ARTICLE OPEN Check for updates Facile fabrication of paper-based flexible thermoelectric generator

Zuoyuan Dong $\mathbb{D}^{1,3}$, Hua Liu^{2,3}, Xin Yang¹, Jichen Fan¹, Hengchang Bi¹, Chaolun Wang¹, Yonghua Zhang¹, Chen Luo¹, Xinqian Chen¹ and Xing Wu $\mathbb{D}^{1}^{\boxtimes}$

Paper, as a foldable, pollution-free, and low-cost material, has become a suitable support substrate for producing flexible thermoelectric (TE) generators to realize waste heat recycling and the application of human-powered electronic devices. We propose a facile fabrication method to modify cellulose paper with inorganic TE powders via vacuum filtration, making a modified paper that possesses good thermoelectric properties. By connecting the modified paper to copper foils, flexible paper-based TE generators (PTGs) are fabricated. The obtained PTG with three units of P–N modules can generate an output voltage of ~41.2 mV at a temperature difference of 50 K. Based on this modified paper, a thermal sensor that responds to heat sources, such as fingers, is proposed with a rapid response time of 0.25 s. This work offers a promising strategy for the simple fabrication of PTGs, paving the way for achieving the commercial application of self-powered wearable electronics.

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INTRODUCTION

The invention of cellulose fiber-based paper has undoubtedly contributed greatly to the progress of society over thousands of years. Recently, paper has also become a popular and promising component used in flexible electronics due to its foldability, low cost, light weight, and environmental friendliness^{1–5}. Some techniques, such as printing and magnetron sputtering, are perfectly combined with paper, making paper a substrate or skeleton to achieve creative applications in flexible field-effect transistors⁶, sensors⁷, and energy harvesting devices⁸. In particular, paper-based thermoelectric (TE) energy harvesting devices have been proposed to realize waste heat utilization on flexible surfaces^{9–12}. TE generators can directly convert heat into electrical energy from a temperature difference. Their efficiency is determined by the dimensionless figure of merit ZT ($ZT = S^2 \sigma T/\kappa$), where S is the Seebeck coefficient, σ is the electrical conductivity, T is the absolute temperature, and κ is the thermal conductivity. Current efforts tend to combine thermoelectricity and wearability to power portable electronic devices through temperature differences between the human body and environment¹³. The obstacle to commercialization of this concept is the difficulty in making lightweight and flexible inorganic TE materials. An effective way is to make TE materials into films or papers^{14,15}. In recent years, some promising TE materials, such as Bi₂Te₃ and Sb₂Te₃, have been prepared for paper-based TE generators (PTGs) by combining with paper, thereby realizing light and flexible TE generators. Rojas et al.⁹ prepared a flexible, paper-based origami TE generator by magnetron sputtering, and its optimized output power reached ~80 nW at a temperature difference of 75 K. Zhao et al.¹⁰ fabricated a transparent and flexible PTG using modified distributor printing technology to obtain a maximum voltage of ~8.3 mV at a temperature difference of 35 K. These works successfully circumvent the brittleness of inorganic semiconductors to achieve flexible PTGs and demonstrate their possible application.

There are some issues, such as complicated preparation processes, high preparation costs, and poor performance in current PTGs. Therefore, it is necessary to develop more efficient and inexpensive preparation techniques to achieve the large-scale application of PTGs. In this work, we explore a simple method to modify cellulose paper and use modified paper to fabricate PTGs. In this method, cellulose paper is modified by infiltrating inorganic TE materials (doped Bi₂Te₃ and Sb₂Te₃) into a paper matrix via a vacuum-assisted filtration process. The foldable PTGs are fabricated by connecting the cut modified paper to copper foils. The obtained PTG with three units of P-N modules can generate ~41.2 mV at a temperature difference of 50 K. Furthermore, based on the modified paper, a finger touch sensor is fabricated, which can respond quickly to heat sources with a relaxation time of 0.25 s. This work demonstrates the feasibility of PTGs and thermal sensors prepared by modified cellulose paper.

RESULTS AND DISCUSSION

Fabrication of the generators

Figure 1a shows the fabrication process of modified cellulose papers and PTGs. The N- and P-type modified papers are prepared through the vacuum filtration method. The N-type material is Bi₂Te₃ doped with Se, and the P-type material is Sb₂Te₃ doped with Bi. First, N-type TE powder (100 mg) and sodium carboxymethyl cellulose (CMC-Na) are dispersed in 30 ml deionized water at a mass ratio of 12 to 1, and the mixture is stirred for 10 min to form an N-type TE dispersion. CMC-Na is used to enhance the stability of the TE dispersion. The dispersion is then sonicated for 40 min to reduce the particle size of the TE powder and to allow it to fully disperse. The treated dispersion is poured into a vacuum flask for suction filtration. A pump is connected to the suction bottle mouth to maintain a pressure difference. The relative pressure is -0.06 MPa, and suction filtration is conducted for 4–5 h. The P-type TE powder is prepared with the same procedure. The experimental process of vacuum-assisted filtration has been

¹Shanghai Key Laboratory of Multidimensional Information Processing, School of Communication and Electronic Engineering, East China Normal University, Shanghai, China. ²Department of Cardiology, Shanghai Geriatric Medical Center, Shanghai, China. ³These authors contributed equally: Zuoyuan Dong, Hua Liu. ^{Se}email: xwu@ee.ecnu.edu.cn



Fig. 1 Preparation process of flexible paper-based thermoelectric generator (PTG) and the photos display. a Schematic diagram of the fabrication process for PTGs. The N- and P-type modified papers are prepared through the vacuum filtration method, cut into small strips and connected with copper foil in an alternating sequence. b–e Photographs of the complete modified papers obtained by the vacuum filtration method (b), displaying their high flexibility (c), the small 5 mm \times 20 mm strips (d), and the PTG with three units of P–N modules (e). The smallest grid point of the background grid paper represents 1 mm.

described in our reported works^{16,17}. Relying on the pressure difference, the TE particles infiltrate into and adhere to the filter paper, and the modified papers shown in Fig. 1b are formed after drving. Changing the quality of TE powder results in modified paper with different weight percentages (the mass of TE particles as a percentage of the total mass of modified paper). In this work, we prepare modified papers in three different percentages: 37% (modified paper₃₇), 59% (modified paper₅₉), and 70% (modified paper₇₀), with 100, 200, and 300 mg of TE powders, respectively. The modified papers display excellent flexibility, which is shown in Fig. 1c. Subsequently, the N- and P-type modified papers are cut into identical strips with dimensions of 5 mm × 20 mm, which are shown in Fig. 1d. After this, the small strips are used as TE legs and are alternately connected to copper foils in the form of an "N-P-N-P" sequence to form a conductive path. Both sides of the obtained series of TE legs are covered with polyimide (PI) for packaging and then flattened with a pressure anvil at 10 MPa to enhance the compactness of the TE particles. After the wires are attached on the ends of the TE legs, the flexible PTG shown in Fig. 1e is finally fabricated, which is comprised of several pairs of P-N modules. This is a facile and inexpensive method for preparing flexible TE generators and can be applied on a large scale.

General characterization

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The cross-sectional morphology of the modified paper was characterized by scanning electron microscopy (SEM). For comparison, Fig. 2a, b shows the cross-section SEM images of the pristine paper at scale bars of 100 and 10 μ m. The inset of Fig. 2a is a photograph of filter paper used in the experiment. Figure 2c provides the cross-section micromodel, which shows that paper is

composed of adjacent and interlaced cellulose fibers. Figure 2d, e shows the SEM images of the N-type modified paper at the corresponding scale. In Fig. 2d, the upper layer of the modified paper is enlarged in the insert with a scale bar of 50 µm, and the lower layer is enlarged in Fig. 2e. Through vacuum filtration, some of the particles are deposited on the surface of the paper, which forms a compact layer called the deposition layer, while some of the particles penetrate into the paper and adhere to the cellulose fibers, forming an infiltration layer. The final modified paper consists of a deposition layer and infiltration layer, and its structural model is illustrated in Fig. 2f. Due to the same treatment procedure, the sizes of the N- and P-type powders are similar (less than 10 µm). The TE grains in the deposition layer are compact and are adjacent to each other to form a conductive path. The grains that infiltrate into the paper are used as a conductive supplement, and the cellulose fiber ensures the flexibility of the modified paper.

The elemental composition of the active materials in the modified paper was characterized by transmission electron microscopy (TEM). The P-type TE material is Sb₂Te₃ doped with Bi, and the N-type is Bi₂Te₃ doped with Se. Their crystalline structures are exhibited in Fig. 2g, h, which show that Sb₂Te₃ and Bi₂Te₃ are hexagonal crystalline structures formed by stacking quintuple layers. The two quintuple layers are connected by weak van der Waals forces. Figure 2i, j are high-resolution TEM (HRTEM) images of Sb₂Te₃ doped with Bi and Bi₂Te₃ doped with Se, respectively. The corresponding fast Fourier transform (FFT) images indicate the hexagonal structure of both Sb₂Te₃ and Bi₂Te₃. Both the HRTEM and FFT images show the good crystallinity of Sb₂Te₃ and Bi₂Te₃. Figure 2k, I are the energy



Fig. 2 Microscopic characterizations of pristine and modified papers with SEM and particles with high-resolution TEM. a Cross-sectional SEM images of the pristine paper with scale bars of 100 μ m and **b** 10 μ m. The inset of **a** is a photograph of the filter paper used in the experiment. **c** Simple structural model of the filter paper with the adjacent cellulose fiber. **d** Cross-sectional SEM image of the N-type modified paper with a scale bar of 100 μ m. The insert is an enlarged view of the deposition layer on the upper part of the modified paper, and the scale bar is 50 μ m. **e** Enlarged view of the infiltration layer marked with an orange rectangle in (**d**). The TE particles are less than 10 μ m. The SEM images are from the N-type modified paper. **f** Micromodel of the modified paper composed of a deposition layer and infiltration layer. **g** Crystalline structures of Sb₂Te₃ doped with Bi and **h** Bi₂Te₃ doped with Se. The scale bars are 0.5 nm. **k** Energy dispersive spectroscopy (EDS) results of Sb₂Te₃ doped with Bi and **l** Bi₂Te₃ doped with Se. The atomic percentages of the corresponding elements are listed in the inserted table.

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Fig. 3 TE performance tests of the PTGs. a–**c** Open-circuit voltage of the PTGs prepared by modified $paper_{37}$ (**a**), modified $paper_{59}$ (**b**), and modified $paper_{70}$ (**c**) at temperature differences of 5 to 50 K. **d** Open-circuit voltage of the PTGs versus the three weight percentages at a temperature difference of 30 K. **e** Seebeck coefficients (absolute value) of a single leg of the PTGs at the three weight percentages. **f** Output voltage and output power curves according to the various external circuit currents. **g** Changes in the resistance and Seebeck coefficient after 400 bending cycles. The insert is the schematic diagram of the bending test. **h** Photograph of human skin generating electricity with the PTGs.

Table 1. Comparison of the reported Seebeck coefficient of a single leg of the flexible TE devices at room temperature.			
TE materials	Method	Seebeck coefficient (μ V·K ⁻¹)	Reference
Bi ₂ Te ₃ /paper composite	Modified distributor printing technology	60	10
PEDOT:PSS	Screen-printing	99	18
PEDOT nanowires	Vacuum-assisted filtration	25.5	19
Bi_2Te_3 and Sb_2Te_3 modified paper	Vacuum-assisted filtration	142	This work

dispersive spectroscopy (EDS) results of Sb₂Te₃ and Bi₂Te₃, respectively. The atomic percentages indicate that Sb:Te:Bi is approximately 33:61:6 and Bi:Te:Se is approximately 46:50:4. The specific composition of the N- and P-type active materials has been clarified.

Performance of the generators

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PTGs with 1-3 units of P-N modules are fabricated and packaged with PI. The TE performance of the PTGs was tested, as shown in Fig. 3a-c shows graphs of the open-circuit voltage of PTGs with different weight percentages of active materials versus the temperature difference. At the same weight percentage, the open-circuit voltage increases proportionally with the units of the P–N modules. The largest voltage reaches \sim 41.2 mV at a ΔT of 50 K and a weight percentage of 70%. The open-circuit voltages with different weight percentages at a ΔT of 30 K are summarized in Fig. 3d. This figure shows that as the weight percentage increases, the generated voltage increases because more active materials participate in power generation. In regard to the weight percentages at 37%, 59%, and 70%, the PTGs with three units of P–N modules generate open-circuit voltages of ~19.6 mV, ~22.3 mV and ~25 mV at a ΔT of 30 K, respectively. The Seebeck coefficient is an important parameter to characterize TE performance, which is defined as the magnitude of the generated TE voltage per degree of temperature difference. The definition can be expressed as

$$S = \frac{dV}{dT}$$
(1)

where *S* is the Seebeck coefficient and *V* is the TE voltage. Thus, the Seebeck coefficients of the flexible PTGs are obtained by calculating the single leg of PTGs, which are shown in Fig. 3e. For modified paper₃₇, modified paper₅₉, and modified paper₇₀, the average Seebeck coefficients are 112, 128, and 142 μ V K⁻¹ (absolute value), respectively. Compared to previous reports on flexible TE generators, which are listed in Table 1^{10,18,19}, the above values are impressive. Of course, the high efficiency of TE generators is not determined by a single parameter, which requires us to make further efforts to this end. Figure 3f shows the variations in the external circuit voltage and output power with current in the PTG with three units of modules. As the load resistance increases, the current in the circuit decreases, and the voltage across the resistor increases. The value of the output power is the product of the external circuit voltage and current.



Fig. 4 Sensor response of the modified paper with a finger touch. a Voltage response with a finger touch at a frequency of approximately 1 s^{-1} . The insert is the illustration of the finger touch test. **b** Enlarged view of the blue dashed box in (**a**).

The current can be obtained by

$$I = \frac{U_o}{R_i + R_L} \tag{2}$$

where U_o is the open-circuit voltage of the TE device, R_i is the internal resistance of the PTG, and R_L is the load resistance of the circuit. The external circuit voltage U_e can be expressed as

$$U_e = I \cdot R_L \tag{3}$$

and the output power P can be expressed as

$$P = U_e \cdot I \tag{4}$$

In Fig. 3f, it can be observed that the maximum output power is ~709 pW at a ΔT of 40 K, ~351 pW at a ΔT of 30 K, and ~155 pW at a ΔT of 20 K. The biggest reason for the output power being at a low level is that the internal resistance of the device is too large, which is over 50 k Ω for a single leg in the PTG. The durability of PTGs is tested with repeated bending cycles. Figure 3g shows that the variation in internal resistance is less than 10% after 400 bending cycles with a bending angle of approximately 103°, and the Seebeck coefficient is less than 5%. The good stability and durability indicate the potential application of the modified paper in flexible heat source identification devices. Flexible PTGs can be applied to human skin for power generation using the temperature difference between the ambient air and body. Figure 3h displays the PTG attached to the wrist of a human body, which produces an open-circuit voltage of 2.38 mV at a temperature difference of 5-6 K. This observation demonstrates that these PTGs have potential applications for human energy harvesting.

Flexible modified paper can also be used as a thermal sensor to achieve a rapid response to contacting a heat source. Figure 4a shows the voltage response of the flexible modified paper with a finger touch, and Fig. 4b is the enlarged view in the blue dashed box of Fig. 4a. The inset shows the test process of the sensor response. When the finger is completely pressed on one side of the paper for heating, the open-circuit voltage of the paper reaches approximately 5 mV. After 25 s, the position touched by the finger changes from one terminal of the modified paper to the other, and the polarity of the voltage alternates accordingly. The graphs depict that the voltage increases and decreases sharply with the finger touch at a frequency of approximately 1 s⁻¹, illustrating that the modified paper is sensitive to changes in external temperature. It is noted that the maximum voltage for each cycle is not consistent, which is due to the different temperature changes induced by the finger touch. From Fig. 4b, a response time (τ_{res}) of 0.25 s and a recovery time (τ_{recov}) of 0.40 s are obtained. The response time is defined as the time required for the sensor to move from the baseline to 90% of its maximum voltage after finger pressing, and the recovery time is the time to move from 90% of its maximum voltage back to the baseline value after retracting the finger. Paper-based thermal sensors are expected to enable the self-powered control of wearable electronics.

In summary, N- and P-type modified paper and flexible PTGs were simply fabricated via vacuum filtration, and a high output voltage was obtained. Regarding the modified paper, some of the particles were deposited on the surface of the paper to form a deposition layer, and some of the particles penetrated into the paper to form an infiltration layer. The modified paper comprised of these two layers formed a conductive path. The TE particles were characterized by HRTEM and EDS, which showed that the specific component of the P-type TE material was SbTeBi with a ratio of approximately 33:61:6 and that the N-type TE material was BiTeSe with a ratio of approximately 46:50:4. The modified paper possessed a high Seebeck coefficient of 142 μ V K⁻¹, and PTGs with three units of P-N modules could obtain a maximum output power of ~709 pW at a ΔT of 40 K. Furthermore, based on the TE effect, a paper-based thermal sensor with a response time of 0.25 s was investigated. This work demonstrates the feasibility of PTGs and paper-based thermal sensors prepared by vacuum-assisted filtration.

METHODS

Materials

Doped Bi_2Te_3 (powder, 99.99%) and Sb_2Te_3 (powder, 99.99%) were purchased from Qijin New Material (Quanzhou, China). CMC-Na was purchased from Shandong Usolf Chemical Technology Company (Linyi, China). Medium-speed qualitative filter paper with a diameter of 9 cm was used in the experiment.

Characterization and testing

The SEM images were obtained by using an FEI XL30 FEG with an accelerating voltage of 20 kV. To conduct electricity, the cross-sections of the paper and TE film were covered with 20 nm of Au. To obtain an intact cross-section, the paper and paper-based TE film were broken after cooling with liquid nitrogen. The structural and compositional characterization of the samples were carried out by a JEM-ARM300F equipped with EDS at an accelerating voltage of 300 kV. TEM samples were prepared by the ultrasonic processing and centrifugation of the powder samples. Then, the supernatants of the centrifuged samples were drop cast on lacey carbon films and dried naturally for TEM characterization.

A heating stage (NWJ-3020) was used to heat the PTGs, and a thermocouple was used to monitor the real-time temperature. The voltage and sensor tests were carried out on an electrochemical workstation (CHI660E), and the current was measured by a picoammeter (Keithley Model 6485).

DATA AVAILABILITY

The datasets generated and analyzed during the current study are available from the corresponding authors upon reasonable request.

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AUTHOR CONTRIBUTIONS

X.W., Z.D., and H.L. conceived and designed the experiments. Z.D., J.F., and C.W. fabricated and measured the PTGs. H.L. C.L., X.C., and X.Y. characterized and analyzed the materials. X.W., H.B., C.W., and Y.Z. supervised the overall research. Z.D., H.L. H.B., X.W., and C.L. contributed to the writing of the paper. Z.D. and H.L. are contributed equally to the paper.

COMPETING INTERESTS

The authors declare no competing interests.

ADDITIONAL INFORMATION

Correspondence and requests for materials should be addressed to X.W.

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