Polymer Journal, Vol. 7, No. 5, pp 588-590 (1975)

SHORT COMMUNICATION

Structure and Properties of Highly Cross-Linked Polymers

Kenkichi MURAKAMI and Sumio TAKASUGI

The Chemical Research Institute of Non-Aqueous Solutions, Tohoku University, Sendai, Japan. (Received March 17, 1975)

KEY WORDS Crosslinkages / Isotropic Network / Poly(oxyethylene) / Semi-Primary Bonds /

Tetrafunctional cross-linked polymers can generally be divided into three types, as shown in Figure 1, assuming that \bar{n}_c is the chain length of a crosslinkage, and \bar{n}_m is that between two cross-linkages. Figure 1a is considered to be the most general case for tetrafunctional crosslinked polymers. Z is the index showing the functionality of the cross-linking agent; Z=2in this case.

Z=3 in the case of $\bar{n}_{\rm m} \approx \bar{n}_{\rm c}$, as shown in Figure 1b and Z will approach unity as $\bar{n}_{\rm m} < \bar{n}_{\rm c}$, *i.e.*, as the cross-linked polymer becomes more tight, as shown in Figure 1c.

It is well known that eq 1 is applicable for the rubbery region of ideally Affine deformed network polymers.¹

$$G = \frac{f}{\alpha - \alpha^{-2}} = \nu(0)RT \qquad (1)$$

Here, G is the shear modulus, f the stress at relative length, and $\nu(0)$ the initial number of effective network chains per cubic centimeter.

R and T are, respectively, the gas constant and the absolute temperature.

For tightly cross-linked polymers and their special structures,² eq 1 should be modified to eq 2.

$$f = \frac{\overline{r_{0}^{2}}}{\overline{r_{0}^{2}}} \nu(0) R T(\alpha - \alpha^{-2})$$
 (2)

Here, $\overline{r^2}$ is the mean-square end-to-end separation of a chain in the isotropic network, and $\overline{r_0^2}$ is the mean-square end-to-end separation of a chain in the absence of network constraint.

Equation 3 was recently suggested by Smith for such tightly cross-linked polymers.³

$$\frac{\nu(0)RT}{G} = \frac{1}{\Phi} - \frac{6\bar{C}_n}{5q^2n}$$
(3)

Here Φ is the front factor, $\Phi = \overline{r^2}/\overline{r_0^2}$. \overline{C}_n and q are values which will be shown by the following relations.

For a free chain having n backbone bonds of length l, eq 4 and 5 can be employed:



Figure 1. (a) Cross-linking mechanism for $\bar{n}_m > \bar{n}_c$; (b) cross-linking mechanism for $\bar{n}_m \approx \bar{n}_c$; (c) cross-linking mechanism for $\bar{n}_m < \bar{n}_c$.

$$\overline{r_0^2} = C_n n l^2 \tag{4}$$

$$r_{\rm m} = qnl$$
 (5)

where the characteristic ratio⁴ C_n is a function of *n* when *n* is small. For example, C_n for poly(oxyethylene) essentially equals its asymptotic value C_{∞} when n=50, but C_n decreases rapidly with a decrease of *n* when *n* is less than about 25.

For ethyl acrylate—dimethacrylate networks, C_n is closely represented by eq 6.

$$C_n = n^{0.57}$$
 for $1 \le n \le 20$ (6)

q is, in general, a dimensionless factor determined by bond angles and lengths.

As it is very clear that eq 1 is not applicable for such tightly cross-linked polymers, the value of $\nu(0)$ obtained by eq 1 is now designated as $\nu_{\rm M}(0)$, which means the apparent value for these polymers. Therefore, from eq 1 and 3, eq 7 is derived.

$$\frac{\nu_{\text{real}}(0)}{\nu_{\text{M}}(0)} = \frac{1}{\Phi} - \frac{6\bar{C}_n}{5q^2n}$$
(7)

Where, $\nu_{real}(0)$ is the real cross-linking density of such tightly cross-linked polymers.

For a chain-containing only carbon—carbon single bonds, q equals 0.83. Substituting this value of q and eq 6 into eq 7, eq 8 is obtained.

$$\frac{\nu_{\text{real}}(0)}{\nu_{\text{M}}(0)} = \frac{1}{\Phi} - \frac{6}{5(0.83)^2 n^{0.43}} \tag{8}$$

Here, $\phi = 0.5$ is used in eq 8 for those tightly cross-linked polymers whose polymerization degree, between two cross-linkages, is $n=10-20.^{3}$

For measuring the cross-linking density of amorphous polymers, there are in general two kind of methods. One is based upon eq 1, which is not applicable for tightly cross-linked polymers, and the other uses the swelling method derived by Flory and Rehner.⁵ The cross-linking density obtained by the latter is signified as $\nu_{s}(0)$.

The relation between $\nu_{\rm M}(0)$ and $\nu_{\rm S}(0)$ for vulcanized natural rubber, is depicted in Figure 2. From this figure, it will be observed that $\nu_{\rm M}(0)$ is larger than $\nu_{\rm S}(0)$ below a certain point (for example, $\nu_{\rm M}(0) \approx 4.2 \times 10^{-4}$ mol/cc for natural rubber vulcanizates), and once over that point, $\nu_{\rm M}(0)$ is smaller than $\nu_{\rm S}(0)$, independent of the

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Figure 2. The relation of $\nu_M(0) vs. \nu_S(0)$ and $\nu_{real}(0) vs. \nu_S(0)$ for natural rubber vulcanizates: \bigcirc , $\nu_M(0) vs. \nu_S(0)$; \bigoplus , $\nu_{real}(0) vs. \nu_S(0)$.

kind of polymers and solvents used for the swelling measurement.

Hereafter the cross point between the curve and the straight line of slope=1 is called *P*.

The fact that $\nu_{\rm M}(0)$ is larger than $\nu_{\rm S}(0)$ in the range where the cross-linking density $\nu(0)$ is lower than *P* as seen in Figure 2 is considered to be due to $\nu_{\rm M}(0)$, which usually involves a number of entanglements which are surrounded with the real cross-linkages and then regarded as the primary bonds⁶ and strong dipole groups⁷ of the apparent primary bonds. Some of these semiprimary bonds will probably not contribute to $\nu_{\rm S}(0)$.

The reason why it will be $\nu_{\rm S}(0) > \nu_{\rm M}(0)$ in the range of $\nu(0) > P$, however, remained unsolved in our previous report.⁶ By using the value of $\nu_{\rm real}(0)$ from eq 8 instead of $\nu_{\rm M}(0)$ for tightly cross-linked polymers ($\nu(0) > P$), the relation between $\nu_{\rm real}(0)$ and $\nu_{\rm S}(0)$ for natural rubber vulcanizates was depicted as shown in Figure 2. As is clearly seen from this result, the tendency of $\nu_{\rm M}(0) > \nu_{\rm S}(0)$ was observed even in the range of $\nu(0) > P$: the reason was satisfactorily explained in the case of $\nu(0) < P$ described above.

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