c)	0.10	0.12	HT-Aq DAC without co-capture: main paper and Supplementary Data 1, Co-capture case: Keith et al. (2018) ¹ , Figure 2: 112 t CO ₂ captured per hour, 13.4 t CH ₄ burned per hour
Methane supply chain emissions (t, d)	0.10	0.12	HT-Aq DAC without co-capture: main paper and Supplementary Data 1, Co-capture case: Scaled up from the case without co-capture using the methane flow c.
CO ₂ vented (t, e)	0.28	0.00	By definition
Fuel CO ₂ captured for storage (t, f)	0.00	0.33	By definition
Total CO ₂ captured for storage (t, g)	1.00	1.33	Total CO ₂ captured for storage = Atmospheric CO ₂ captured (a) + Fuel CO ₂ captured for storage (f)
Lifecycle CO ₂ e emissions to capture 1t CO ₂ (t CO ₂ e, h)	0.54	0.24	HT-Aq DAC without co-capture: main result (see SD.1, Table F1.a, cell J4) Co-capture: Lifecycle CO ₂ e emissions to capture 1 t CO ₂ (h) = Lifecycle CO ₂ e emissions to capture 1 t CO ₂ (h, modelled case) – methane supply chain emission (d, modelled case) – fuel CO ₂ captured for storage (f, co-capture case) + methane supply chain emissions (d, co-capture case)
Lifecycle CO ₂ e emissions to transport and store total captured CO ₂ (t CO ₂ e, i)	0.05	0.06	HT-Aq DAC without co-capture: main result (see Supplementary Data 1, Tab F, Table 2.a, cell I40) Co-capture case: Scaled up from the case without co-capture using the capture flow g.
Life cycle CO ₂ e emission to capture, transport, and store 1 t atmospheric CO ₂ (t CO ₂ e, j)	0.59	0.30	Total life cycle CO ₂ emission to capture 1 t atmospheric CO ₂ (j) = Life cycle CO ₂ emissions to capture 1 t CO ₂ (h) + Life cycle CO ₂ e emissions to transport total captured CO ₂ (i)
CCE (%)	41	70	CCE% = 100*(a-j)/a

In Carbon Engineering's setup, it is physically impossible to separate the two CO₂ streams at the outlet of the calciner¹.

For the comparative LCA, we decided to model the HT-Aq DAC product system with different energy supply options and then compare it to the product systems of other DAC technologies with the same energy supply. Therefore, the calciner in the modelled product system for HT-Aq DAC has two CO₂ streams at the outlet, calculated from the separate mass balances for limestone decarbonization and methane combustion. For the energy supply baseline, the combustion-related CO₂ flow in the product system is not co-captured and stored.

This modification allows us to model various sources of thermal heat, and it ensures comparability between the different DAC products systems for different energy supply options, including the current electricity grid mix and natural gas supply. One must note, however, that such devices are currently not commercially available at large scale, and commercially available calciners retain both CO₂ streams. With the co-capture of CO₂ in the current design of Carbon Engineering, their prototype operates at a better carbon capture efficiency (CCE, see paper) than our modelled baseline product system without co-capture. We have now calculated the CCE of HT-Aq DAC where both CO₂ streams are retained and subsequently sequestered to be 70% (compared to 41% for our HT-Aq result without co-capture). These numbers are calculated from Table 1 below.

The separation of the calciner heat supply process also enables us to consider different types of electricity and heat supply in a potential calcination process with indirect heating, as done in the sensitivity analysis (see Fig. 2 of the main paper). In such an indirectly or jacket-heated calciner, the heat source (e.g., natural gas burners, electrical heaters, etc.) is located outside the shell of the calciner. Such a calciner can utilize sources of energy other than gaseous fuel, including high-temperature solar-thermal heat². Assessing the large-scale technical and economic feasibility for utilizing an indirectly heated calciner in the current Carbon Engineering plant design is outside the scope of this paper.

To clarify the modelling used in the study, in the main paper, text in the Abstract, main text "Goal and scope of the comparative assessment" and "DAC carbon capture efficiency" sections, Methods "Life-cycle CCE" and "HT-Aq DAC" subsections, and Supplementary Note 4 and the cover sheets of Supplementary Data 1 and 2 have been modified. The updates are available in the HTML and PDF versions of the article.

References

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