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## Tunable Twin Matching Frequency ( $f_{m1}/f_{m2}$ ) Behavior of $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4/\text{NBR}$ Composites over 2–12.4 GHz: A Strategic Material System for Stealth Applications

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The gel to carbonate precipitate route has been used for the synthesis of  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x = 0, 0.25, 0.5$  and  $0.75$ ) bulk inverse spinel ferrite powder samples. The optimal zinc (50%) substitution has shown the maximum saturation magnetic moment and resulted into the maximum magnetic loss tangent ( $\tan\delta_m$ )  $> -1.2$  over the entire 2–10 GHz frequency range with an optimum value  $\sim -1.75$  at 6 GHz.  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$ -Acrylo-Nitrile Butadiene Rubber (NBR) composite samples are prepared at different weight percentage (wt%) of ferrite loading fractions in rubber for microwave absorption evaluation. The 80 wt% loaded  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4/\text{NBR}$  composite (FMAR80) sample has shown two reflection loss (RL) peaks at 5 and 10 GHz. Interestingly, a single peak at 10 GHz for 3.25 mm thickness, can be scaled down to 5 GHz by increasing the thickness up to 4.6 mm. The onset of such twin matching frequencies in FMAR80 composite sample is attributed to the spin resonance relaxation at  $\sim 5$  GHz ( $f_{m2}$ ) and destructive interference at  $\lambda_m/4$  matched thickness near  $\sim 10$  GHz ( $f_{m1}$ ) in these composite systems. These studies suggest the potential of tuning the twin frequencies in  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4/\text{NBR}$  composite samples for possible microwave absorption applications.

Microwave absorbing materials are important in the present war scenario to reduce the Radar Cross Section (RCS) for strategic airborne objects<sup>1</sup>. These materials also important for applications in civil sector viz. communication interference between electronic devices, antenna background clutters etc. Various dielectric, magnetic and carbonaceous materials, such as barium titanate<sup>2</sup>, core-shell materials<sup>3</sup>, carbon black<sup>4</sup>, carbonyl iron<sup>5,6</sup>, carbon nanotubes (CNTs)<sup>7</sup>, iron oxide<sup>8</sup> and ferrites<sup>9,10</sup> etc. are being investigated as the functional filler materials for microwave absorption applications. There are continuous efforts to achieve the enhanced wide band MW absorption properties by converting the materials in different geometries viz. ferrite nanofibers<sup>11</sup>, porous hollow microrods<sup>12</sup>, nested structure<sup>13</sup> etc. Further, among these, ferrite materials provide several advantages such as relatively smaller values of absorber thickness, particularly for lower frequencies in the MW region, tunability of ferromagnetic resonance (FMR)<sup>14</sup>, excellent environmental stability, etc. in comparison to the dielectric materials.  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  inverse spinel ferrite system attracted special attention because of possible tunable electrical<sup>15,16</sup>, magnetic<sup>17,18</sup>, and microwave absorption properties<sup>19–22</sup> by modulating the magnetic interaction at magnetic ion sites.  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  (at  $x = 0$ ) having the inverse spinel structure of  $(\text{Fe}^{3+})^{\text{tet}}[\text{Ni}^{2+}, \text{Fe}^{3+}]^{\text{oct}}\text{O}_4$  with cation's antiparallel spin arrangements at tetragonal (A) and orthogonal (B) sites gives rise to the magnetic properties due to the superexchange interaction between A and B sites mediated through  $\text{O}^{2-}$  ions. The net magnetization ( $M_T$ ) in Ni-Zn ferrite system is the result of the difference of magnetization at octahedral ( $M_B$ ) and tetrahedral sites ( $M_A$ ) giving rise to the ferrimagnetism. The spin arrangement in Ni-Zn system can be altered by substituting  $\text{Zn}^{2+}$  ions, replacing  $\text{Fe}^{3+}$  ions at the tetragonal sites  $(\text{Zn}_x\text{Fe}_{1-x}^{3+})^{\text{tet}}[\text{Ni}_{1-x}^{2+}, \text{Fe}_{1+x}^{3+}]^{\text{oct}}\text{O}_4$ . This substitution results in the significant change of magnetic interaction and thus magnetic properties<sup>23,24</sup>. The absorption frequencies of these

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ferrite materials depend on the electron spin arrangement and also on the domain spin orientations. The incident microwave radiation can be absorbed in ferrite materials by exciting spin relaxation process, which may be transferred to host lattice due to spin-lattice coupling. The spin-lattice interaction<sup>25</sup> in spinel ferrites, which strongly affects MW absorption characteristics, depends on the distribution of cations in the crystal structure, which is not only decided by the chemical composition and synthetic route but also by the other parameters including pH of chemical reactions<sup>26</sup>, annealing temperature, the rate of heating/cooling, etc.

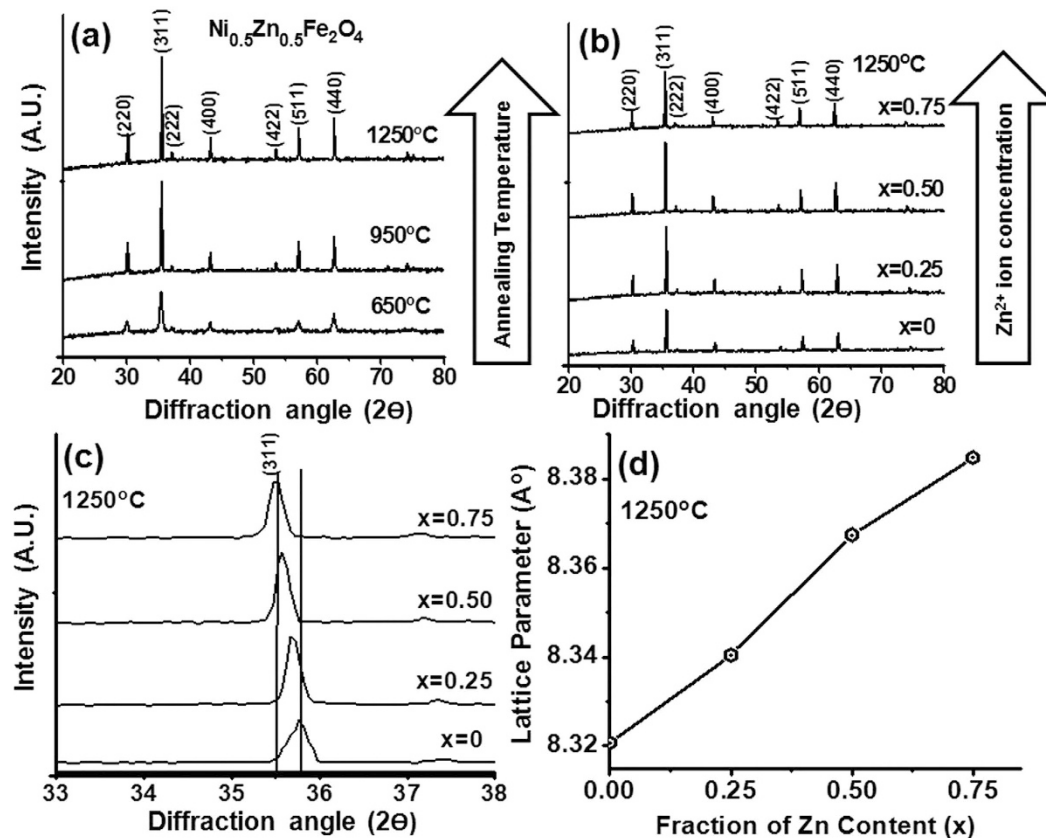
The ferrite materials need to be dispersed in suitable binder resin matrix to realize the practical microwave absorbing products. Therefore, studies on MW absorbing composites with dispersed magnetic ferrite materials in polymer/resin matrix has always been a subject of interest<sup>27</sup>. Dispersion of ferrite granules has been attempted in different host matrices viz. epoxy resin<sup>28,29</sup>, polyvinylchloride (PVC)<sup>30</sup>, wax<sup>31,32</sup> etc., wherein the studies have been focused on understanding the variation of electromagnetic characteristics of composites with a loading percentage of filler materials as well as their dispersion behavior. Further, the filler-host matrix interactions facilitate multiple scattering of MW radiation via suspended filler granules which may significantly enhance the MW absorption properties in the composites<sup>33</sup>. Yet, there are numerous challenges in the synthesis of homogeneous composite system e.g. dispersion/suspension of the high-density ferrite powder in liquid resin/wax medium leading to the inhomogeneities in the composites. The elastomeric matrix may provide a relatively better host for uniform dispersion of high-density filler due to the entrapment of heavy ferrite granules in cross-linked rubber structure during mixing and vulcanization process<sup>34</sup>. In spite of these advantages, there are very few studies on ferrite-elastomeric composites, directing to microwave absorption. Considering these advantages, in this report, we have focused our studies on the microwave absorbing properties of  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ferrite as filler in Acrylo-Nitrile Butadiene Rubber (NBR) elastomeric matrix due to its light weight, flexible nature, high elongation, resistance to the corrosion, good high/low temperature stability ( $-20\text{ }^\circ\text{C}$  to  $+125\text{ }^\circ\text{C}$ ) and high values of tensile strength.  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x = 0, 0.25, 0.50$  and  $0.75$ ) ferrite powders have been prepared using simple, scalable and energy efficient wet chemical method. As synthesized powders have been annealed at different temperatures to study their size-dependent physical and microwave absorption properties. Flexible sheets were fabricated in NBR host matrix with different loadings fractions in the range of 50–80 weight percent (wt%) of the Ni-Zn ferrite material with optimal Zn concentration showing maximum saturation magnetization and investigated for their reflection loss characteristics in the microwave frequency range of 2–12.4 GHz.

## Results and Discussion

The representative XRD spectra are shown in Fig. 1a for  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x = 0.50$ ) ferrite powder sample, annealed at  $650\text{ }^\circ\text{C}$ ,  $950\text{ }^\circ\text{C}$  and  $1250\text{ }^\circ\text{C}$  temperatures. International Centre for Diffraction Data (ICDD) powder diffraction file (PDF) # 22-106 has been used as a reference for phase identification and all the observed diffraction peaks could be indexed with this reference. The appearance of characteristics spinel phase peaks due to (220), (311), (222), (400), (422), (511) and (440) planes, marked in Fig. 1a, confirm the formation of pure spinel phase of  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  annealed at  $650\text{ }^\circ\text{C}$ . The broadening of XRD peaks for  $650\text{ }^\circ\text{C}$  annealed powder suggests the formation of ultrafine particles. Further, enhancement of intensities and decrease of respective broadening for these diffraction peaks have been observed with the increase in sequential annealing temperatures at  $950\text{ }^\circ\text{C}$  and  $1250\text{ }^\circ\text{C}$ , respectively. The other compositions of  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x = 0, 0.25$  and  $0.75$ ) ferrite powders showed similar XRD spectra (Fig. 1b). However, the diffraction peaks are relatively shifted  $\sim 0.26^\circ$  in  $2\theta$  towards lower angle with an increase in  $\text{Zn}^{2+}$  ion concentration from  $\text{NiFe}_2\text{O}_4$  to  $\text{Ni}_{0.25}\text{Zn}_{0.75}\text{Fe}_2\text{O}_4$  as shown in Fig. 1c, attributed to the enlargement of cubic lattice parameter 'a' for these inverse spinel compounds from  $8.321\text{ \AA}$  for pure Ni ferrite ( $x = 0$ ) to  $8.385\text{ \AA}$  for  $\text{Ni}_{0.25}\text{Zn}_{0.75}\text{Fe}_2\text{O}_4$  ferrite ( $x = 0.75$ ) composition, as shown in Fig. 1d. The increased 'a' with  $\text{Zn}^{2+}$  ion concentration is caused by the replacement of  $\text{Ni}^{2+}$  ion (ionic radii  $\sim 0.78\text{ \AA}$ ) to the large sized  $\text{Zn}^{2+}$  ion (ionic radii  $\sim 0.83\text{ \AA}$ ) in the crystal lattice of cubic  $\text{NiFe}_2\text{O}_4$  structure<sup>35-37</sup>.

Scanning electron microscope (SEM) micrographs are shown in Fig. 2a,b, for  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  powders ( $x = 0$  and  $0.5$ ), annealed at  $650\text{ }^\circ\text{C}$ ,  $950\text{ }^\circ\text{C}$  and  $1250\text{ }^\circ\text{C}$ . Ferrite powder samples, annealed at  $650\text{ }^\circ\text{C}$ , show fine microstructure with spherical particle morphology, Fig. 2a(i). The grain growth has been observed with annealing temperature, resulted into the distorted spherical morphology observed for the powder samples, annealed at  $1250\text{ }^\circ\text{C}$ , Fig. 2a(iii).  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x = 0.50$ ) showed larger grain size with fused particles, as shown in Fig. 2b (iii). This observation indicates that the addition of Zn promotes the grain growth in  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ferrite composition. The results are consistent with the reported literature<sup>38</sup>.

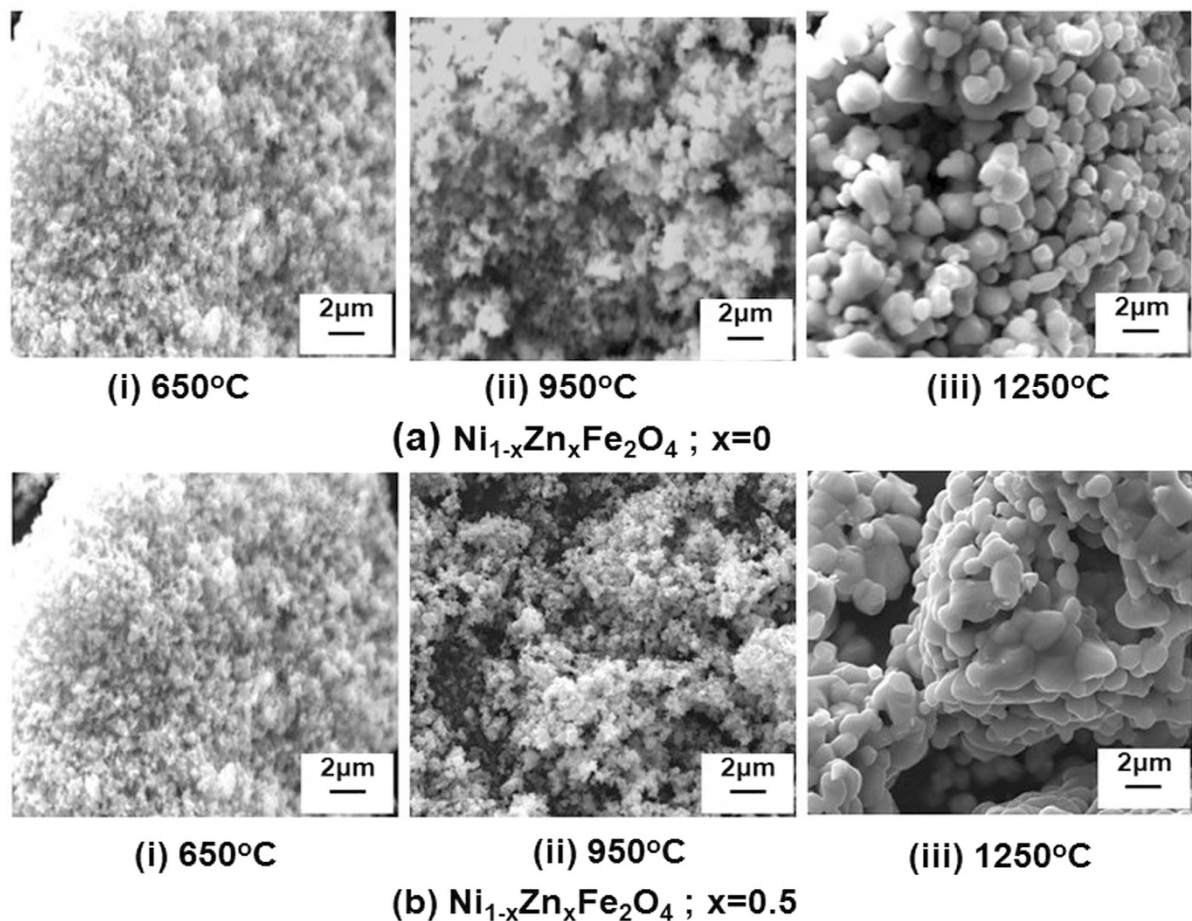
The room temperature field dependent magnetic measurements are summarized in Fig. 3a–d for  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x = 0, 0.25, 0.50$  and  $0.75$ ) ferrite powders annealed at  $650\text{ }^\circ\text{C}$ ,  $950\text{ }^\circ\text{C}$  and  $1250\text{ }^\circ\text{C}$ . All these compositions show ferrimagnetic behavior with different saturation magnetization ( $M_s$ ) and coercive field ( $H_c$ ) values. The variation of  $M_s$  and  $H_c$  with respect to annealing temperature and  $\text{Zn}^{2+}$  ion concentration and composition are plotted in Fig. 3e and f respectively. The saturation magnetization increases with increasing the annealing temperature for all these compositions except for the  $\text{Ni}_{0.25}\text{Zn}_{0.75}\text{Fe}_2\text{O}_4$  ferrite powder. The marginal decrease in saturation magnetization has been observed for this composition ( $x = 0.75$ ) while annealed at  $950\text{ }^\circ\text{C}$  and then a small increase in value for annealing at a higher temperature  $\sim 1250\text{ }^\circ\text{C}$ . Similarly, the coercive field values were found to decrease with increase in annealing temperature for all the compositions except for ferrite powder with high Zn content ( $x = 0.75$ ). The distribution of ions in tetrahedral and octahedral sites takes place during the thermal treatment for the formation of inverse spinel crystallographic phase. The cation ordering increases with increasing the temperature, resulting in the higher saturation magnetization, as observed in samples annealed at  $1250\text{ }^\circ\text{C}$ <sup>25,39</sup>. Further, saturation magnetization increases initially with an increase in  $\text{Zn}^{2+}$  ion concentration and a significant decrease in value has been observed beyond  $x = 0.5$  for ferrite composition as shown in Fig. 3f. At low concentration of  $\text{Zn}^{2+}$  ions, spin site occupancy reduces at A (tetrahedral) sites due to the presence of non-magnetic  $\text{Zn}^{2+}$  ions, however, net magnetization increases due to the shift of  $\text{Fe}^{3+}$  ions from A site to B (octahedral) sites. The increase in  $\text{Zn}^{2+}$  substitution beyond  $x = 0.5$  resulted in the reduced effective spin A site contributions due to



**Figure 1.** (a) XRD pattern of  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  ferrite powders annealed at different elevated temperatures of 650 °C, 950 °C and 1250 °C. (b) XRD pattern of  $\text{Ni}_{0.5}\text{Zn}_x\text{Fe}_2\text{O}_4$  ferrite powders with  $\text{Zn}^{2+}$  ion concentration (c) Shifting in (311) plane XRD peak with  $\text{Zn}^{2+}$  ion concentration (d) Variation in lattice parameter with Zn content in compositions.

the non-availability of the minimum number of spins sites for the oxygen mediated super-exchange interaction between A and B cation sites, leading to decrease in magnetization value, as observed in the present study<sup>17,37</sup>. Moreover, the annealing temperature has favored grain growth, resulting in the enhanced number of domain walls or even larger domains within the grains. The contribution of a domain wall in magnetization/demagnetization process dominates against domain rotation, as domain wall movement is less energetic than the domain wall rotation<sup>18</sup>. Therefore, such energy competition between domain rotation and domain wall movement in larger grains has led to the lower coercive field values for compositions annealed at high temperature i.e. 1250 °C. The decrease in coercive field values is attributed to the decrease in magneto-crystalline anisotropy with Zn substitution, as substantiated in our experimental observations<sup>40</sup>.

The complex permittivity ( $\epsilon_r^* = \epsilon_r' - j\epsilon_r''$ ) and permeability ( $\mu_r^* = \mu_r' - j\mu_r''$ ) values were computed by Nicolson and Ross algorithm using S-parameters measured through waveguide transmission line technique over MW frequency range (2–12.4 GHz)<sup>41</sup>. The imaginary values of complex EM parameters ( $\epsilon_r''$ ,  $\mu_r''$ ) represent the MW attenuation/absorption characteristics of material and are depicted on the negative scale, following the standard convention for representing the loss factor. All the  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  samples annealed at 1250 °C show similar values of  $\epsilon_r' \sim 6.3 \pm 0.1$  over the measured frequency range 2–12.4 GHz. The imaginary permittivity values exhibit non-dispersive behavior with a constant value nearly  $\sim 0.005$  for all  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  samples over the entire frequency range. These measurements suggest that  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  samples do not show any dielectric loss  $\tan\delta_e$  ( $=\epsilon_r''/\epsilon_r'$ ) over the frequency range 2–12.4 GHz due to negligible imaginary permittivity. The measured real relative permeability ( $\mu_r'$ ) values are decreasing from  $\sim 2.5$  to  $\sim 1$  for  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x=0, 0.25, 0.50$  and  $0.75$ ) ferrite compositions annealed at different temperatures over the 2–12.4 GHz frequency range, as shown in Fig. 4a–d. The imaginary relative permeability ( $\mu_r''$ ) values also change from  $\sim -3.12$  to  $-0.11$  simultaneously with an increase in annealing temperature for  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ( $x=0, 0.25$  and  $0.50$ ) ferrite compositions with a dispersive behavior as shown in Fig. 4a–c for the 2–12.4 GHz frequency range. Further,  $\mu_r''$  values increase relatively in the 2–8 GHz low-frequency region and the effect is more prominent for  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$ . The values are negligible  $\sim -0.02$  for all different temperature annealed  $\text{Ni}_{0.25}\text{Zn}_{0.75}\text{Fe}_2\text{O}_4$  samples, as shown in Fig. 4d. These measurements suggest that both annealing temperature and  $\text{Zn}^{2+}$  ion concentration in  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$ , affect  $\mu_r''$  dispersive behavior over the frequency range 2–12.4 GHz. The imaginary permeability, which is responsible for MW energy loss, depends on saturation magnetization ( $M_s$ ) and coercive field ( $H_c$ ) as given in equation (1)<sup>42</sup>

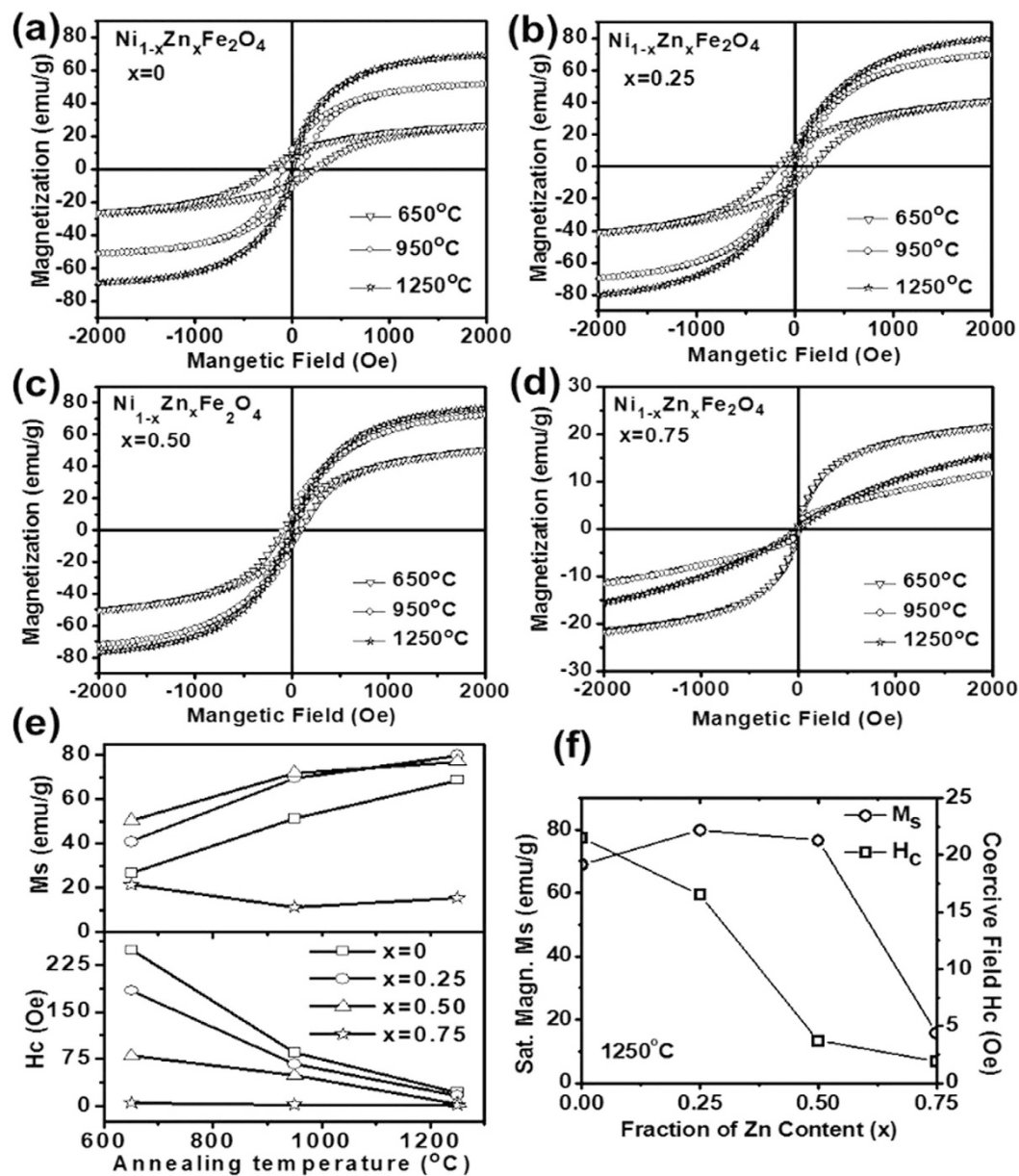


**Figure 2.** SEM micrograph of Ni<sub>1-x</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> powder annealed at elevated temperatures of 650 °C, 950 °C and 1250 °C for (a) x = 0 (b) x = 0.5.

$$\mu'' = \frac{M_s^2}{4\mu_0 K_1 \alpha} \propto \frac{M_s^2}{H_c} \quad (1)$$

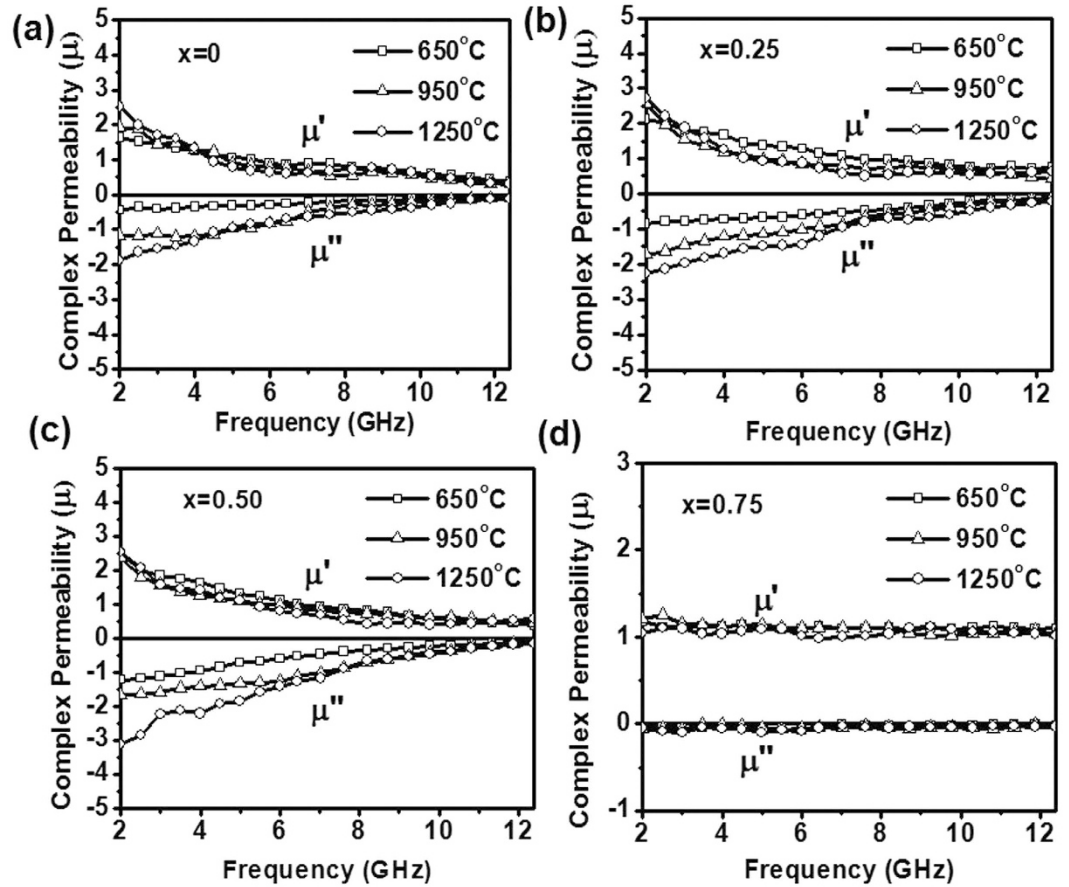
where  $M_s$  is saturation magnetization,  $K_1$  is anisotropic constant,  $\alpha$  is Gilbert constant,  $H_c$  is a coercive field and  $\mu_0$  is intrinsic permeability. The  $\mu_r''$  values show an increasing trend from  $-1.90$  to  $-3.2$  at 2 GHz with an increase in annealing temperature from 650 °C to 1250 °C. This is in accordance with the observed increase in saturation magnetization  $M_s$  and the decrease in coercive field  $H_c$  for the samples ( $x = 0$  to  $x = 0.5$ ). The magnetic loss tangent ( $\tan\delta_m = \mu_r''/\mu_r'$ ) for Ni<sub>1-x</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> ( $x = 0, 0.25, 0.50$  and  $0.75$ ) ferrite powder samples, annealed at different temperatures viz. 650 °C, 950 °C and 1250 °C, are plotted in Fig. 5a–d. An increase in the loss tangent values has been observed for Ni<sub>1-x</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> ferrite samples for both (i) increase in  $x$  from 0 to 0.5 and (ii) annealing temperature from 650 °C to 1250 °C. The 1250 °C annealed Ni<sub>1-x</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> sample showed  $\tan\delta_m > -0.8$  for  $x = 0$  and 0.25 over the 2–8 GHz and 2–10 GHz frequency bands with the maximum  $\tan\delta_m \sim -1.27$  ( $x = 0$ ) and  $\sim -1.65$  ( $x = 0.25$ ) at  $\sim 6$  GHz frequency. The sample with  $x = 0.5$  has shown even enhanced  $\tan\delta_m > -1.2$  over 2–10 GHz with maximum value  $\sim -1.75$  at 6 GHz. These measurements suggest that the maxima of loss tangent ( $\tan\delta_m$ )<sub>max</sub> values increase with Zn<sup>2+</sup> ion concentration up to  $x = 0.50$  and beyond that at  $x = 0.75$  reduced sharply to the negligible loss tangent  $\sim -0.05$  as shown in Fig. 5e. These observations are consistent with the behavior of saturation magnetization and coercive field values as described earlier in the text. Further, it is interesting to note that the ( $\tan\delta_m$ )<sub>max</sub> for all compositions ( $x = 0, 0.25, 0.50$  and  $0.75$ ) is found at 6 GHz, nearly independent of the frequency. The Ni<sub>0.5</sub>Zn<sub>0.5</sub>Fe<sub>2</sub>O<sub>4</sub> ferrite powder annealed at 1250 °C shows maximum loss tangent values among all other compositions and therefore, has been considered for preparation of rubber composites for microwave absorption applications.

A 50 wt% loaded ferrite-NBR sample, FMAR50, showed the real permittivity ( $\epsilon_r'$ )  $\sim 2.8 \pm 0.1$  over the entire 2–12.4 GHz frequency range. With the increase in Ni<sub>0.5</sub>Zn<sub>0.5</sub>Fe<sub>2</sub>O<sub>4</sub> ferrite filler loading,  $\epsilon_r'$  value has increased to  $\sim 4.2 \pm 0.2$  at 60 wt% loading in sample FMAR60,  $\sim 4.7 \pm 0.1$  at 70 wt% in sample FMAR70 and  $\sim 5.9$  at 80 wt% loading in sample FMAR80 as shown in Fig. 6a. The values of the imaginary component of the permittivity are found negligible between  $\sim -0.0015$  and  $\sim -0.002$  for all the different ferrite loaded rubber composites over the entire frequency range of 2–12.4 GHz. This small value of complex permittivity suggests the absence of dielectric



**Figure 3.** Room-temperature M-H Hysteresis curve of  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ferrite powders at (a)  $x=0$  (b)  $x=0.25$  (c)  $x=0.50$  (d)  $x=0.75$  (e) variation of  $M_s$  with annealing temperature for each composition of ferrite powders (f) variation of saturation magnetization  $M_s$  and coercive field  $H_c$  with Zn concentration.

loss contribution for microwave absorption in these rubber composites. The real component of the permeability values ( $\mu_r'$ ) in rubber composite samples has shown a decrease with increase in frequency as shown in Fig. 6b and  $\mu_r'$  values lie in the range of 1.14 to 0.90, 1.25 to 0.80, 1.26 to 0.83 and 1.37 to 0.70, for FMAR50, FMAR60, FMAR70, and FMAR80 samples respectively. The imaginary permeability ( $\mu_r''$ ) components for FMAR50 sample is found to be in the range of  $\sim -0.33$  to  $-0.03$  with reducing trend towards the higher frequency range. Further, enhancement of  $\mu_r''$  values has been observed with increase in loading fraction of  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  ferrite powder in composite samples. In FMAR60 sample, the  $\mu_r''$  shows wider dispersion characteristics with values in the range of  $\sim -0.65$  to  $-0.10$  over the entire frequency range. The similar trend has been observed for FMAR70 and FMAR80 samples where  $\mu_r''$  values fall in the range  $\sim -0.82$  to  $-0.17$  and  $\sim -1.03$  to  $-0.20$  respectively as shown in Fig. 6c. The magnetic loss tangent ( $\tan\delta_m$ ) values show wide dispersion and values range from  $\sim -0.28$  to  $-0.03$ ,  $-0.50$  to  $-0.11$ ,  $\sim -0.63$  to  $-0.20$  and  $\sim -0.80$  to  $-0.30$  in the entire 2–12.4 GHz frequency range for FMAR50, FMAR60, FMAR70 and FMAR80 samples respectively, as summarized in Fig. 6d. Thus, we observed that the magnetic loss tangent values have increased with  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  loading fraction in these rubber composite samples with decreasing trend towards higher frequency range. The observed enhancement in loss tangent values has been attributed to the increasing loading fraction of ferrite in NBR by 1.50, 2.33 and 4.00 times in comparison to



**Figure 4.** Frequency dependence of the complex permeability for annealed  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  powder (a)  $x = 0$  (b)  $x = 0.25$  (c)  $x = 0.50$  (d)  $x = 0.75$ .

sample FMAR50 (Table 1). The MW reflection losses (R.L.) have been computed for  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  ferrite loaded composite samples (FMAR50 - FMAR80) by using the following equation (2)<sup>43</sup>:

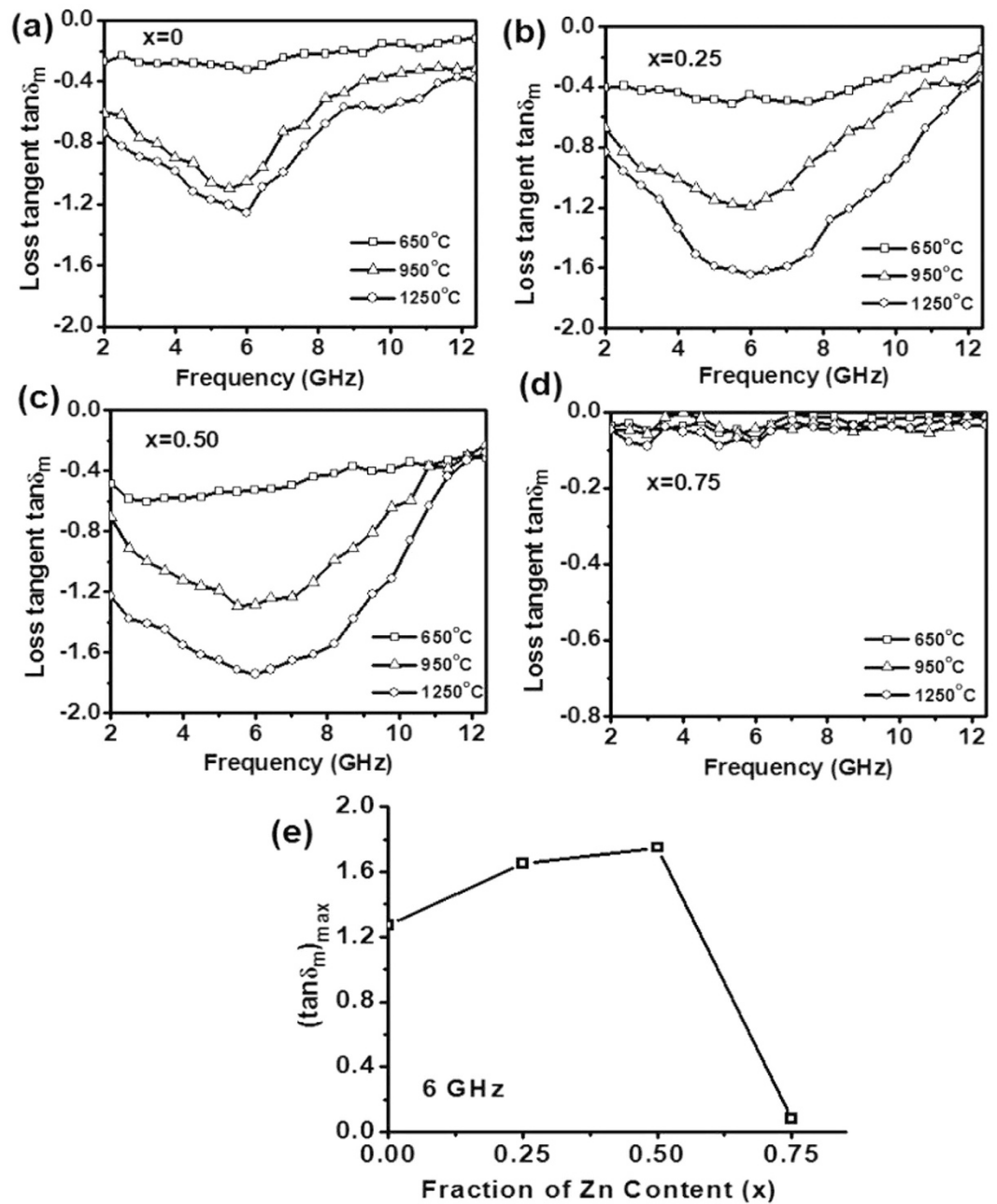
$$R.L. = 20 \log_{10} \left| \frac{\sqrt{\frac{\mu_r^*}{\epsilon_r^*}} \tan h \left( \frac{j 2\pi d}{\lambda_0} \sqrt{\mu_r^* \epsilon_r^*} \right) - 1}{\sqrt{\frac{\mu_r^*}{\epsilon_r^*}} \tan h \left( \frac{j 2\pi d}{\lambda_0} \sqrt{\mu_r^* \epsilon_r^*} \right) + 1} \right| \quad (2)$$

where,  $\lambda$  is the wavelength,  $\mu_r^*$  is the complex relative permeability,  $\epsilon_r^*$  is the complex relative permittivity and  $d$  is the absorber thickness. Further, the impedance of absorber's top layer should be comparable to the free space impedance  $Z_0$  ( $377 \Omega$ ) to enter the microwaves inside the absorber for its effective attenuation as explained schematically in Fig. 7. Considering the close approximation of matched wave impedance criterion, the reflection loss of absorber should have matched values for absorber thickness ( $d_m$ ) at  $\lambda_m/4$ , to satisfy the destructive interference criterion among surface reflected and metal back-reflected wave with the following dependence, as explained by eqs (3) and (4) (Fig. 7)<sup>32,44</sup>

$$\frac{4d}{\lambda} = \frac{\left( \sqrt{\mu_r' \epsilon_r'} \right)}{(1 + \tan^2 \delta_m)} \quad (3)$$

$$d_m = \frac{c}{4f \sqrt{|\mu_r^*| |\epsilon_r^*|}} \quad (4)$$

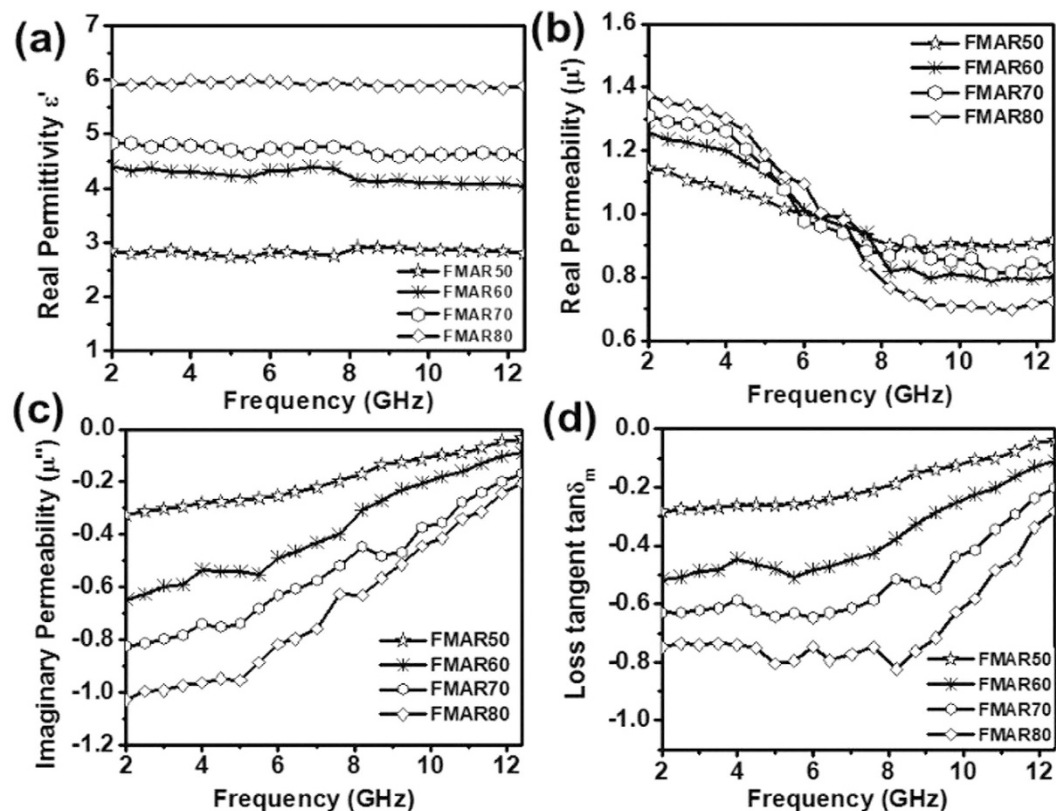
The calculated reflection loss values for different  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  ferrite loaded samples are shown in Fig. 8a–d. FMAR50 sample shows the maximum possible reflection loss value  $(R.L.)_{\max} \sim -4\text{dB}$  at  $\sim 8\text{GHz}$  for 5 mm absorber thickness, which has increased up to  $\sim -10\text{dB}$  at  $\sim 7\text{GHz}$  for FMAR60 sample for the same thickness. Similarly, with further increase of ferrite loading (FMAR70), the  $(R.L.)_{\max}$  value has further increased to  $\sim -15\text{dB}$  at 10 GHz,  $\sim -20\text{dB}$  at 8.3 GHz and  $\sim -24\text{dB}$  at 7 GHz for absorber thickness values of  $\sim 3.5\text{mm}$ , 4.0 mm, and 4.6 mm, respectively. It is interesting to note that the absorption peak is shifting towards the lower frequency with



**Figure 5.** Frequency dependence of the loss tangent ( $\tan\delta_m$ ) for annealed  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  powder (a)  $x=0$  (b)  $x=0.25$  (c)  $x=0.50$  (d)  $x=0.75$  (e) variation of maximum loss tangent with Zn concentration at resonating frequency of 6 GHz.

increasing the absorber thickness for this composition. The observed shifting in reflection loss, towards lower frequency for FMAR70 composite can be explained using eqs (3 and 4). These relations suggest that absorber thickness will effectively reduce with increasing  $\epsilon_r'$  and  $\tan\delta_m$ . The insignificant values of reflection loss observed for FMAR50 and FMAR60 are mainly because of the relatively lower  $\tan\delta_m$ , for these composite samples as shown in Fig. 6d. Interestingly, the onset of twin match frequencies ( $f_{m1}/f_{m2}$ ) has been observed at two different matched thicknesses ( $t_{m1}$  and  $t_{m2}$ ), Fig. 8d, for FMAR80 composite sample. At absorber thickness  $t_{m1} = 4.6$  mm, the first matched (R.L.)<sub>max</sub> value is  $\sim -43$  dB at the first matching frequency  $f_{m1} \sim 5$  GHz. With the decrease in absorber thickness, R.L. profile has shifted towards higher frequency side with lower (R.L.)<sub>max</sub> values  $\sim -22$  dB and  $\sim -26$  dB for absorber thicknesses  $\sim 4$  mm and  $3.5$  mm, respectively. On further reduction in the absorber thickness at  $t_{m2} = 3.25$  mm, the second matched (R.L.)<sub>max</sub> value  $\sim -43$  dB has been observed at the second matching frequency  $f_{m2} \sim 10$  GHz.

The existence of such two matching frequencies has been observed earlier in pure ferrite powders, however, in rubber-ferrite composite samples only a single matching frequency has been reported<sup>37,45</sup>. The two possible MW absorption loss mechanism are generally attributed in ferrite materials: (i) relaxation mechanism due to



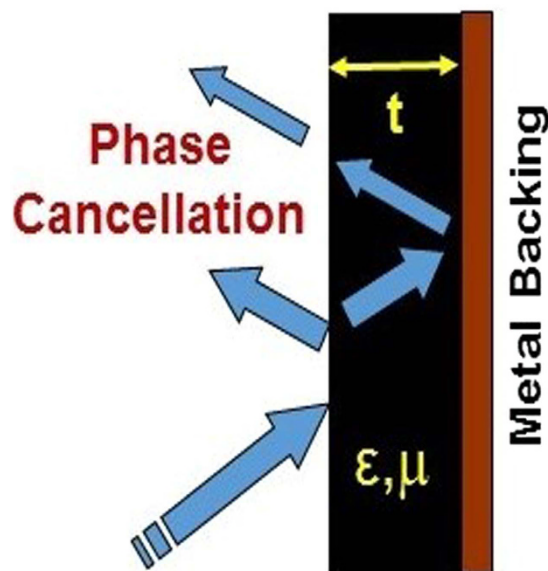
**Figure 6.** (a) Real permittivity plots for ferrite loaded rubber composites FMAR50-80 with MW frequencies (b) real permeability behavior of ferrite loaded rubber composites (c) imaginary permeability plots of ferrite loaded rubber composites (d) loss tangent profiles for ferrite loaded rubber composites.

S. No.	Sample Code	Quantity of NBR (g)	Quantity of $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$ ferrite in compound (wt%)	Quantity of ferrite power (g)	Enhancement in filler loading as compared to sample FMAR50 (X)
1	FMAR50	30	50	30	1.00
2	FMAR60	30	60	45	1.50
3	FMAR70	30	70	70	2.33
4	FMAR80	30	80	120	4.00

**Table 1.** Compositions of MW Rubber Absorbers.

the domain wall motion and (ii) the spin rotational resonance. The domain wall resonance mechanism usually dominates at lower MW frequency range ( $<1$  GHz), as the relaxation of domain motion does not follow the higher MW frequency beyond 1 GHz, whereas relaxation of spin resonance or ferromagnetic resonance (FMR) dominates at the higher MW frequencies. The maximum loss tangent values observed at  $\sim 6$  GHz for  $1250^\circ\text{C}$  annealed  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  ferrites, is close to the first matching frequency ( $f_{m1}$ ) observed at  $\sim 5$  GHz for 4.6 mm thick FMAR80 sample as shown in Fig. 8d, and is attributed to the spin resonance relaxation mechanism in these samples<sup>46</sup>. As discussed earlier, the FMR frequencies and thus, MW absorption of Ni-Zn ferrite system depends strongly on chemical composition, synthetic route and post processing conditions. Shi *et al.* tuned the resonance frequency  $\sim 2.54$  GHz for Ni spinel ferrite nanoparticles prepared using sol-gel process<sup>47</sup> whereas Zhao *et al.* adjusted the matching absorption frequencies for Ni-Zn spinel ferrite in the range of  $\sim 1$ –12 GHz by substitution of  $\text{Cu}^{2+}/\text{Co}^{2+}$  ions<sup>48</sup>. The second matching frequency ( $f_{m2}$ ) has been observed at  $\sim 10$  GHz for 3.25 mm FMAR80 absorber thickness. The  $f_{m2}$  is independent of resonance frequency and is observed because of matched absorber thickness ( $\lambda_m/4 \sim 3.25$  mm) as given by eq. (4). The R.L. profile associated to  $f_{m1}$  at absorber thickness  $\sim 4.6$  mm may extend towards the higher frequency side with a decrease in thickness up to 3.5 mm. Whereas, the R.L. profile associated with  $f_{m2}$  may contribute towards lower frequency side with an increase in thickness up to 4 mm. It has been observed that R.L. profiles have both the components of matching frequencies ( $x.f_{m1} + y.f_{m2}$ ) at these thicknesses, where  $x$  and  $y$  are the fractional contribution from individual matching frequencies  $f_{m1}$  and  $f_{m2}$ , respectively. At the intermediate absorber thickness of 3.5 mm and 4.0 mm the matching frequency ( $f_M$ ) behavior follows the trend as given in eqs (5 and 6)





**Figure 7.** A schematic representation of reflection loss mechanism for incident MW radiation at optimal absorber thickness.

$$d = 3.5 \text{ mm}; f_M = x \cdot f_{m1} + y \cdot f_{m2}, \text{ while } x < y \quad (5)$$

$$d = 4.0 \text{ mm}; f_M = x \cdot f_{m1} + y \cdot f_{m2}, \text{ while } x > y \quad (6)$$

The matching frequencies ( $f_m$ ) for  $d = 3.5$  mm and  $4.0$  mm thick FMAR80 samples are 9 and 6 GHz respectively, as shown in Fig. 8d. The fractional contributions ( $x$  and  $y$ ) for  $d = 3.5$  mm thick FMAR80 sample are  $x = 0.2$  and  $y = 0.8$  corresponding to  $f_{m1}$  (5 GHz) and  $f_{m2}$  (10 GHz) respectively. For  $d = 4.0$  mm thick FMAR80 sample, the fractional contributions are  $x = 0.8$  and  $y = 0.2$ , corresponding to  $f_{m1}$  (5 GHz) and  $f_{m2}$  (10 GHz) respectively, substantiating the proposed mechanism of twin matching frequencies contribution for microwave absorption in these ferrite-rubber composite samples.

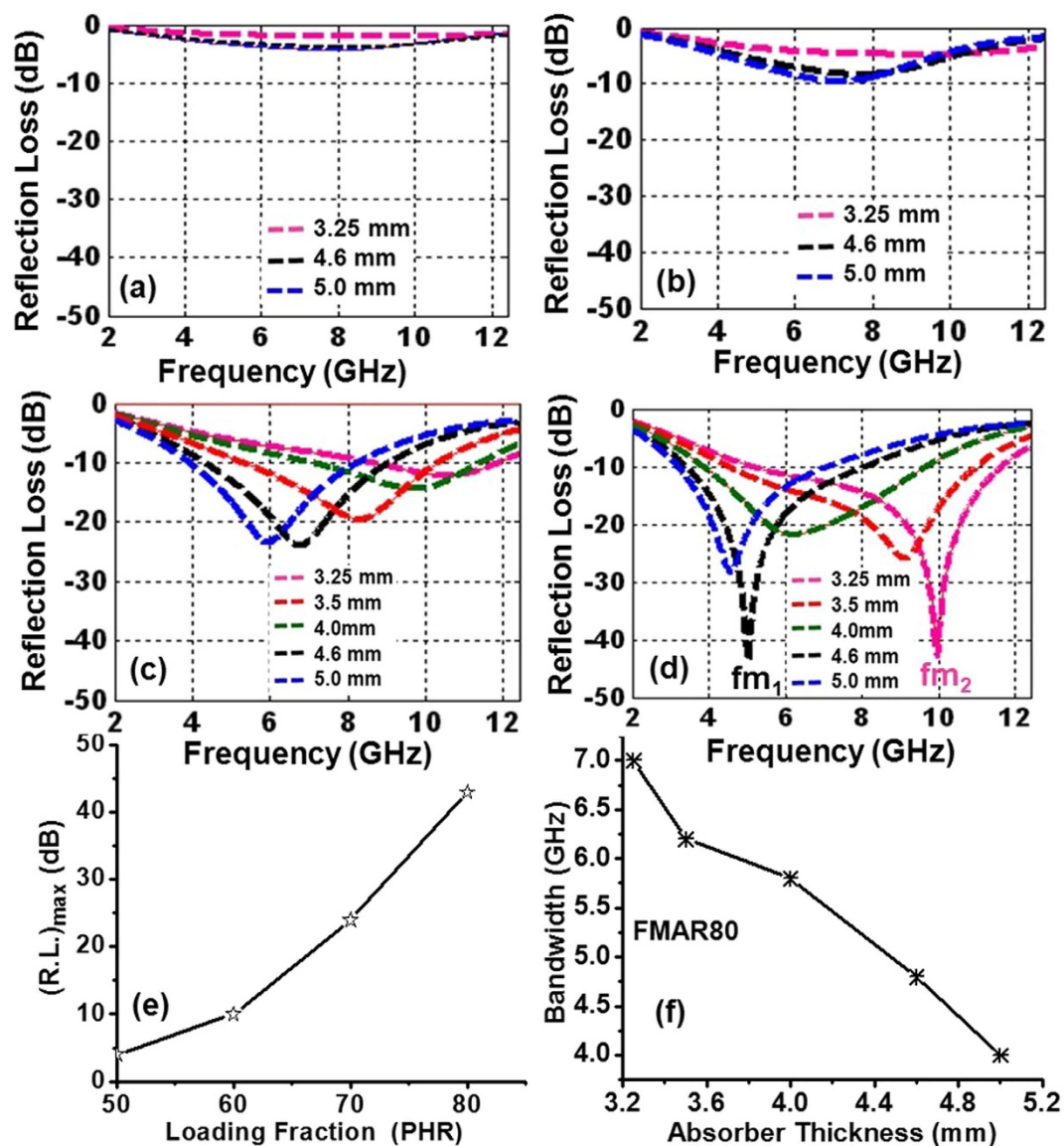
## Conclusions

The maximum reflection loss (R.L.)<sub>max</sub> values increase with loading fraction of  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  ferrite powder in these rubber composites, as shown in Fig. 8e. Interestingly, for FMAR80 the desired frequency bandwidth (where R.L.  $\geq 10$  dB or at least 90% attenuation of MW signal) decreases with absorber thickness as shown in Fig. 8f. The MW absorber at 3.25 mm thickness (corresponding to  $f_{m2}$ ) has the widest bandwidth of  $\sim 7$  GHz, whereas, at absorber thickness of 4.6 mm, frequency bandwidth window reduced to  $\sim 4.2$  GHz. In the intermediate thicknesses, the bandwidth lies between this ranges. These studies suggest that the FMAR80 absorber can be used as a tunable MW frequency absorber using the thickness as a controlling parameter for strategic applications such as microwave stealth over the different frequency bands.

## Methods

**Experimental details.** The ferrite powders are prepared using gel to carbonate precipitation method, where the co-precipitations of divalent cations ( $\text{Ni}^{2+}$ ,  $\text{Zn}^{2+}$ ) as fine particles of carbonates within hydrated gels of ferric hydroxide has been carried out by adding the alkali solution into the mixed metal salt ions. 1 M solution of  $\text{FeCl}_3$  (Merck CAS No. 7705-08-0),  $\text{NiCl}_2$  (Merck CAS No. 7718-54-9),  $\text{ZnCl}_2$  (Merck CAS No. 7646-85-7) were mixed stoichiometrically, followed by adding dropwise 1 M  $\text{Na}_2\text{CO}_3$  solution (Merck CAS No. 497-19-8) while maintaining pH  $\sim 9$ , to realize the co-precipitation. The obtained precipitate was washed and dried in an oven at  $\sim 90^\circ\text{C}$  for 2 hours in the air ambient. The resultant composite powder consists of sub-micron crystalline particles of carbonates, embedded within the amorphous medium of  $\text{Fe}_2\text{O}_3 \cdot x\text{H}_2\text{O}$  ( $70 < x < 110$ ). The composite powder was annealed sequentially at  $650^\circ\text{C}$ ,  $950^\circ\text{C}$  and  $1250^\circ\text{C}$  for 3 hours each to obtain final sample, which was used for detailed characterization of the physical and microwave absorption properties. The similar process has been followed to prepare a series of  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  spinel ferrites with  $x = 0, 0.25, 0.50$  and  $0.75$ , to understand the effect of Zn substitution on the physical and microwave absorption properties.

Rubber based microwave absorbing sheets are fabricated using mechanical milling followed by high-temperature compression moulding (HTCM), to get the desired shape and size of composite samples. Initially, 30 g of NBR was thoroughly mixed in two roll mixing mill (TRMM) and  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  powder was added in different filler ratio in wt%, as listed in the Table -I. Different additives were mixed in quantity of parts per hundred (PHR) of rubber for vulcanization and curing of the rubber compound. The additives include sulphur (02 PHR) as vulcanizing agent, mercaptobenzothiazole disulphide (MBTS) (1.5 PHR) as accelerator for



**Figure 8.** Optimal Reflection Loss (R.L.) over frequency range 2–12.4 GHz and matching thicknesses of ferrite loaded rubber composites (a) FMAR50 (b) FMAR60 (c) FMAR70 (d) FMAR80 (e) variation of maximum reflection loss with ferrite powder loading fraction in composite (f) optimal R.L. bandwidth profile with composite absorber thickness.

curing of rubber-filler compound, ZnO (05 PHR), Steric Acid (02 PHR) as activator to enhance the effect of accelerator and Trimethyl-Di-Quinoline TDQ (01 PHR) as antioxidant for rubber to prevent it from environmental degradation<sup>29</sup>. After homogeneous mixing, the compounds were transferred into 200 mm × 200 mm × 2 mm (L × B × D) size mould and hydraulically pressed at 150 °C with 30 Ton pressure for 30 minutes. The mould was then allowed to cool down to the ambient temperature and rubber sheet was collected for MW characterization. The loading of ferrite powder (>80 wt%) in NBR matrix was not possible due to the enhanced brittleness, making difficult to handle the composite materials.

X-ray diffraction measurements (Philips X'Pert Pro) were carried out with  $\text{CuK}\alpha$  ( $\lambda = 1.514 \text{ \AA}$ ) radiation as incident X-ray in  $20^\circ$  to  $80^\circ$   $2\theta$  range, to identify the  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  crystallographic phase. Infrared (IR) spectroscopic studies were carried out using FTIR system (Model: Bruker Vertex 70 V). Shape and morphology of  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  powders were analyzed using Oxford EVO5 Scanning Electron Microscope (SEM) system. The room temperature magnetic hysteresis studies (M-H plots) were carried out using Vibrating Sample Magnetometer (VSM) Model ADE EV-5 for  $-2\text{ kOe}$  to  $+2\text{ kOe}$  magnetic field. Electromagnetic parameters i.e. complex permittivity and permeability values were measured in 2–12.4 GHz MW frequency bands using Vector Network Analyzer model ZVM from Rohde and Schwarz for both pristine  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$  ferrite powders and  $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4/\text{NBR}$  composite samples loaded with different concentrations of ferrite powder.

## References

- Vinoy, K. J. & Jha, R. M. *Radar Absorbing Materials: From Theory to Design and Characterization* (Kluwer Academic Publishers, Norwell, Boston, USA, 1996).
- Zhu, Y. F., Zhang, L., Natsuki, T., Fu, Y. Q. & Ni, Q. Q. Facile synthesis of BaTiO<sub>3</sub> nanotubes and their microwave absorption properties. *ACS Appl. Mater. Inter.* **4**, 2101–2106 (2012).
- Gupta, V. *et al.* Synthesis and investigations on microwave absorption properties of core-shell FeCo(C) alloy nanoparticles. *Sci. Adv. Mat.* **6**, 1–7 (2014).
- Oh, J. H., Oh, K. S., Kim, C. G. & Hong, C. S. Design of radar absorbing structures using glass/epoxy composite containing carbon black in X-band frequency ranges. *Compos. Part B* **35**, 49–56 (2004).
- Meng, W., Yuping, D., Shunhua, L., Xiaogang, L. & Zhijiang, J. Absorption properties of carbonyl-iron/carbon black double-layer microwave absorbers. *J. Magn. Magn. Mater.* **321**, 3442–3446 (2009).
- Duan, Y., Li, G., Liu, L. & Liu, S. Electromagnetic properties of carbonyl iron and their microwave absorbing characterization as filler in silicone rubber. *Bull. Mater. Sci.* **33**(5), 633–636 (2010).
- Zhao, D. L., Li, X. & Shen, Z. M. Microwave absorbing property and complex permittivity and permeability of epoxy composites containing Ni-coated and Ag filled carbon nanotubes. *Compos. Sci. Tech.* **68**, 2902–2908 (2008).
- Huang, X. *et al.* Fabrication and electromagnetic loss properties of Fe<sub>3</sub>O<sub>4</sub> nanofibers. *J. Mater. Sci.: Mater. Electron.* **26**, 3474–3478 (2015).
- Zou, H. *et al.* Determining factors for high performance silicone rubber microwave absorbing materials. *J. Magn. Magn. Mater.* **323**, 1643–1651 (2011).
- Abbas, S. M., Dixit, A. K., Chatterjee, R. & Goel, T. C. Complex permittivity, complex permeability and microwave absorption properties of ferrite-polymer composites. *J. Magn. Magn. Mater.* **309**, 20–24 (2007).
- Huang, X., Zhang, J., Xiao, S., Sang, T. & Chen, G. Unique electromagnetic properties of the zinc ferrite nanofiber. *Mat. Lett.* **124**, 126–128 (2014).
- Huang, X. *et al.* Facile preparation and microwave absorption properties of porous hollow BaFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> composite microrods. *J. Alloy. Compound.* **648**, 1072–1075 (2015).
- Zhao, J. *et al.* Lanthanum and neodymium doped barium ferrite-TiO<sub>2</sub>/MCNTs/poly(3-methyl-thiophene) composites with nest structures: preparation, characterization and electromagnetic microwave absorption properties. *Sci. Rep.* **6**, 20496 (2016).
- Li, N. *et al.* Electrostatic tuning of ferromagnetic resonance and magneto electric interactions in ferrite-piezoelectric heterostructures grown by chemical vapor deposition. *Appl. Phys. Lett.* **99**, 192502 1–3 (2011).
- Dzunuzovic, A. S. *et al.* Structure and properties of Ni-Zn ferrite obtained by auto-combustion method. *J. Magn. Magn. Mater.* **374**, 245–251 (2015).
- Razzitte, A. C., Fano, W. G. & Jacobo, S. E. Electrical permittivity of Ni and Ni-Zn ferrite polymer composites. *Phys. B.* **354**, 228–231 (2004).
- Krishna, K. R., Kumar, K. V., Ravindernathgupta, C. & Ravinder, D. Magnetic properties of Ni-Zn ferrites by citrate gel method. *Adv. Mat. Phys. Chem.* **2**, 149–154 (2012).
- Costa, A. C. F. M., Tortella, E., Morelli, M. R. & Kiminami, R. H. G. A. Synthesis, microstructure and magnetic properties of Ni-Zn ferrites. *J. Magn. Magn. Mater.* **256**, 174–182 (2003).
- Amiri, G. R. *et al.* Magnetic properties and microwave absorption in Ni-Zn and Mn-Zn ferrite nanoparticles synthesized by low-temperature solid-state reaction. *J. Magn. Magn. Mater.* **323**, 730–734 (2011).
- Huang, X., Zhang, J., Lai, M. & Sang, T. Preparation and microwave absorption mechanisms of the Ni-Zn ferrite nanofibers. *J. Alloy. Compound.* **627**, 367–373 (2015).
- Kakirde, A., Sinha, B. & Sinha, S. N. Development and characterization of nickel-zinc spinel ferrite for microwave absorption at 2.4 GHz. *Bull. Mater. Sci.* **31**(5), 767–770 (2008).
- Kim, S. S., Han, D. H. & Cho, S. B. Microwave absorbing properties of sintered Ni-Zn ferrite. *IEEE Trans. Magn.* **30**(6), 4554–4556 (1994).
- Fawzi, A. S., Sheikh, A. D. & Mathe, V. L. Structural, dielectric properties and AC conductivity of Ni<sub>(1-x)</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> spinel ferrites. *J. Alloy. Compound.* **502**, 231–237 (2010).
- Moulson, A. J. & Herbert, J. M. *Electroceramics* (Chapman and Hall, London, 1990).
- Hench, L. L. & West, J. K. *Principles of Electronic Ceramics* (A Wiley-Inter Science Publication, Singapore, 1989).
- Huang, X. *et al.* Effect of pH value on electromagnetic loss properties of Co-Zn ferrite prepared via coprecipitation method. *J. Magn. Magn. Mater.* **405**, 36–41 (2016).
- Kong, I. *et al.* Magnetic and microwave absorbing properties of magnetite-thermoplastic natural rubber nanocomposites. *J. Magn. Magn. Mater.* **322**, 3401–3409 (2010).
- Lima, U. R., Nasar, M. C., Nasar, R. S., Rezende, M. C. & Araujo, J. H. Ni-Zn nanoferrite for radar-absorbing material. *J. Magn. Magn. Mater.* **320**, 1666–1670 (2008).
- Verma, A., Saxena, A. K. & Dube, D. C. Microwave permittivity and permeability of ferrite-polymer thick films. *J. Magn. Magn. Mater.* **263**, 228–234 (2003).
- Dosoudil, R., Usakova, M., Franek, J., Slama, J. & Olah, V. RF electromagnetic wave absorbing properties of ferrite polymer composite materials. *J. Magn. Magn. Mater.* **304**, e755–e757 (2008).
- Zhu, L. *et al.* Electromagnetic and microwave-absorbing properties of magnetic nickel ferrite nanocrystals. *Nanoscale* **3**, 2862–2864 (2011).
- Bueno, A. R., Gregori, M. L. & Nobrega, M. C. S. Microwave-absorbing properties of Ni<sub>0.50-x</sub>Zn<sub>0.50-x</sub>Me<sub>2x</sub>Fe<sub>2</sub>O<sub>4</sub> (Me=Cu, Mn, Mg) ferrite-wax composite in X-band frequencies. *J. Magn. Magn. Mater.* **320**, 864–870 (2008).
- Singh, V. K. *et al.* Microwave absorbing properties of a thermally reduced graphene oxide/nitrile butadiene rubber composite. *Carbon* **50**(6), 2202–2208 (2012).
- Barlow, F. W. *Rubber Compounding* (Marcel Dekker Inc., New York, 1993).
- Hwang, C. C., Tsai, J. S. & Huang, T. H. Combustion synthesis of Ni-Zn ferrite by using glycine and metal nitrates- investigations of precursor homogeneity, product reproducibility and reaction mechanism. *Mater. Chem. Phys.* **93**(2–3), 330–336 (2005).
- Jalaly, M., Enayati, M. H., Kameli, P. & Karimzadeh, F. Effect of composition on structural and magnetic properties of nanocrystalline ball milled Ni<sub>1-x</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> ferrite. *Phys. B* **405**, 507–512 (2010).
- Zhang, M. *et al.* Magnetic and microwave absorption properties of Ni<sub>1-x</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> nanocrystalline synthesized by sol-gel method. *Sci. China Tech. Sci.* **56**(1), 13–19 (2013).
- Smith, J. & Wijn, H. P. J. *Ferrites* (Philips Technical Library, Netherlands, 1959).
- Peelamedu, R., Grimes, C., Agrawal, D. & Roy, R. Ultralow dielectric constant nickel-zinc ferrites using microwave sintering. *J. Mater. Res.* **18**(10), 2292–2295 (2003).
- Verma, A., Goel, T. C., Mendiratta, R. G. & Kishan, P. Magnetic properties of nickel-zinc ferrites prepared by the citrate precursor method. *J. Magn. Magn. Mater.* **208**(1–2), 13–19 (2000).
- Nicolson, A. M. & Ross, G. F. Measurement of the intrinsic properties of materials by time-domain techniques. *IEEE Trans. Instrum. Meas.* **19**(4), 377–382 (1970).
- Chen, N. & Gu, M. Microstructure and microwave absorption properties of Y-substituted Ni-Zn ferrites. *Op. J. Mat.* **2**, 37–41 (2012).

43. Michielssen, E., Sajer, J., Ranjithan, S. & Mitra, R. Design of lightweight, broad-band microwave absorbers using genetic algorithms. *IEEE Trans. Microw. Theo. Tech.* **41**(6), 1024–1031 (1993).
44. Petrov, V. M. & Gagulin, V. V. Microwave absorbing materials. *Inorg. Mater.* **37** (2), 93–98 (2001).
45. Kim, S. S. *et al.* Complex permeability and permittivity and microwave absorption of ferrite-rubber composite in X-band frequencies. *IEEE Trans. Magn.* **27**(6), 5462–5464 (1991).
46. Shin, J. Y. & Oh, J. H. The microwave absorbing phenomena of ferrite microwave absorbers. *IEEE Trans. Magn.* **29**(6), 3437–3439 (1993).
47. Shi, Z. *et al.* Magnetic resonance of the NiFe<sub>2</sub>O<sub>4</sub> nanoparticles in the gigahertz range. *Nanoscale Reas. Lett.* **8**, 404–408 (2013).
48. Zhao, D. L., Ly, Q. & Shen, Z. M. Fabrication and microwave absorbing properties of Ni-Zn spinel ferrite. *J. Alloy. Compound.* **480**, 634–638 (2009).

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## Author Contributions

Lokesh Saini, Manoj Kumar Patra, Ambesh Dixit and Sampat Raj Vadera coined the problem and planned experiments. Lokesh Saini, Raj Kumar Jani, and Goutam Kumar Gupta carried out experimental work. The data and results are discussed by all authors. Lokesh Saini, Ambesh Dixit, and S.R. Vadera wrote the manuscript and all authors have approved the manuscript.

## Additional Information

**Competing Interests:** The authors declare no competing financial interests.

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