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Low limit of detection of the AlGaN/GaN-based sensor by the Kelvin connection detection technique

Hanyuan Zhang¹, Ying Gan², Shu Yang^{1,3}, Kuang Sheng^{1,3} and Ping Wang²

Abstract

The AlGaN/GaN-based sensor is a promising POCT (point-of-care-testing) device featuring miniaturization, low cost, and high sensitivity. BNP is an effective protein biomarker for the early diagnosis of HF (heart failure). In this work, a novel AlGaN/GaN device with the Kelvin connection structure and the corresponding detection technique was proposed. This technique can effectively suppress the background noise and improve the SNR (signal-to-noise ratio). A BNP detection experiment was carried out to verify the effectiveness of this technique. It is shown that compared with that of the traditional detection method, the LOD (limit of detection) was improved from 0.47 ng/mL to 1.29 pg/mL. The BNP detection experiment was also carried out with a traditional electrochemical Au-electrode sensor with the same surface functionalization steps. The AlGaN/GaN sensor showed a better LOD than the Au-electrode sensor. Moreover, the influence of AlGaN/GaN sensor package on background noise was investigated with the mechanism of the noise source revealed. Finally, based on the optimized package, the optimal SNR quiescent operating point of the AlGaN/GaN sensor was determined. By biasing the sensor at the optimal quiescent operating point and immobilizing the magnetic beads with anti-BNP on the gate of the AlGaN/GaN sensor, the LOD for BNP detection was further improved to 0.097 pg/mL.

Introduction

Heart failure (HF) is a cardiovascular disease that is one of the leading causes of death worldwide. The detection of clinically relevant cardiac biomarkers is effective in allowing the early diagnosis of HF, reducing the complications and the risk of recurrence, and ultimately reducing the economic burden on the entire medical system. Brain natriuretic peptide (BNP) is one of the most promising clinical biomarkers of HF. Based on various reports^{1,2}, the clinical cutoff level of BNP in chronic HF diseases is ~100 pg/mL. In addition, there are reports that BNP has predictive value in the diagnosis of

²Biosensor National Special Laboratory, Department of Biomedical Engineering, Zhejiang University, 310027 Hangzhou, China Full list of author information is available at the end of the article These authors contributed equally: Hanyuan Zhang, Ying Gan Currently, the clinical diagnostic systems used to detect protein biomarkers has drawbacks such as the need for relatively high volumes of blood samples, well-trained experts, large-scale equipment, and long processing times. A low cost, portable, and accurate POCT device is urgently needed for increased in-home monitoring of protein biomarkers for global epidemics such as HF.

The AlGaN/GaN FET sensor is a promising POCT device⁴⁻⁶. With the use of different functionalization processes, the AlGaN/GaN immunoFET⁷ can detect various disease biomarkers^{4,5,8-10}. However, compared with other traditional electrochemical biosensors, such as Au electrodes, the manufacturing process for AlGaN/GaN FET devices is more complicated, GaN epitaxy is more expensive, and the device package design is more difficult, while the advantages of AlGaN/GaN sensors versus Au electrodes are not clear. In this work, by adopting the same surface

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Correspondence: Shu Yang (eesyang@zju.edu.cn)

¹College of Electrical Engineering, Zhejiang University, 310027 Hangzhou, China

anthracycline-induced cardiotoxicity $(AIC)^3$, for which the diagnostic threshold is 107.9 pg/mL.

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functionalization method for the traditional Au-electrode electrochemical sensor and the AlGaN/GaN FET sensor (Device A in this work), the BNP detection performances of the two sensors were compared.

The two-dimensional electron gas (2DEG) structure formed by the AlGaN/GaN heterojunction can achieve both high carrier mobility (typically, $\sim 2000 \text{ cm}^2/\text{V} \cdot \text{s}$) and high electron density (typically, $\sim 1 \times 10^{13} \text{ cm}^{-2}$)¹¹; thus, the current sensitivity S_{I} , which represents the ability of the AlGaN/GaN device to amplify the biosignal, is very high¹². Therefore, methods to improve the sensitivity of AlGaN/GaN sensors have been extensively studied¹¹⁻¹⁹. However, in practical applications, the background noise of the device may also be amplified, and the benefits of the high sensitivity will then be offset. As a result, it is very important to determine how to reduce the background noise of the device to improve the overall performance. To reduce the background noise and improve the SNR of the device, we proposed using a Kelvin connection device structure and the corresponding test method. The fourprobe test method is an electrical measurement method used to accurately measure resistance while excluding the influence of the series resistance. The principle involves decoupling the current loop and the voltage measurement loop so that the current and voltage signals can be measured accurately and the resistance can be calculated accurately. The Kelvin connection technique was also used in traditional ISFET sensors²⁰. However, the role of the Kelvin connection in ISFETs and AlGaN/GaN devices is different. In the ISFET device, the Kelvin connection technique is used to isolate the terminal voltage measurement loop from the current source loop. However, in the AlGaN/GaN sensor, it is used to suppress the background noise and improve the SNR. The difference in the Kelvin connection technique of the two devices originates from the differences in sensor structures and sensor characteristics. In the fabrication process of the CMOScompatible ISFET, it is relatively difficult to produce a successful passivation layer to selectively expose the active sensing area and to protect the metal leads from the solution at the same time. Therefore, there are long source and drain regions that are highly doped with Si, and these are simplify the use of materials such as thick epoxy to cover the metal leads²¹. The highly doped drift regions provide excessive series resistance, which reduces the current sensitivity of the FET sensor¹¹. Moreover, since the SiO₂ gate oxide layer grown by the thermal oxidation process is easily penetrated by the ions in the solution, which causes the turn-on voltage shift and device failure, the poly gate is connected to the thick SiN_x layer acting as the passivation layer and the gate-sensitive membrane²¹. The SiN_x layer provides excessive series capacitance to the gate of the ISFET, and the current sensitivity is further reduced. Therefore, to compensate for the poor current sensitivity, source and drain follower read-out circuits are often used in sensor arrays to ensure that the reference electrode is grounded²². In the ISFET read-out circuit, both drain-to-source voltage (V_{DS}) and drain-to-source current (I_{DS}) are constant, and the change in the solution will cause a change in the gate voltage ΔV_G through the double layer on the solution/SiN_x interface. $\Delta V_{\rm G}$ is equal to the output signal source voltage (V_S) and is amplified by the off-chip amplifier. To accurately read the $V_{\rm S}$, the voltage readout circuit loop is decoupled with the current-flowing circuit loop based on the Kelvin connection technique. In the source and drain follower read-out circuit, the ΔV_G signal is not amplified, and the signal-to-noise ratio (SNR) is limited by the electronic noise of the read-out circuit instead of the ISFET device itself. In this work, the AlGaN/GaN sensor is biased with a constant $V_{\rm DS}$ voltage, and $I_{\rm DS}\,{=}\,\Delta V_{\rm G}\,{\times}\,g_{\rm m}$ is read out as the output signal (equivalent to $R_{\rm DS} = V_{\rm DS}/I_{\rm DS}$ when $V_{\rm DS}$ is a constant). $\Delta V_{\rm G}$ is amplified by $g_{\rm m}$, and the SNR is limited by both gm and the noise of the AlGaN/GaN sensor itself. The reason for using the Kelvin connection technique in the AlGaN/GaN sensor is that according to our previous study¹¹, the series resistance reduces the g_m of the sensor. The Kelvin connection technique can reduce the influence of the series resistance and improve $g_{\rm m}$. However, in the experiment, we unexpectedly found that the Kelvin connection technique also contributes a positive role in the noise performance of the device; it not only reduces the thermal white noise on the series resistance but also effectively reduces the overall 1/f mode background noise of the AlGaN/GaN sensor and improves the LOD.

Passivation is one of the key challenges in liquid sensors⁷. It is well known that the quality of the package will affect the device lifetime 2^{23-27} and the safe operating area $(SOA)^{28}$. However, the influence of the package on the device background noise has not been discussed. PECVD-grown SiO₂ and SiN_x are CMOS-compatible packaging materials often used as liquid sensors^{17,18,29,30} In our previous work, the PI/SiN_x/SiO₂ multilayer package was found to effectively suppress the leakage current I_G flowing between the metal and the reference electrode in the solution under different voltage stres ses^{31} . By comparing the correlation between I_G and the background noise for the PI/SiN_x/SiO₂ multilayer package and the traditional SiO₂/SiN_x package, we found that the package material affects the device background noise by influencing the gate leakage current. The mechanism of the process was also illustrated by the experimental results.

The quiescent operating point of the AlGaN/GaN sensor is an important factor that influences the sensitivity³². However, the effect of the quiescent operating point on the SNR has not been investigated. In this work, the

SNR of the AlGaN/GaN device with different quiescent operating points was determined. Another method to detect BNP was developed by immobilizing anti-BNP on the magnetic beads and adsorbing the magnetic beads on the surface of the AlGaN/GaN open gate area through a magnet⁸. The device (Device B in this work) was biased at the optimal quiescent operating point, and the LOD for BNP detection was further improved to 0.097 pg/mL.

Results

BNP detection: Au-electrode with EIS

Figure 1a shows the change in the charge transfer resistance (R_{CT}) of the Au electrode with the functionalization process in the Electrochemical Impedance Spectroscopy (EIS) test. The R_{CT} increased from 1 to 2 after the Au electrode was coated with BNP antibody (anti-BNP) and further increased from 2 to 3 after the binding sites were blocked by bovine albumin (BSA). When BNP and anti-BNP were specifically bound, $R_{\rm CT}$ decreased from 3 to 4, and the amount of $R_{\rm CT}$ decrease was $\Delta R_{\rm CT}$. The inset shows the circuit model used to simulate the $R_{\rm CT}$ value in the EIS curve. $R_{\rm S}$ represents the series resistance, including the solution resistance and the series resistance in the circuit. $R_{\rm CT}$ is the charge transfer resistance, and constant phase element (CPE) is used to simulate the capacitance of the double layer and compensate for the nonhomogeneity in the system. Figure 1b shows the plot of $\Delta R_{\rm CT}$ versus different BNP concentrations ranging from 1 ppb to 500 ppb. R_{CT3} is the charge transfer resistance of the Au electrode after BSA blocking, and the standard deviation is $\sigma_{RCT3} = 849.4 \Omega$, which can be regarded as the background noise. Substituting σ_{RCT3} three times into Y of the linear fitting line of $\Delta R_{\rm CT}$ -BNP, the X value obtained is the LOD of BNP detection by the Au electrode. In this work, the LOD of the Au-electrode is 2.73 ppb.

The selectivity of the Au electrode treated with this functionalization method was determined, and the results are shown in Fig. S1 in the supplementary material.

Fabrication of the AlGaN/GaN sensor

Two types of AlGaN/GaN devices designed in this work, Device A and Device B, are shown in Fig. 2b, c. The fabrication and packaging process of Device B has been described³¹, and the only difference between Device A and Device B is that the open gate area was deposited with a layer of Au as the sensitive membrane. The PI/SiN_x/SiO₂ multilayer was used as the package in this work. There are four terminals for both Device A and Device B. High force (H. F) and high sense (H. S) terminals are connected to the drain, and low force (L. F) and low sense (L. S) terminals are connected to the source, and the circuit schematic and the actual device connection diagram are shown in Fig. 2a.

BNP detection: AlGaN/GaN sensor (Device A) with Au gate

Figure 3a shows the change in $I_{\rm DS}$ output with the functionalization process of Device A. The trend of $I_{\rm DS}$ change was similar to that of the Au electrode; after the Au gate was coated with anti-BNP, $I_{\rm DS}$ was reduced, and in other words, the channel resistance of the AlGaN/GaN device increased. Then, the Au gate was blocked by BSA, and the $I_{\rm DS}$ increased. Finally, after BNP and anti-BNP were specifically bonded, the $I_{\rm DS}$ decreased again.

Figure 3b shows the $R_{\rm DS}$ baseline measurement for the Kelvin connection technique and two-probe test method after the BSA blocking process. $V_{\rm DS}$ was fixed to be 0.4 V. It is shown that $R_{\rm DS-4probe}$ (drain-to-source resistance measured by Kelvin connection technique) was smaller than $R_{\rm DS-2probe}$ (drain-to-source resistance measured by two-probe method) by ~5 Ω in absolute value, and its



Fig. 1 BNP detection results based on Au-electrode. a Change of R_{CT} in the EIS with the surface functionalization process. The inset is the circuit model used to simulate the R_{CT} value. Z'_{Re} is the real part, and Z'_{Im} is the imaginary part of the impedance in the EIS of the Au electrode. **b** Change in R_{CT} at different concentrations of BNP.



force (H. F) and high sense (H. S) are connected to the drain terminal, low force (L. F) and low sense (L. S) are connected to the source terminal. V_{DS} voltage is applied between the H. F and L. F to form the current loop. The voltage between the H. S and L. S is measured as V_{DS-S} . The diagram on the left is the schematic diagram and that on the right is the OM (Optical microscope (OM) top view of the real device. **b** Device A. The open gate area of device A is deposited by the Au layer. AuNPs (Au nanoparticles) are electroplated on the Au gate, and the anti-BNP is immobilized on the AuNPs to selectively detect BNP. **c** Device B. The open gate area of Device B is bare AlGaN. Magnetic beads immobilized with anti-BNP are absorbed on the AlGaN surface with a permanent magnet on the back side of the chip.



Fig. 3 BMP detection results based on AlGaly/GaN sensor with Au gate memorane (Device A). a Change of I_{DS} output of Device A with the surface functionalization process. **b** R_{DS} -t baseline comparison ($V_{DS} = 0.4$ V) between the Kelvin connection test and the traditional two-probe test. **c** $R_{DS-4probe}$ -t and $R_{DS-2probe}$ -t response to BNP with concentrations ranging from 0.1 ppt to 10 ppb using Device A as the transducer and anti-BNP immobilized on the Au gate. **d** ΔR_{DS} results of BNP detection.

variation was also smaller than that of $R_{\rm DS-2probe}$. The absolute value of $R_{\rm DS-4probe}$ was reduced because it eliminated the influence of the series resistance in both the measurement circuit and the thin film resistance of

the wafer. The reduction in the resistance variation indicates that the series resistance can not simply be regarded as a constant resistance; it also introduced noise into BNP measurements, thereby affecting the LOD of the sensor. The standard deviation of the Kelvin connection technique $\sigma_{RDS-4probe}$ was 0.09 Ω , while that of the two-probe method $\sigma_{RDS-2probe}$ was 0.251 Ω .

Figure 3c shows the $R_{\text{DS-4probe}}$ and $R_{\text{DS-2probe}}$ responses to BNP at concentrations ranging from 0.1 ppt to 10 ppb, indicating that $R_{\text{DS-4probe}}$ showed a more stable response than $R_{\text{DS-2probe}}$. Figure 3d shows the plot of ΔR_{DS} (drainto-source resistance change) versus different concentrations of BNP. Substituting $3\sigma_{R\text{DS-4probe}}$ into the linear fitting curve of Fig. 3d, the LOD of Device A using the Kelvin connection technique is 1.29 ppt. On the other hand, the LOD of the two-probe testing method is only 0.47 ppb due to the larger background noise.

The selectivity of Device A with this functionalization method was determined, and the results are shown in Fig. S2 in the supplementary material.

Package and background noise

Packaging materials need to ensure that the device can be safely operated in solution. An important indicator for characterizing packaging quality is the gate leakage current through the reference electrode of the device under different $V_{\rm G}$ bias voltages. This work showed that the gate leakage current affects the background noise in the $R_{\rm DS}$ baseline of the device. Therefore, optimizing the quality of the package not only directly expands the safe operating area of the device but also effectively reduces the background noise and enables the sensor to obtain a lower LOD. Figure 4a-e are the baseline test results of Device B with different $V_{\rm G}$ biases ranging from 0 V to -3.8 V. The packaging material was PI/SiN_x/SiO₂, which was demonstrated to effectively suppress the gate leakage current in prior work³¹. Figure 4f shows the baseline test of Device B with $V_{\rm G} = 0$ V, but the packaging material was traditional SiN_x/SiO_2 . The leakage I_G current was ${<}10^{-9}\,{\rm A}$ for the ${\rm PI}/{\rm SiN}_{\rm x}/{\rm SiO}_2$ package, while $I_{\rm G}$ was on the order of 10^{-6} A for the SiN_x/SiO₂ package. Moreover, it is obvious from Fig. 4f that $I_{\rm G}$ and $R_{\rm DS}$ showed a strong correlation.

BNP detection: AlGaN/GaN sensor (Device B) with magnetic beads

The $I_{\rm DS}$ background noise $N_{\rm IDS}$ is obtained by calculating the standard deviation of the steady-state $I_{\rm DS}$ (500 ms/sample, sample time 2000 s) with $V_{\rm DS} = 0.4$ V. The $I_{\rm DS}$ response $\Delta I_{\rm DS}$ is obtained from the change in surface potential ψ_0 multiplied by the transconductance $g_{\rm m}$. Thus, the SNR is defined as:

$$SNR = \frac{\Delta I_{DS}}{N_{IDS}} = \psi_0 \frac{g_m(V_G)}{N_{IDS}}$$
(3)

Since ψ_0 depends only on the interaction between the solution and the sensitive membrane, so g_m/N_{IDS} represents the SNR of the device per voltage change in surface potential. Figure 5c shows the test results of g_m of Device B and its g_m/N_{IDS} under different V_G biases. The SNR of Device B reached the optimal value at $V_G = -3.8$ V.

The reason that Device A could not be operated with a negative $V_{\rm G}$ bias is that the SOA (safe operating area) of Device A is very small, so the Au metal on the gate region would be corroded²⁸ at a negative V_G bias. To bias the device at the optimal SNR quiescent operating point, Device B (with a larger SOA) was used as the transducer. To immobilize the anti-BNP on the gate-sensitive area, anti-BNP was first immobilized on magnetic microbeads and then the microbeads were adsorbed on the open gate area of Device B with a magnet. When BNP specifically bonded with anti-BNP, it caused a potential change $\Delta V_{\rm G}$ on the gate of Device B so that the channel resistance R_{DS} was read out as the output signal. The advantage of immobilizing the anti-BNP on the magnetic microbeads is that this method for detecting BNP can be used on Device B, which has a larger SOA. Moreover, the expensive AlGaN/GaN sensor can be easily refreshed and reused by removing the magnet and washing away the microbeads from the gate area. The BNP detection results are shown in Fig. 5a, b. The background noise of Device B at $V_G = -3.8$ V was 0.18 Ω , and the calculated LOD was 0.097 ppt.

The selectivity of Device B with this functionalization method was determined, and the results are shown in Fig. S3 in the supplementary material.

Discussion

The Spearman correlation coefficients of the $I_{\rm G}$ and $R_{\rm DS}$ (Fig. 4) are compared in Fig. 6a. This result shows that for the PI/SiN_x/SiO₂ package, the gate leakage current $I_{\rm G}$ and the baseline noise $R_{\rm DS}$ presented a weak negative correlation between -0.62 and 0 with any quiescent working points of $V_{\rm G}$ from 0 V to -3.8 V. However, for the SiN_x/SiO₂ package, the gate leakage current $I_{\rm G}$ had a strong positive correlation of 0.83 with the baseline noise $R_{\rm DS}$ with $V_{\rm G} = 0$ V.

To illustrate the mechanism causing this difference in the correlations of two types of package materials, the steady-state values of I_G , excluding the capacitance effect under different V_G voltage stresses, are plotted in Fig. 6b. For the PI/SiN_x/SiO₂ package, the $I_G - V_G$ curve obeyed Ohm's Law:

$$J = en\mu E = en\mu V/a \tag{1}$$

where *e* is the charge of an electron, *n* is the intrinsic carrier density, μ is the carrier mobility, *E* is the electric field of the current, *V* is the voltage, and *a* is the thickness of the material. This indicated that the high-resistance





package layer completely blocked the contact between the metal and the solution, and most of the potential between the source/drain metals and the gate reference electrode fell on the package layer. The gate leakage current was dominated by the package layer featuring ohmic characteristics; this finding indicated that there were no external carriers injected into the package layer, and only the internal carriers were driven by the V_G voltage stress to form the leakage current I_G . At this time, the leakage current level was not strong enough to cause a significant voltage fluctuation at the open gate area of the device;

thus, the $R_{\rm DS}$ baseline was not strongly influenced by the $I_{\rm G}$, so the correlation between $I_{\rm G}$ and the background baseline $R_{\rm DS}$ was weak.

For the SiN_x/SiO_2 package, the I_G-V_G curve obeyed the Butler–Volmer Law:

$$J = J_0 \left[\exp\left(-\frac{\alpha n F \eta}{RT}\right) - \exp\left(\frac{\beta n F \eta}{RT}\right) \right]$$
(2)

where J_0 is the exchange current density, R is the ideal gas constant, T is the absolute temperature, n is the number



ranging from 0.1 ppt to 1 ppb, using Device B as the transducer and anti-BNP immobilized on the magnetic beads. The inset is the optical microscope (OM) top view of the AlGaN/GaN device immobilized with magnetic beads. **b** $\Delta R_{DS-4probe}$ results of BNP detection with the Kelvin connection technique and $V_G = -3.8$ V. **c** Transconductance of Device B and its SNR versus different V_G biases of the reference electrode. **d** Comparison of the LOD values for the Au-electrode, Device A using the two-probe method, Device A using the Kelvin connection technique, and Device B biased at the optimal SNR quiescent working point ($V_G = -3.8$ V), using the Kelvin connection technique.



of electrons participating in the reaction, *F* is the Faraday constant, α is the transfer coefficient of the oxidation reaction, β is the transfer coefficient of the reduction reaction, and η is the overpotential of the electrochemical

reaction. This indicated that the SiN_x/SiO_2 package failed to thoroughly protect the source/drain metals from the solution. There were local areas of metal in direct contact with the solution. At this time, the V_G mainly fell on the

interface between the metal and the solution, which led to the overpotential η . The electrochemical reaction was driven by η_1 and the rate of the electrochemical reaction became the dominant factor in gate leakage current I_G at this time. The electrochemical reaction rate was also related to the surface state at the interface, the concentrations of reactants, the convection velocity of the solution, and other factors, so there were large fluctuations in I_{G} . Although only a small part of the metal was in contact with the solution, the $I_{\rm G}$ was much larger with this packaging system than that in the PI/SiN_x/SiO₂ package. This fluctuating leakage current $I_{\rm G}$ flowed through the solution resistance and formed a fluctuating voltage drop on the open gate area of the device, which was further reflected in the device baseline as the R_{DS} fluctuation, in other words, as the background noise. When I_G decreased (the absolute value increased), the open gate voltage of the device increased, so the channel resistance R_{DS} decreased. As a result, we found that there was a strong positive correlation between $I_{\rm G}$ and $R_{\rm DS}$ for the SiN_x/SiO₂ package.

Consequently, the quality of the packaging material affects the leakage current on the reference electrode and then affects the background noise of the device. If the packaging material is perfect and the leakage current on the reference electrode obeys Ohm's law, then I_G and R_{DS} show weak correlations, and other effects dominate the background noise. On the other hand, if the packaging material is poor, a local area of the metal electrode is in contact with the solution, and I_G-V_G obeys the Butler–Volmer Law. Then, I_G and R_{DS} show a strong positive correlation, and the leakage current dominates the background noise. Therefore, high-quality packaging not only increases the lifetime of the device and enlarges the safe operating area but also reduces the background noise of the device, thereby increasing its LOD.

In summary, the LODs for BNP detection by the Au electrode, Device A using the two-probe method, Device A using the Kelvin connection technique, and Device B using

magnetic beads as the sensitive membrane are compared in Fig. 5d. Compared with the Au electrode, the AlGaN/GaN FET device, which was made with exactly the same functionalization process, improved the BNP LOD from 2.73 ppb to 0.47 ppb. The Kelvin connection technique designed in this work was proven to effectively reduce the background noise and increase the LOD to 1.29 ppt, which was lower than the cutoff concentration for HF disease. This method can be used not only in the AlGaN/GaN device but also in any other kind of FET sensor. The quality of the package was very important to the AlGaN/GaN sensor, since it can affect the magnitude of the leakage current to the reference electrode and thereby influence background noise. The optimal SNR was also shown in this work. It was found that as long as the package effectively protected the metal from undergoing electrochemically reactions with the solution, the optimal SNR quiescent operating point roughly coincided with the peak $g_{\rm m}$ point. Biasing the device at the optimal SNR working point led to an extremely low LOD of 0.097 ppt. Table 1 compares the LODs exhibited by various immunosensors for various proteins. Table 1 also shows comparisons of the LOD for BNP detection in this work (Device B) with LODs of other sensors used to detect BNP, AlGaN/GaN sensors used to detect other proteins with a similar method (antigen antibody specific binding) and other two-dimensional material devices and nanodevices. Compared with the electrochemical sensors described in references^{33,34}, the LOD is this work is more than 40 times smaller. Compared with other AlGaN/GaN immunosensors in references 35-40, the LOD is more than 3 orders of magnitude lower. Compared with the graphene sensor and the silicon nanowire in references^{36,37}, the LOD is approximately 4 orders of magnitude lower.

Materials and methods

Surface functionalization and BNP detection

For the Au electrode, the first step was to perform surface activation in a $0.1 \text{ M H}_2\text{SO}_4$ solution with a cyclic

Transducer	Bioprobe	Target molecule	LOD	Refs.
AlGaN/GaN	Anti-BNP on microbeads	BNP	97 fg/mL	This work
Screen-printed carbon electrodes	Peroxidase-labeled BNP antibodies on gold nanoparticles	BNP	4 pg/mL	33
Silver disk electrode	Acetylcholinesterase-labeled anti-BNP antibodies	BNP	10 ng/mL	34
AlGaN/GaN HEMT	NT-proBNP specific aptamer	NT-proBNP	0.22 ng/mL	35
AlGaN/GaN HEMT	FHC antibody	Protein-peptide	56.7 ng/mL	38
AlGaN/GaN HEMT	Botulinum antibody	Botulinum toxin	1 ng/mL	39
AlGaN/GaN HEMT	Anti-NT-proBNP	NT-proBNP	181 pg/mL	40
Graphene	Human anti-EGP	EGP	1 ng/mL	36
Silicon nanowire	Anti-APOA1	hAPOA1	1 ng/mL	37

 Table 1
 Comparison of LODs for detection of different proteins by different transducer platforms

voltammetry (CV) sweep. Then, AuNPs (Au nanoparticles) were electroplated on the Au electrode with a constant V = -0.2 V sweep for 200 s in a 0.25-mM chloroauric acid solution. Subsequently, the Au electrode was incubated in 10 µg/mL anti-BNP in a 37 °C incubator for 3 h. The Au electrode was rinsed with PBST solution (PBS:Tween-20 = 1000:1) to remove the excess anti-BNP. BSA solution (5 mg/mL in PBS) was used to block sites on the Au electrode for 30 min in a 37 °C incubator and the electrode was again cleaned with PBST. Finally, the Au electrode was incubated in solutions with different concentrations of BNP at 37 °C for 1.5 h. EIS (electrochemical impedance spectroscopy) was measured in a mixed solution containing 2 mM potassium ferricyanide, 2 mM potassium ferrocyanide and 0.1 M KCl after each functionalization step.

For Device A, the functionalization steps before BNP binding were exactly the same as those of the Au electrode. The Ag/AgCl reference electrode was biased at 0 V. A constant voltage of 0.4 V, V_{DS} , was applied between H. F and L. F, and the drain-to-source current I_{DS} was measured with a Keithley (USA) 2602B SMUA. The voltage V_{DS-S} between H. S and L. S was measured with SMUB. I_{DS} and $V_{\text{DS-S}}$ were sampled simultaneously every 500 ms. Traditionally, $I_{\rm DS}$ is used as the output signal to monitor the change in BNP concentration in the solution. For the Kelvin connection technique, $R_{\text{DS-4probe}} = V_{\text{DS-S}}/I_{\text{DS}}$ was monitored as the output signal. Since $V_{\rm DS}$ is a constant, $I_{\rm DS}$ is equivalent to $R_{\rm DS-2probe} = V_{\rm DS}/I_{\rm DS}$. Theoretically, $R_{\text{DS-4probe}} - R_{\text{DS-2probe}}$ should be a constant R_{S} , which is the series resistance in the circuit. Different concentrations of BNP (diluted in 0.01×PBS solution) were spiked onto the FET gate area, and the responses of the $R_{DS-4 \text{ probe}}$ and $R_{\rm DS-2\ probe}$ were monitored.

For Device B, $10 \,\mu\text{L}$ magnetic beads ($30 \,\text{mg/mL}$) were mixed with 10 µL anti-BNP (0.5 mg/mL) and incubated for 6 h at 37 °C. Then, MBs were collected with a permanent magnet, and the supernatant was removed. The magnetic beads were washed 3 times with PBS, and then the binding sites were blocked by immersion in 1 mg/ mL BSA solution for 0.5 h. Finally, magnetic beads with a concentration of 5 mg/mL were added to the surface of Device B and held with an N52 permanent magnet on the back side of the chip. The reason that we did not use the electromagnet was to avoid heat dissipation by the electromagnet, which may influence the temperature of the sensor. In the baseline test with different quiescent working points, the reference electrode was biased from 0 V to -3.8 V (0 V, -2 V, -3 V, -3.5 V, -3.8 V), and the $R_{\rm DS-4probe}$ and the gate leakage current $I_{\rm G}$ were both monitored versus time. In the BNP measurement experiment, the change in $R_{DS-4probe}$ was monitored when different concentrations of BNP were spiked on the open gate area.

All experiments for the 3 types of transducers were repeated at least 3 times to ensure that the results were consistent.

Reagents and materials

The Au-electrode CHI101 was purchased from CH Instruments Ins. Anti-BNP (ab20984) and BNP (ab87200) were purchased from Abcam. Magnetic beads (DynabeadsTM M-280 Tosylactivated) were purchased from Thermo Fisher Scientific.

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Author details

¹College of Electrical Engineering, Zhejiang University, 310027 Hangzhou, China. ²Biosensor National Special Laboratory, Department of Biomedical Engineering, Zhejiang University, 310027 Hangzhou, China. ³Hangzhou Global Scientific and Technological Innovation Center, Zhejiang University, 310027 Hangzhou, China

Author contributions

Experiment, analysis, writing by H.Z.; experiments by Y.G.; conception of the idea, review and editing by S.Y.; review and editing by K.S.; review and editing by P.W. All authors have read and agreed to the published version of the manuscript.

Conflict of interest

The authors declare no competing interests.

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