# Studies on Interaction between Silica Gel and Polymer Blend by Inverse Gas Chromatography

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ABSTRACT: Inverse gas chromatography of columns prepared with polymer blends of poly(ethylene oxide) and poly(methyl methacrylate) in the presence of a pulverized porous inorganic material of silica gel was carried out. From the analysis of subtle changes in the retention diagrams, information on interaction between silica gel and the blends was obtained even in the composition where the transition behavior of the blends is greatly changed by thermal treatment.

KEY WORDS Inverse Gas Chromatography / Polymer Blend / Poly(ethylene oxide) / Poly(methyl

methacrylate) / Silica Gel / Compatibility / Transition Behavior / Thermal Treatment /

Inverse gas chromatography (IGC) is a simple and useful technique to investigate the physical properties of polymers such as glass transition temperature  $(T_{a})$ or melting temperature  $(T_m)$  of a polymer.<sup>1</sup> This technique has been widely used to determine thermodynamic quantities for polymers such as solubility parameters.<sup>2,3</sup> In recent years IGC has also been utilized for polymer surface characterization.<sup>4-8</sup> We applied IGC to the evaluation of the morphological change in hydrophilichydrophobic polymer systems such as polymer blends of poly(ethylene oxide) (PEO) and polystyrene (PS),9 of poly(acrylic acid) and PS,<sup>10</sup> of PEO and poly(methyl methacrylate) (PMMA),<sup>11</sup> and triblock copolymers of PEO and PMMA<sup>12</sup> prepared by anionic polymerization.<sup>13-15</sup> Further, we have succeeded in applying IGC technique to the study on interaction between inorganic materials and polymer.<sup>16,17</sup> Inorganics-polymer interaction is a most interesting subject and many studies have been made by various methods.<sup>18-20</sup>

In a previous paper, we clarified the transition phenomena in PEO/PMMA blends of various compositions by means of IGC.<sup>11</sup> In compositions below ca. 15 wt% PEO, the transition behavior of the blends was mainly dominated by the PMMA component. Above ca. 45 wt% PEO, PEO domains were segregated in the homogeneous polymer matrix and spread out with increase in PEO content. In both regions of composition, fundamental transition behavior of the blends did not change by thermal treatment. In ca. 15-25 wt% PEO, transition behavior was greatly changed by thermal treatment. This composition range corresponded to a critical state of above-mentioned two states. In the previous study, we investigated the effect of the addition of silica gel to the PEO/PMMA blends of 5 and 50 wt% PEO, in which fundamental transition phenomena were unchanged by thermal treatment.<sup>17</sup> Information on interaction between the blends and silica gel was obtained from changes in the retention diagrams of IGC, i.e., silica gel incorporated both PEO and PMMA into its pores and the ability of incorporation of PEO into the pores of silica gel was superior to that of PMMA.<sup>17</sup> To promote IGC technique to one of useful tools for morphological study of multicomponent polymer systems, however, it is of great importance to know whether such information is obtainable even when the blends are morphologically changed by thermal treatment.

In this study, IGC measurements of columns prepared with both PEO/PMMA blends (15—40 wt% PEO) and silica gel were carried out. This paper presents the information on interaction between silica gel and the blend before and after thermal treatment.

## **EXPERIMENTAL**

#### Materials

PMMA was prepared by radical polymerization of methyl methacrylate in benzene at 60°C initiated with  $\alpha, \alpha'$ -azobis(isobutyronitrile) (AIBN). Both PEO (Nacalai Chemical's PEO \$6000,  $M_n$ =8500) and PMMA ( $M_n$ = 46800) were freeze-dried from respective benzene solutions before use. Silica gel (Merck's silica gel 60, BET surface area 537 m<sup>2</sup> g<sup>-1</sup>) was pulverized by dry-grinding in agate mortar for 1 h. Chromosorb P AW-DMCS 60—80 mesh (Shimadzu Co., BET surface area 3 m<sup>2</sup> g<sup>-1</sup>), a good solid support for IGC measurements,<sup>21</sup> was used as a support for the polymer. *n*-Nonane was used as received.

#### Columns

The columns prepared are summarized in Table I. A certain amount of pulverized silica gel was dispersed in a benzene solution (2.5 w/v%) of PEO/PMMA blend by stirring sufficiently, and to this a prescribed amount of Chromosorb was added. The benzene was allowed to evaporate at ambient temperature by gentle and continuous stirring of the solution followed by drying at  $45^{\circ}$ C under slightly reduced pressure. A weighed amount of Chromosorb prepared in this manner was tightly packed into a  $1.5 \text{ m} \times 3 \text{ mm}$  internal diameter stainless-steel column. The column was dried for 5 h at  $45^{\circ}$ C under a constant stream of helium.

#### Measurements

Gas chromatograms were recorded on a Shimadzu GC-8A equipped with a thermal conductivity detector,

 Table I.
 Column specifications

Column No.	PEO content in the blend wt%	Polymer loading <sup>a</sup> wt%	Silica gel loading <sup>b</sup> wt%
2	$0^{d}$	9.7	0
3	15	9.6	0
4	20	9.7	0
5	25	9.8	0
6	35	9.7	0
7	40	9.7	0
8	15	9.9	0.5
9	15	9.6	3.8
10	20	9.9	0.5
11	20	9.6	3.8
12	25	9.9	0.5
13	25	9.6	3.8
14	35	9.9	0.5
15	35	9.6	3.8
16	40	10.0	0.5
17	40	9.8	3.8

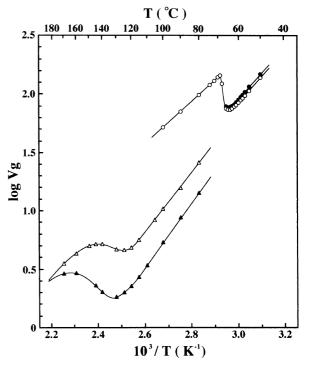
<sup>a</sup> Polymer (g)/[Polymer (g) + Chromosorb (g) + Silica gel (g)] × 100. <sup>b</sup> Silica gel (g)/[Polymer (g) + Chromosorb (g) + Silica gel (g)] × 100. <sup>c</sup> Only PEO was loaded. <sup>d</sup> Only PMMA was loaded.

with helium as the carrier gas, n-nonane as the solute, and air as the noninteracting marker. The method of IGC measurement has been described in previous papers.9,10,12 The gas chromatographic measurement was carried out by increasing the column temperature T (K). The specific retention volume  $V_g$  (ml g<sup>-1</sup>) was calculated from the equation  $V_g = V_N/w$ .  $V_N$  (ml) is the net retention volume of the solute from the air peak and w (g) is the loaded polymer weight in the column. The retention diagram (RD) was obtained by plotting  $\log V_{*}$ vs.  $10^{3}/T$ . Several days after the first measurement on a freshly packed column, the second measurement was carried out to investigate the influence of the thermal treatment on the surface feature of the polymer. The BET surface area of silica gel was measured on a Shibata SA-1000 by one-point N2-adsorption method at liquid nitrogen temperature.

### **RESULTS AND DISCUSSION**

Figure 1 shows the retention diagrams (RDs) of the first measurement (RDs-1st) of the columns No. 1 and 2 together with RDs of the second measurement (RDs-2nd). In a Z-shaped curve, the temperature of the first deviation from linearity corresponds to the transition temperature of the polymer.<sup>1</sup> This temperature remains unchanged after thermal treatment. As can be seen from Figure 1, the  $T_{\rm m}$  of PEO and the  $T_{\rm g}$  of PMMA were about 62 and 115°C, respectively. It should be noted that the value of log  $V_g$  in the RD of PEO at a certain temperature is fairly larger than that in the RD of PMMA. The RD-2nd reflects the thermally-treated phase structure of the polymer. The retention mechanism was reported previously.<sup>1,10,11,21</sup> In brief, the result that the RD-2nd is not so different from the RD-1st is a characteristic of PEO. The result that the value of log  $V_{\sigma}$  in RD-2nd is smaller than that in the RD-1st (downward shift of RD) is a characteristic of PMMA.

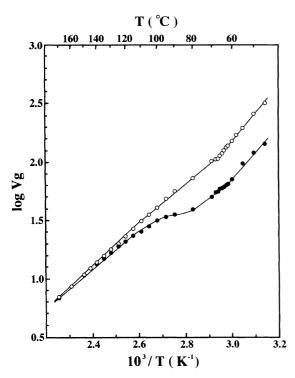
RDs of the third measurements were the same as the



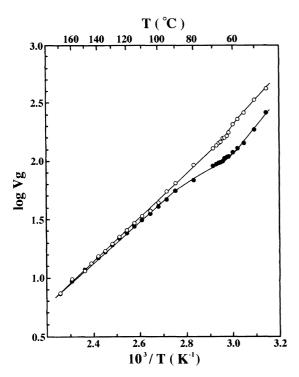
**Figure 1.** Retention diagrams of PEO and PMMA: ( $\bigcirc$ ) column No. 1 (PEO, first measurement); ( $\bigcirc$ ) No. 1 (second); ( $\triangle$ ) No. 2 (PMMA, first); ( $\triangle$ ) No. 2 (second).

respective RDs-2nd. Therefore, it is not necessary to take into account the results of the third measurements to discuss the effects of thermal treatment on phase structure of the polymer.

Figures 2–5 show the RDs of columns No. 3–6 (15-35 wt% PEO) prepared without silica gel. In the RDs of 15 wt% PEO, only slight bendings of the slope were observed at about 60°C and 110°C and a Z-shaped curve did not appear in the RD-1st, whereas a Z-shaped curve was clearly observed at around 80°C in the RD-2nd. In 15 wt% PEO, therefore, the features of PMMA did not appear before thermal treatment but appeared after. In the RDs of 20 wt% PEO was seen similar tendency to that observed in 15 wt% PEO. In the RD-2nd, however, sharpness of the Z-shaped curve was weakened. In the RD-1st of 25 wt% PEO, a very slight bending of the slope was observed at about 60°C. In the RD-2nd of 25 wt% PEO, the temperature of the bending was raised to about 70°C and a small downward shift of RD was yet observed, which indicates features of PMMA somewhat to appear by thermal treatment. In 35 wt% PEO, the RD-1st and RD-2nd were almost linear and overlapped. These results mean that the blend is a homogeneous polymer system which exhibits no transition phenomenon and the features of it are mainly governed by PEO. The RDs of 40 wt% PEO were completely the same as those of 35 wt% PEO. Detailed results are reported in a previous paper.<sup>11</sup> The composition range of 15-25 wt% PEO is considered to be a critical state of the two homogeneous states, *i.e.*, PMMA-predominant state(below *ca.* 15 wt% PEO) and PEO-predominant state(above ca. 35 wt% PEO). The results of IGC measurements of columns prepared with both the blends of this composition range and silica gel are described below.

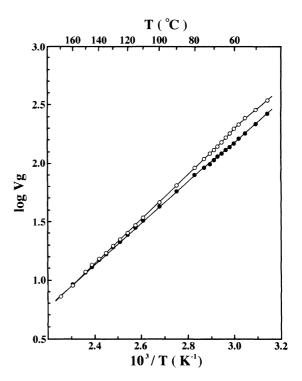


**Figure 2.** Retention diagrams of column No.  $3(15 \text{ wt}\% \text{ PEO}, \text{ without silica gel}): (<math>\bigcirc$ ) first measurement; ( $\bigcirc$ ) second.

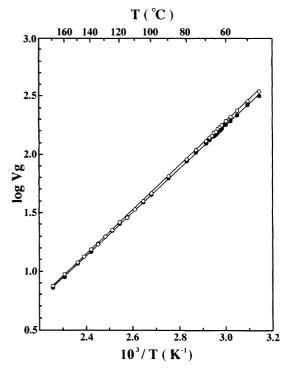


**Figure 3.** Retention diagrams of column No. 4 (20 wt% PEO, without silica gel):  $(\bigcirc)$  first measurement;  $(\bigcirc)$  second.

To interpret the following results a model for adsorption sites for the solute of *n*-nonane on Chromosorb was proposed in previous papers<sup>16,17</sup> and is shown in Figure 6. Three adsorption sites were considered in the retention mechanism: the surface of polymer which covers the Chromosorb surface (site A); the uncovered surface of porous inorganic material of silica gel (site B); the polymer-covered moiety of silica gel where all the pores are filled with polymer (site C). Since the



**Figure 4.** Retention diagrams of column No. 5 (25 wt% PEO, without silica gel):  $(\bigcirc)$  first measurement;  $(\bigcirc)$  second.



**Figure 5.** Retention diagrams of column No. 6 (35 wt% PEO, without silica gel): ( $\bigcirc$ ) first measurement; ( $\bigcirc$ ) second.

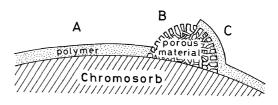


Figure 6. A model for adsorption sites for *n*-nonane.

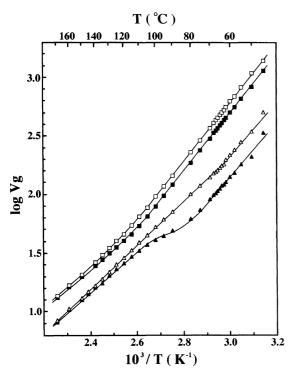
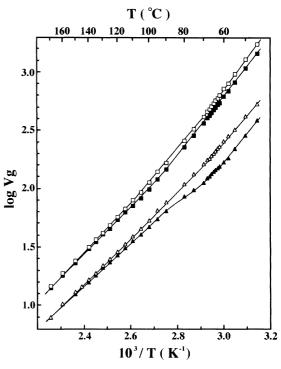


Figure 7. Retention diagrams of PEO/PMMA blends with silica gel: ( $\triangle$ ) column No. 8 (15 wt% PEO, 0.5 wt% silica gel, first measurement); ( $\blacktriangle$ ) No. 8 (second); ( $\square$ ) No. 9 (15 wt% PEO, 3.8 wt% silica gel, first measurement); ( $\blacksquare$ ) No. 9 (second).

grain size of Chromosorb was fairly larger than that of silica gel, the surface area of polymer at site A is considered to be much larger than that at site C. The adsorption-desorption of the solute (*n*-nonane) at site A, therefore, mainly governs the features of retention diagrams. The adsorption of *n*-nonane at the surface of silica gel (site B) is much stronger than that of polymer. The existence of site B, therefore, brings about increase in retention volume of the solute in gas chromatography, which results in upward shift of RD. A large amount of site C corresponds to decrease in amount of polymer at the site A, which changes fundamentally the feature of RD.

Figure 7 shows the RDs of columns No. 8 and 9 (15 wt% PEO, with silica gel). In the RD-1st of 0.5 wt% silica gel, the bending at about  $60^{\circ}C$  became much slighter and that at about 110°C disappeared. This is due to decrease in amount of PEO and PMMA at site A as a result of incorporation of polymer into pores of silica gel (site C). In the RD-2nd of 0.5 wt% silica gel, a Z-shaped curve appeared at around 80°C as well as in the case of non-addition of silica gel. The addition of silica gel, therefore, does not prevent the appearance of features of PMMA by thermal treatment. The RDs of 3.8 wt% silica gel depicted straight lines and weak curves below and above about 105°C, respectively. Linearity at around 60°C, which corresponds to the  $T_{\rm m}$  of PEO, means incorporation of most of PEO into pores of silica gel. If only PEO is selectively incorporated into pores of silica gel similarly to the blend of PEO and



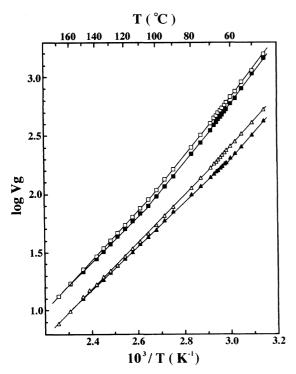
**Figure 8.** Retention diagrams of PEO/PMMA blends with silica gel:  $(\triangle)$  column No. 10 (20 wt% PEO, 0.5 wt% silica gel, first measurement); ( $\triangle$ ) No. 10 (second); ( $\square$ ) No. 11 (20 wt% PEO, 3.8 wt% silica gel, first measurement); ( $\blacksquare$ ) No. 11 (second).

PS,<sup>16</sup> the composition of PMMA at site A will increase more than 85 wt% PMMA and consequently a Z-shaped curve should appear at around 110°C in the RD of higher silica gel content. As can be seen from Figure 6, however, no Z-shaped curve was observable in the RDs of 3.8 wt% silica gel. This indicates that both PEO and PMMA were incorporated into pores of silica gel. Since the absolute amount of PMMA at site A was small, the RDs at around 105°C did not depict Z-shaped curves but weak curves in 3.8 wt% silica gel.\*<sup>1</sup> Downward shift of RDs indicates that the transition behavior of the blend is mainly governed by PMMA. Upward shift of RDs with the increase in amount of silica gel is due to an increase in amount of site B.

In Figure 8 are shown the RDs of columns No. 10 and 11 (20 wt% PEO, with silica gel). Fundamental tendency is the same as is in the case of 15 wt% PEO. In the RDs of 3.8 wt% silica gel, the shape of RDs at around  $105^{\circ}$ C changed from weak curves to very slight bendings. This is ascribed to a decrease in amount of PMMA in the column of 20 wt% PEO compared to that of 15 wt% PEO. Downward shift of RD-2nd, however, shows the existence of PMMA at site A.

Figure 9 depicts the RDs of columns No. 12 and 13 (25 wt% PEO, with silica gel). In the RD-1st of 25 wt% PEO without silica gel, a very slight bending of the slope was observable at around 60°C, whereas the temperature shifted to about 70°C in the RD-1st of 25 wt% PEO with 0.5 wt% silica gel. This means the appearance of features of PMMA in the blend and suggests that the composition of silica gel. In the RD-1st of 3.8 wt% silica gel, a slight bending of the slope emerged at around 105°C in addition to that at around 70°C. These bendings became

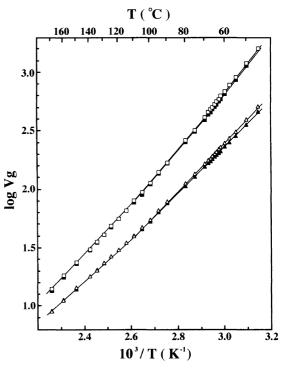
<sup>\*1</sup> From our unpublished results, low loading of PMMA on Chromosorb resulted in the RD of a weak curve and also in no Z-shaped curve.



**Figure 9.** Retention diagrams of PEO/PMMA blends with silica gel:  $(\triangle)$  column No. 12 ( 25 wt% PEO, 0.5 wt% silica gel, first measurement); ( $\blacktriangle$ ) No. 12 (second); ( $\square$ ) No. 13 (25 wt% PEO, 3.8 wt% silica gel, first measurement); ( $\blacksquare$ ) No. 13 (second).

somewhat clearer in the RD-2nd. The emergence of the bendings at around 105°C indicates that the features of PMMA clearly appeared at site A. If ability of incorporation of PMMA is identical with that of PEO, the composition of the blend at site A is constant (25 wt% PEO=75 wt% PMMA) and the bendings of the slope at around 70°C and 105°C in RD is expected not to be observed. However, they were observed at around respective temperatures. Therefore, it is concluded that ability of incorporation of PEO into the pores of silica gel is superior to that of PMMA. In contrast silica gel selectively incorporated PEO into the pores in the PEO/PS blends.<sup>16</sup>

The RDs of columns No. 14 and 15 (35 wt% PEO, with silica gel) are shown in Figure 10. In this composition without silica gel, two components are completely compatible and the transition behavior of the blend is mainly dominated by PEO component.<sup>11</sup> As can be seen from the RDs of 0.5 wt% silica gel, slight bendings of the slopes were observed at around 110°C. These appearance of the bendings are due to an increase in composition of PMMA brought by preferential incorporation of PEO into the pores of silica gel. Further, in the RDs of 3.8 wt% silica gel, slight bendings of the slopes were seen at around 70°C in addition to that appeared at around 110°C. The RDs of 3.8 wt% silica gel became analogous to the RDs of the column prepared by less PEO content (ca. 20 wt% PEO). These results are consistently explained on the basis of the preferential incorporation of PEO into the pores of silica gel. In the RDs of 40 wt% PEO (columns No. 16 and 17, with silica gel), almost the same results were obtained as were in the RDs of 35 wt% PEO.



**Figure 10.** Retention diagrams of PEO/PMMA blends with silica gel:  $(\triangle)$  column No. 14 (35 wt% PEO, 0.5 wt% silica gel, first measurement); ( $\blacktriangle$ ) No. 14 (second); ( $\square$ ) No. 15 (35 wt% PEO, 3.8 wt% silica gel, first measurement); ( $\blacksquare$ ) No. 15 (second).

### CONCLUSIONS

In PEO/PMMA blends, porous inorganic material of silica gel incorporated not only PEO but PMMA into its pores and the ability of incorporation of PEO into the pores of silica gel was superior to that of PMMA. This information has already been obtained for the blends of 5 and 50 wt% PEO where compatibility of both components was basically unchanged by thermal treatment.<sup>17</sup> The same information was obtained even for the blends where the transition behavior is greatly changed by thermal treatment. As described above, IGC is a simple, sensitive and useful technique and will be widely applicable to studies of many multicomponent polymer systems. Especially, delicate change in the transition behavior by thermal treatment can be easily detected.

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