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Magnesium diboride coated bulk niobium: a new approach to higher acceleration gradient

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Bulk niobium Superconducting Radio-Frequency cavities are a leading accelerator technology. Their performance is limited by the cavity loss and maximum acceleration gradient, which are negatively affected by vortex penetration into the superconductor when the peak magnetic field at the cavity wall surface exceeds the vortex penetration field (H_{vp}). It has been proposed that coating the inner wall of an SRF cavity with superconducting thin films increases H_{vp}. In this work, we utilized Nb ellipsoid to simulate an inverse SRF cavity and investigate the effect of coating it with magnesium diboride layer on the vortex penetration field. A significant enhancement of H_{vp} was observed. At 2.8 K, H_{vp} increased from 2100 Oe for an uncoated Nb ellipsoid to 2700 Oe for a Nb ellipsoid coated with ~200 nm thick MgB$_2$ thin film. This finding creates a new route towards achieving higher acceleration gradient in SRF cavity accelerator beyond the theoretical limit of bulk Nb.

Particle accelerators are our main window to explore particle physics and understand the early universe. Bulk niobium superconducting radio frequency (SRF) cavities are the leading accelerator technology, and in the last 2 decades, their performance has been improved to being very close to the theoretical limit. New materials and/or approaches are needed to further improve the performance and reduce the cost of SRF cavities[1,2]. In this work, we studied the magnesium diboride (MgB$_2$) coated bulk niobium and showed the coated SRF cavities have the potential to reach 30% higher acceleration gradient than the state of the art Nb cavities.

The technology of SRF cavities is based on the Meissner effect, characterized by the expulsion of magnetic field from a bulk superconducting material. In type II superconductors, such as Nb, the Meissner state can only be sustained up to a certain magnetic field, above which flux will penetrate the material in the form of vortices. In the presence of an RF excitation these vortices will oscillate, producing dissipation that drastically reduces the quality factor (Q), thus rendering the cavity useless. The limiting factor is the maximum accelerating gradient (E_{acc}), which is related to the maximum magnetic field parallel to the cavity surface that can be sustained without vortex penetration (H_{vp}). In thermodynamic equilibrium, H_{vp} of a bulk superconductor in the absence of demagnetizing effects is equal to the lower critical field (H_{c1}). However, surface barriers may preclude the vortex entry, allowing the Meissner state be retained under metastable conditions up to a higher superheating field H_{sh}[3]. The best Nb cavities have E_{acc} 50 MV/m at temperature $T \sim 2$ K (the operating temperature of the SRF cavities at $f > 500$ MHz), corresponding to $H_{vp,Nb} \sim 2000$ Oe[4], which is very close to the ideal limit set by the intrinsic material properties, $H_{sh,Nb}(2\,\text{K}) \approx 2280$ Oe[5].

To increase H_{vp}, Gurevich proposed coating the inside of Nb cavities with multilayers of thin superconducting films separated by insulating layers[2]. The idea is that the superconducting films will partially screen the cavity magnetic field, reducing it to a value lower than $H_{vp,Nb}$ at the internal surface of the Nb wall. We will focus on the simplest case of a SRF cavity coated with a single layer of superconductor, because this S-I-S structure already exhibits all the relevant physics and detailed theoretical analyses of its shielding effect have recently been performed with various approaches[6–9].

The principle of operation of the S-I-S structure involves two concepts. First, when the thickness of the superconducting film (d_S) is comparable to or smaller than the penetration depth (λ), H_{c1} for field parallel to the surface increases. This is because the internal field is nonzero everywhere within the thin film, thus the free energy cost of shielding the external field by a screening current is lowered and vortex penetration does not become

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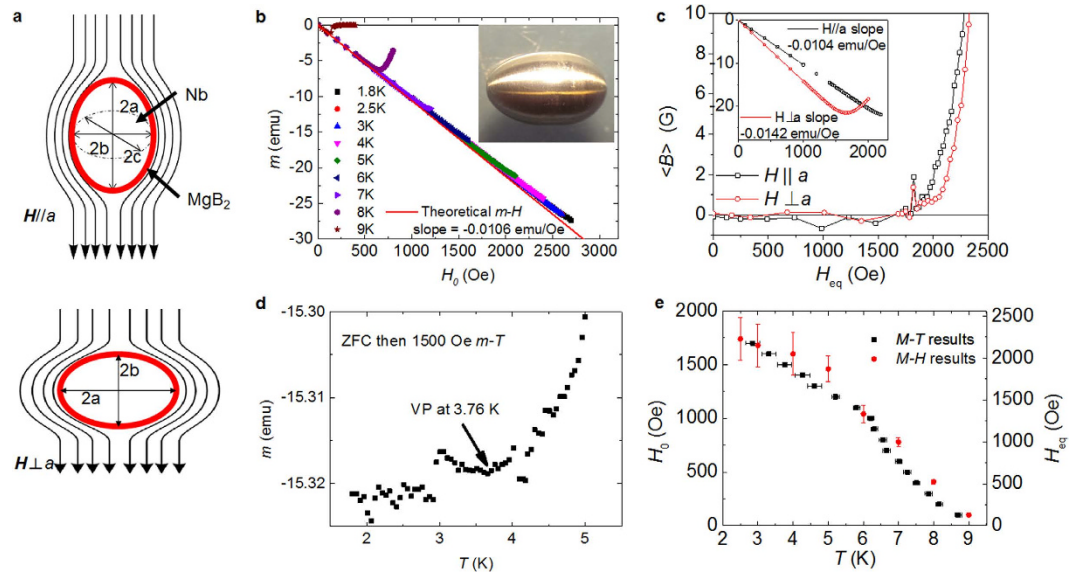
Figure 1. (a) Schematic of the vortex penetration field measurement. (b) ZFC m-H curves of bare Nb ellipsoid at different temperatures. (c) $<B>$-H curves of bare Nb ellipsoid at different orientations. (d) Typical ZFC m-T curve of bare Nb ellipsoid under 1000 Oe applied field. Arrow signals the temperature where H_{vp} equals the applied field. (e) Comparison of H_{vp} obtained from both methods.

favorable until a higher field. For instance, if H is applied on both sides of a film with $d_S \ll \lambda$, H_{c1} increases from the bulk values $H_{c1} \propto \Phi_0/\lambda^2$ to $H_{c1} \propto \Phi_0/d_S^2$ (here $\Phi_0 = 2.07 \times 10^{-7}\,\mathrm{Gcm^2}$ is the flux quantum). The situation is somewhat different when the field is only applied on one side[6], but also in this case H_{c1} for a thin film is substantially enhanced, resulting in a higher H_{vp} for the film-coated Nb cavity[10]. The second concept is that the screening (reduction) of the field produced by the film is $\Delta H \sim d_S J$, where the superconducting current density (J) depends on the details of the geometry but cannot exceed the superconducting depairing current density (J_d) in the film, $J_d \sim H_c/\lambda$, where H_c is the thermodynamic critical field ($H_c > H_{c1}$ in type II superconductors). It is clear from the previous considerations that if d_S is too large there is no enough H_{c1} enhancement and if it is too small H_{vp} is only increased by a small amount ΔH, so there must be some optimum d_S that produces the largest H_{vp}. T. Kubo[9,11] has shown that, when the simple estimate of an exponential decay of the magnetic field from the film surface is replaced by the simultaneous solution of the Maxwell and London equations in the complete S-I-S structure with the appropriate boundary conditions, H_{vp} depends on the properties of both the coating layer and bulk superconducting materials, on d_S, and on the thickness of the insulating layer (d_I). In particular, these studies show that the shielding effect still exists for $d_I = 0$, that is, without an insulating layer between the thin film and the niobium underneath. In this paper we provide the first experimental demonstration of the concept, by showing that a Nb SRF cavity coated with a single MgB$_2$ layer could sustain a higher H_{vp}, above the theoretical limit given by the H_{sh} for Nb. This could lead to SRF cavities with higher accelerating gradients.

The increase of H_{c1} in thin films for **H**//surface is a well-established and well understood effect[10], and can be readily observed using a SQUID magnetometer. As H is increased from 0 at a fixed temperature, the initial Meissner state is characterized by a linear $m(H)$ dependence $m_M = -(V_{eff}/4\pi)H$. Here V_{eff} is the effective superconductor volume, which is smaller than the geometrical volume V due to the field penetration near the surfaces. At H_{c1}, $m(H)$ deviates from the linear dependence, signaling vortex penetration. The H_{c1} enhancement in thin MgB$_2$ films has been studied previously using this technique[12]. V_{eff} for $\delta \ll \lambda$ is very small, thus the experimental resolution of the magnetometers is a serious limiting factor for these measurements.

However the second concept of Gurevich proposal, namely that a thin film can sustain a ΔH between both of its surfaces, cannot be tested using the approach described above because both surfaces of the film are exposed to the same ambient field. In this paper we propose a novel approach that overcomes this fundamental limitation, and concomitantly also solves the resolution and alignment problems (see supplementary information). We have fabricated macroscopic-sized ellipsoids and coated them with MgB$_2$ films. The Meissner effect in the film screens the entire ellipsoid volume from the applied field, so a ΔH develops between the internal and external film surfaces. Here the field is outside of the ellipsoid rather than inside as in a real SRF cavity, thus we call it the "inverse cavity" concept. We use ellipsoids because the demagnetizing effects and boundary conditions are well defined, and in the Meissner state the external field at the ellipsoid surface is parallel to the surface everywhere, the same as in real SRF cavities.

The Nb ellipsoids have the nominal semi axes $a = 4\,\mathrm{mm}$, $b = c = 2.5\,\mathrm{mm}$, made from the same bulk material as presently used in SRF cavities. The measurements were performed in a Quantum Design MPMS SQUID magnetometer. When the applied field **H** is parallel to the i axis ($i = a, b, c$) the calculated "Meissner slope" is $m_{M,i}/H = -V/[4\pi(1 - N_i)] = -ab^2/[3(1 - N_i)]$, where N_i are the demagnetizing factors, such that $N_a < N_b = N_c$ and $N_a + N_b + N_c = 1$.
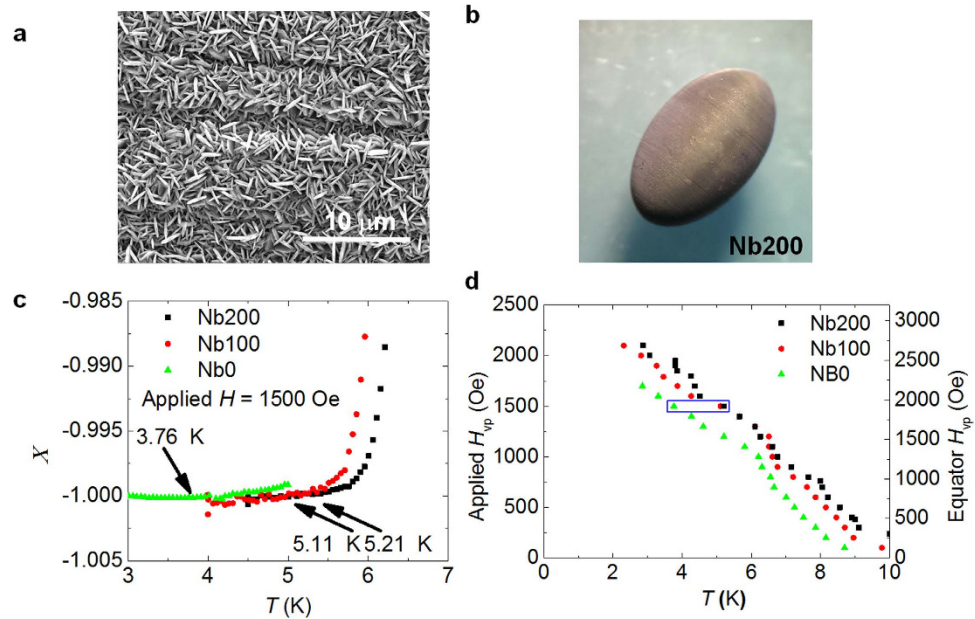
Figure 2. (**a**) SEM image taken on the Nb100 ellipsoid. (**b**) optical image of Nb200 ellipsoid (**c**) m-T curves comparisons between Nb ellipsoids with different thicknesses of MgB_2 coating. ZFC to 1.8 K then apply 1500 Oe field. Arrows indicate the H_{vp} of each sample. (**d**) Comparison of H_{vp}-T curves measured on Nb ellipsoids. Data points in the blue box corresponds to the 3 curves in Fig. 2(c). The actual H field at the ellipsoids equator is calculated on the right y-axis.

Figure 1a shows the schematic of the H_{vp} measurement. Most results in this paper were measured with the applied magnetic field parallel to the long axis of the ellipsoid (top). However, the field alignment to the short axis (bottom) was also measured to confirm the results taking into account the different demagnetizing factors for the two field directions. Figure 1b presents m vs. H at several temperatures for a bare Nb ellipsoid shown in the inset. For each T, the sample was cooled from above $T_c = 9.3$ K to T in $H = 0$ (zero field cooling, ZFC) before the m vs. H measurement. The Meissner slope does not change with T because the variation of the effective superconductor volume due to the change in $\lambda(T)$ is too small compared to the dimensions of the ellipsoid. The solid line in this figure corresponds to the predicted m-H relationship for the ellipsoid with $a = 4$ mm and $b = c = 2.5$ mm in the Meissner state. The m vs. H curves at $T = 5$ K for the Nb ellipsoid are shown in the inset of Fig. 1c for both $\mathbf{H}||a$ and $\mathbf{H} \perp a$. From the slopes of both orientations $m_{M,a}/H$ and $m_{M,b}/H$, we obtained $N_a = 0.1880$ and $N_b = N_c = 0.4060$. The ellipsoid volume was calculated to be $V = 0.1062$ cm^3, in excellent agreement with the designed value (from the weight of this particular ellipsoid we had determined $V = 0.1048$ cm^3).

Although the applied field is uniform, due to the demagnetizing effects the total external field is not. In the Meissner state the total external field at the surface of the ellipsoid is parallel to the surface everywhere, and its magnitude varies along the surface, being zero at the poles and reaching a maximum at equator $H_{eq} = H/(1 - N_i)$, where $i = a, b$. (see Fig. 1a). Consequently, vortex penetration starts at the equator. As seen in the Fig. 1c, the average magnetic induction $<B_i> = 4\pi(1 - N_i)(m - m_M)/V$ of the ellipsoid starts to deviate from zero at the same H_{eq} for both $\mathbf{H}||a$ and $\mathbf{H}||b$ orientations. We define the vortex penetration field H_{vp} as when $<B>$ increases above the noise. The noise level increases with H, reaching about ± 2 G at 1.5 kG, which negatively impact the accuracy of the $H_{vp}(T)$ measurement[13]. This high noise level could be originated from the superconducting magnet in the magnetometer when it was charged between 1000 and 5000 Oe with fine steps[14].

An alternative approach to measure H_{vp} is to apply a field $H < H_{vp}(T)$ after ZFC and then measure $m(T)$. A result is shown in Fig. 1d. As T increases, m initially remains constant at the Meissner value until the vortex penetration occurs, which is signaled by a sudden reduction of the absolute value of m when $H = H_{vp}(T)$. Figure 1e summarizes the $H_{vp}(T)$ results obtained from both $m(H)$ and $m(T)$ measurements. The left and right vertical axes in Fig. 1e show the value of H and H_{eq} for first vortex penetration respectively. The error bars in Fig. 1e stand for the H_{vp} variation when using 5 G and 1 G $<B>$ criterion. The results suggest that the m-T approach is a preferred method for the H_{vp} measurement. At high field, it is more accurate than the m-H technique mainly due to the elimination of the flux creep effect from the superconducting magnet. At low H it is comparable to the m-H technique. Therefore, the m-T technique was used to measure H_{vp} of a bare Nb ellipsoid and two MgB_2 thin film-coated Nb ellipsoids in this work. From Fig. 1e we find that at $T \sim 2$ K vortex penetration starts at $H_{eq} \sim 2200$ Oe, very close to the ideal limit $H_{sh,Nb}(2$ K$) \approx 2280$ Oe, confirming the high quality of the Nb used in our study.

The MgB_2 thin film coating of Nb ellipsoids was performed using hybrid physical-chemical vapor deposition (HPCVD)[15]. Two Nb ellipsoids were coated with MgB_2 layers of 100 nm (Nb100) and 200 nm (Nb200), respectively. Figure 2a shows an SEM image taken at the equator of the ellipsoid Nb100. The film is polycrystalline with grain size of $\sim 1\,\mu$m. The MgB_2 layer covered the entire ellipsoid uniformly without pinholes. An optical image of
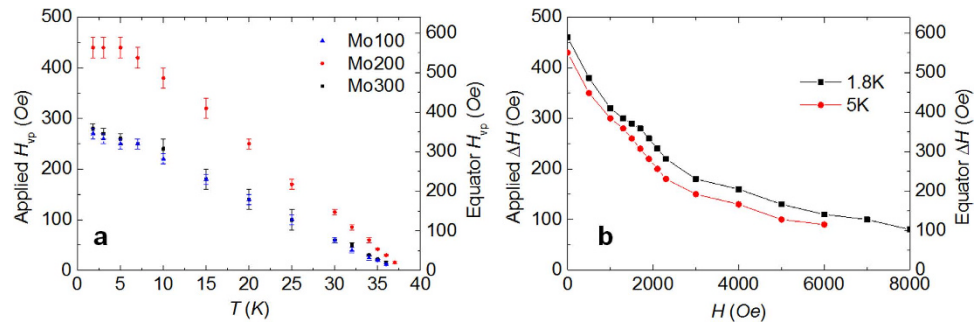
Figure 3. (**a**) The dependence of H_{vp} of the MgB_2/Mo samples on temperature. H_{vp}s of Mo100 and Mo300 are almost overlapped. (**b**) Maximum H difference shieled by a single layer of MgB_2 versus the field inside the MgB_2 shell for Mo200 at 1.8 K and 5 K.

Nb200 is presented as the inset to Fig. 2b. Figure 2c shows the m-T curves for the bare Nb ellipsoid and the Nb ellipsoids coated with 100 nm and 200 nm MgB_2 layers for 1500 Oe applied field. The onset of vortex penetration are marked with black arrows in the figure. With an increasing temperature, vortices penetrate into the bare Nb ellipsoid at 3.76 K. This temperature increases to 5.11 K and 5.21 K for the Nb100 and Nb200 ellipsoid, respectively. By repeating the m-T measurements, the temperature dependence of H_{vp} can be obtained.

Figure 2d summarizes the $H_{vp}(T)$ curves for the bare Nb ellipsoid, Nb100, and Nb200. The three data points within the blue box correspond to the 3 curves in Fig. 2c. The $H_{vp}(T)$ of Nb200 is about 400 Oe higher than the bare Nb ellipsoid in the temperature range from 1.8 K to the T_c of Nb. This increase is approximately constant because the properties of MgB_2 do not change significantly in this temperature range ($T < T_c/4$). The maximum field at the equator that our inverse cavity can sustain before vortex penetration is indicated on the right vertical axis. At $T\sim2.8$ K it is ~2600 Oe, about 500 Oe above the bare Nb ellipsoid.

As an additional test of our inverse cavity concept we deposited MgB_2 films of thickness $d_S = 100; 200$ and 300 nm on non-superconducting molybdenum ellipsoids. For details of the measurements and analysis, see the supplementary material. For the three samples we measured $m(H)$ at several T with **H**$||a$. The Meissner slopes indicate that the full volume of the ellipsoids is screened, implying that the field at the MgB_2-Mo interface is zero. At $H_{vp}(T)$ the field at the interface becomes nonzero and spreads inside the Mo. The obtained $H_{vp}(T)$ curves are shown in Fig. 3a. They extrapolate to zero at the T_c of the MgB_2 films (~38.1; 38.6 and 38.7 K respectively).

As described in detail in the Supplementary Materials, we found out that in all cases H_{vp} at the equator is lower than the prediction for the enhanced H_{c1}, and that the field penetration occurs when the screening current is large enough to eliminate the surface barrier. The fact that H_{vp} in the MgB_2 coated Mo ellipsoids is determined by J rather than H_{c1} is good news for cavity applications, because it implies that H_{vp} is the limit for the *difference* in field that can be sustained between both surfaces of the film, not for the *absolute value* of the field. This is fully consistent with our main experimental finding, namely that by adding an MgB_2 coating we have been able to increase H_{vp} by about 500 Oe on top of the already large penetration field of Nb.

We performed additional studies on the Mo200 ellipsoid to estimate how high H_{vp} could potentially be obtained. After applying a field H_{int} at a temperature above the T_c of MgB_2 (which penetrates homogeneously into the Mo), we cooled down to a measurement T and subsequently increased H. We observed an initial linear $m(H)$ Meissner dependence, indicating that screening currents develop in the MgB_2 that shield the internal Mo volume from the external field variation. Eventually the surface barrier disappears and the field penetrates when the difference between the outside and the inside field, $\Delta H = H - H_{int}$, reaches a value ΔH_{vp}, as summarized in Fig. 3b. The remarkable result is that $\Delta H_{vp} > 0$ even for H_{int} well above the maximum operating fields of Nb cavities. This implies that the operating field of a cavity could be increased by $\Delta H_{vp}/(1 - N_a)$ by internally coating it with this MgB_2 film. For instance, Fig. 3b shows that if a hypothetical cavity were able to sustain $H_{vp}\sim4000$ Oe, at 1.8 K, then this MgB_2 film would further increase that H_{vp} by ~200 Oe.

Our results demonstrate three important facts. First, it is indeed possible to increase the H_{vp} of the Nb material used in the state-of-the-art SRF cavities by a substantial amount (~600 Oe) by coating it with a thin superconducting film that screens vortex penetration. Second, it is technically possible to deposit a thin MgB_2 film with appropriate properties for this purpose on curved bulk Nb. Third, a single layer of superconducting thin film can reduce the magnetic field felt by the bulk material under it. These three facts are enough to demonstrate that it is possible to increase the H_{vp} of existing Nb SRF cavities by ~600 Oe. The superconducting shielding current density at the equator of Nb200 is estimated to be $J\sim\Delta H/d\sim10^7$ A/cm^2, as compared to $J_d\sim10^8$ A/cm^2 reported for MgB_2 thin films[16], therefore the maximum ΔH that a MgB_2 thin film can shield has not been reached. Further, a superconductor/insulating multilayer coating proposed by Gurevich would achieve even higher shielding field ΔH_{total} with MgB_2 films.

Methods

Deposition of MgB$_2$ thin film on Nb ellipsoids. The MgB_2 films were deposited by Hybrid Physical-Chemical Vapor Deposition (HPCVD) technique[15]. The schematic of the deposition technique is presented in Extended Data Fig. 1(a). By heating magnesium pellets above melting temperature and letting magnesium vapor react with boron from the decomposition of diborane gas, this technique has produced the films with the highest quality on both single crystal and metallic substrates[17,18]. In this work, MgB_2 film was deposited at 730 °C in

40 Torr hydrogen atmosphere. The boron source was 20 sccm 5% diborane in hydrogen solution, which gave a growth rate of 55 nm/min. Each ellipsoid was coated three times with rotating 120 degree between each coating to achieve uniform coating. During the first deposition, a piece of $5 \times 5\,mm^2$ silicon carbide (SiC) substrate is put aside of the ellipsoid as a reference for thickness calibration. The nominal thickness of MgB_2 layer coated on the ellipsoid refers to the film thickness on the SiC substrate.

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Acknowledgements

Author Contributions

L.C. first proposed to use coated Nb ellipsoids to study the thin film coated SRF cavities. T. Tan, M.A.W. and X.X.Xi prepared the ellipsoid samples and Figure 2a. L.C. and T. Tan performed the magnetic measurement and prepared all the other Figures of the main text, and Figures 1–3 of the SI. T. Tajima prepared Figure 4 of the SI. T. Tan wrote the first manuscript. All authors reviewed and revised the drafts and contributed to the final manuscript.

Additional Information

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