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Anomalous interface adhesion of graphene membranes

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MECHANICAL PROPERTIES

MECHANICAL AND STRUCTURAL
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In order to understand the anomalous interface adhesion properties between graphene membranes and their substrates, we have developed a theoretical method to calibrate the interface adhesion energy of monolayer and multilayer graphene on substrates based on the bond relaxation consideration. Four kinds of interfaces, including graphene/SiO₂, graphene/Cu, graphene/Cu/Ni and Cu/graphene/Ni, were taken into account. It was found that the membrane thickness and the interface confinement condition determine the adhesion energy. The relationship between the critical interface separation and the graphene thickness showed that the interface separation in the self-equilibrium state drops with decreasing membrane thickness. The size-dependent Young's modulus of graphene membrane and the interfacial condition were responsible for the novel interface adhesion energy. The proposed theory was expected to be applied to the design of graphene-based devices.

Graphene has received special attention in recent years because of its exceptional electronic, mechanical and thermal properties from both fundamental scientific issues and potentially technological applications including biosensors, nanomechanical and nanoelectronic devices, etc.^{1,2}. Supported on a substrate, the interfacial interaction between graphene and its substrate has been one of the key questions from both scientific and technological impetuses^{3,4}. Up to now, a number of theoretical^{5–8} and experimental^{9–12} methods have been employed to address the interface adhesion energy between graphene and different types of substrates and further explore the underlying mechanism. Strikingly, the available results with regard to the adhesion energies in graphene membranes show the evident thickness dependence. For instance, Koenig *et al.*¹⁰ measured the adhesion energy is 0.45 ± 0.02 J/m² for monolayer graphene on SiO₂, which is higher than that of 0.31 ± 0.03 J/m² for multilayer graphene with 2–5 layers using a pressurized blister test. Yoon *et al.*¹³ reported the adhesion energy of monolayer graphene on Cu is 0.72 ± 0.07 J/m² by double cantilever beam fracture mechanics testing. On the other hand, according to the experimental configurations some researchers modeled the mechanics of a single layer of graphene adhered to a substrate^{14–16}, and others studied the effect of membrane thickness and surface forces on the adhesion energy of graphene membranes grown on different substrates^{17–21}. In addition, the substrate roughness (e.g., 1D sinusoidal surface grooves of the underlying substrate) has also been considered on interface interaction of graphene membranes^{22–24}.

Despite recent progress in the fabrication and characterization of graphene membranes grown on different substrates, little is yet known about the elastic strain energy stored in the graphene owing to surface relaxation and its contribution is usually ignored easily. Furthermore, with shrinking the solid size of a material to nanoscale, a variety of physical quantities of graphene membranes will be changed^{25–27}. The atomic identities such as nature, length and strength of nanostructures deviated from the bulk case. Atoms at surface and interface regions have less atomic coordination numbers (CNs) and will become shorter and stronger^{27–29}. For example, Lee *et al.*³⁰ reported that the measured values of Young's modulus of single- and bilayer graphene, respectively, are 2.4 ± 0.4 and 2.0 ± 0.5 TPa, which is much larger than that of the bulk counterpart (~ 1.02 TPa)³¹. Moreover, Huang *et al.*³² calculated the thickness of graphene and single-wall carbon nanotubes directly from the interatomic potential and found the thickness and the related elastic moduli also depend on type of loading.

Accordingly, the lattice strain will take place spontaneously owing to large ratio of uncoordinated atoms located at the end parts and associated with higher energy state compared with the bulk counterpart.

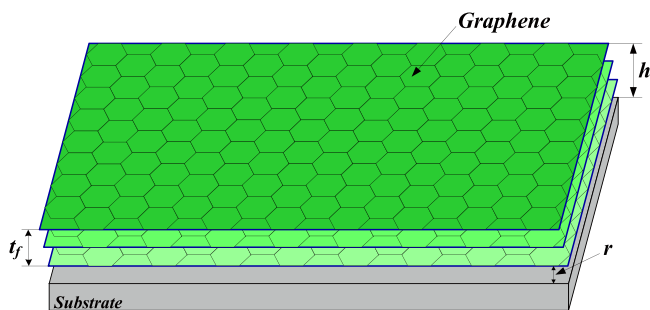


Figure 1 | Schematic illustration of a multilayer graphene on substrate. t_f is the thickness of graphene membrane, r is the interface separation between graphene and substrate, $h = r + t_f$ is the height between the top layer of graphene and the substrate.

Importantly, the interface adhesion energy and other physical-chemical properties, including band offset and mechanical modulus, are determined on the self-equilibrium strain^{19,33–35}. Therefore, it is necessary to put forward a comprehensive understanding between lattice strain and interface adhesion energy in graphene membranes under self-equilibrium state from the perspective of atomistic origin.

Focusing on the adhesion energy of substrate-supported graphene membranes, in this paper we develop a quantitative analytical method that describes the effects original from surface relaxation and interface misfit based on the atomic-bond-relaxation (ABR) consideration. Taking into account the free energy contributions including elastic strain energy stored in graphene membranes and van der Waals interaction between graphene and its substrate, we demonstrate that the adhesion energy depends on the membrane thickness and Young's modulus of graphene. The interface interaction is determined on the various system parameters. Our theoretical results suggest that the interface adhesion energy can be modulated via membrane thickness and various interface confinement conditions. Furthermore, the validity of our method is confirmed by the available evidences.

The schematic illustration of a multilayer graphene with volume V_0 , area A_g , and thickness t_f grown on a substrate is shown in Fig. 1. r and h , respectively, are the distance between the film and the substrate, and the height between the top surface layer and the substrate. Theoretically, the total free energy U_{total} of the graphene membrane can be divided into the van der Waals interaction energy U_{vdw} and the elastic strain energy U_e , i.e.,

$$U_{total} = U_{vdw} + U_e \quad (1.1)$$

Notably, the van der Waals interaction between a carbon and a substrate atom can be expressed by Lennard-Jones potential^{19,36}: $W_{LJ} = -C_1/r^6 + C_2/r^{12}$, where r is the distance between two atoms, C_1 and C_2 are the constants for the attractive and repulsive interactions. In general, we can assume that the interfacial van der Waals interaction between the substrate and the first graphene layer is predominant because the corresponding separation is much larger than the C-C bond length. Thus, the total interaction potential between graphene and substrate can be obtained by integrating all the atoms of film and substrate¹⁹: $W = \int_{A_g} \int_{V_s} W_{LJ} \rho_s \rho_g dV_s dA_g$, where ρ_g represents the number of atoms per unit area of the monolayer graphene, ρ_s is the number of atoms per unit volume of the substrate and V_s is the substrate volume. Thus, the interfacial potential energy can be yielded as

$$U_{vdw} = -\Gamma_0 \left[\frac{3}{2} \left(\frac{r_0}{r} \right)^3 - \frac{1}{2} \left(\frac{r_0}{r} \right)^9 \right] \quad (1.2)$$

where r_0 and Γ_0 denote the interface separation under equilibrium state and the intrinsic adhesion energy per unit area in the bulk case, respectively¹⁹.

On the other hand, according to the continuum mechanics principle, the strain energy per unit area stored in graphene membranes can be given as

$$U_e = \frac{Y(t_f) t_f \epsilon_f^2}{1 - \nu} \quad (1.3)$$

where $Y(t_f)$ and ν are the thickness-dependent Young's modulus and the Poisson's ratio of the graphene membranes, respectively.

Physically, the strain stimulated by the surface and interface effects in nanostructures is one of the importantly fundamental quantities to a wide range of domains owing to inducing novel optical, electronic and mechanical properties as compared to those of the bulk counterpart^{37,38}. For example, the bulk elastic moduli of nanoparticles have shown strain effects induced by the solid sizes and external stimuli such as pressure and temperature³⁹. The related approach demonstrates that the mechanical modulus can be influenced by less-CN's and interlayer relaxation, which provides information on the measurable quantities and the atomic bond identities³⁹. For graphite and graphene membranes, the well-studied bulk graphite offers a well-defined parameterization: a Young's modulus of 1.02 TPa and a interlayer distance of 0.335 nm. However, this viewpoint does not scale down to the monolayer^{40,41}. For example, Zhang *et al.*⁴¹ found that the thicknesses of graphene membranes decrease from 0.331 to 0.082 nm with decreasing layers from five to one. It demonstrated that the bulk value of interlayer separation (0.335 nm) for graphite cannot be suitable for the graphene membranes. In addition, the effective CN's for bulk graphite is 5.335 based on the bond contraction relation by using a length of 0.142 nm for the C-C bond in graphite⁴². Therefore, in terms of the strain-dependent bulk elastic modulus of nanoparticles and taking further the strains original from the surface and interface effects into account, we can derive the Young's modulus of graphene membranes, i.e.,

$$Y(t_f) = \frac{z_b}{\langle z \rangle} \left[\sum_{i < n} \gamma_i (z_{ib} c_i^{-m} - 1) + 1 \right] Y_B (1 + \epsilon_f)^{-3} \quad (1.4)$$

where Y_B is the Young's modulus of the bulk counterpart, $m = 2.56$ is the bond nature indicator²⁵. $\gamma_i = \sum_{i < n} c_i h_0 / t_f$ is the surface-to-volume ratio, $\langle z \rangle = \gamma_i (z_i - z_b) - z_b$ and z_b are the mean CN's of the graphene and that of the bulk.

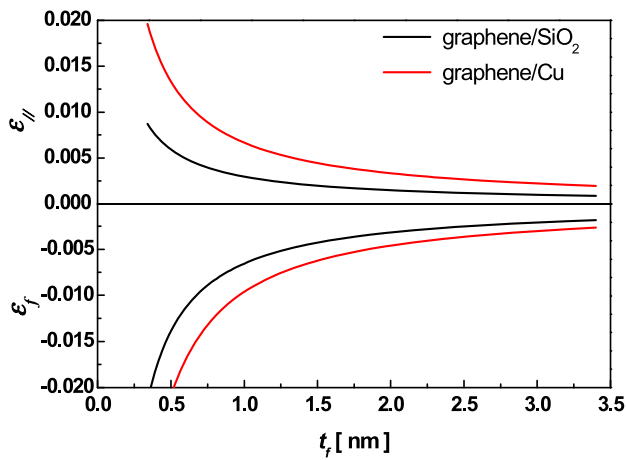
Considering the lattice strains induced by surface relaxation and interface misfit, as well as the van der Waals interaction between the graphene membrane and its substrate, the graphene membrane will be a self-equilibrium state, and the relationship between the critical interface separation r^* and the membrane thickness t_f can be obtained by setting $\partial U_{total} / \partial h = \partial U_{vdw} / \partial r + \partial U_e / \partial t_f = 0$. Thus, we have

$$r^* = r_0 \left[\left(\frac{r_0}{r^*} \right)^4 + \frac{2r_0}{9\Gamma_0} \frac{\partial U_e}{\partial t_f} \right]^{-1/10} \quad (1.5)$$

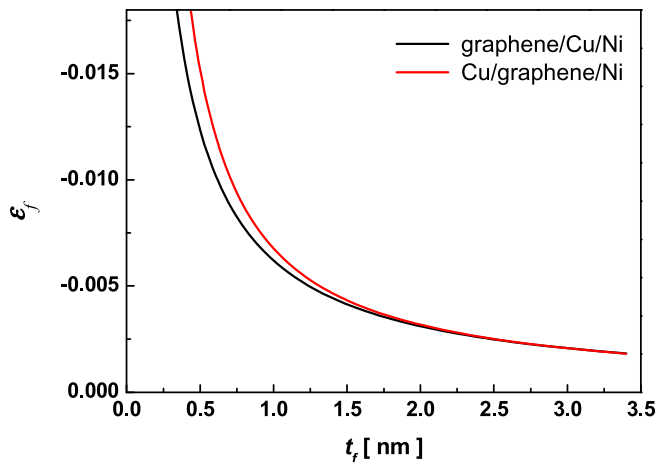
with

$$\frac{\partial U_e}{\partial t_f} = \left[\sum_{i < n} \frac{\gamma_i (z_i - z_b)}{\langle z \rangle} Y(t_f) - \frac{z_b}{\langle z \rangle} \left(\sum_{i < 3} \gamma_i (z_{ib} c_i^{-m} - 1) \right) Y_B (1 + \epsilon_f)^{-3} - \frac{3Y(t_f)(\epsilon_{//} - \epsilon_f)}{(1 + \epsilon_f)} \right] \frac{\epsilon_f^2}{1 - \nu} + \frac{\epsilon_f^2}{1 - \nu} Y(t_f) + \frac{2\epsilon_f(\epsilon_{//} - \epsilon_f)}{1 - \nu} Y(t_f)$$

Consequently, the total free energy per unit area of the graphene membrane in self-equilibrium state can be obtained



(a)



(b)

Figure 2 | Thickness-dependent mean strains of (a) in-plane in graphene/Cu, graphene/SiO₂, and the membranes, (b) in-plane in Cu/graphene/Ni, graphene/Cu/Ni, and the membranes.

$$\tilde{U} = \Gamma_0 \left[\frac{3}{2} \left(\frac{r_0}{r^*} \right)^3 - \frac{1}{2} \left(\frac{r_0}{r^*} \right)^9 \right] + \frac{Y(t_f)t_f \varepsilon_f^2}{1-\nu} \quad (1.6)$$

Results

Single interface. In order to address the interface adhesion energy between graphene membrane grown on a substrate, we take

graphene/SiO₂ and graphene/Cu(111) with single interface and graphene/Cu/Ni and Cu/graphene/Ni with complex interfaces as examples to check the validity. Note that in our cases we assume that the graphene membranes are grown on the purity substrate as depicted in Figure 1.

Using Eq.(2.1) and (2.2), we first calculate the thickness-dependent in-plane strains in graphene/Cu(111) and graphene/SiO₂ as well as the total strains in graphene membranes, as shown in Figure 2(a). The necessary parameters are listed in Tables 1. It is clear to see that both of the in-plane strains and the total strains in these two types of systems increase gradually with decreasing thickness. He *et al.*³⁴ measured the strain in graphene on Cu(111) and found the mean compressive strain is 0.5% for the C-C bond length according to the Raman spectroscopy analysis. Evidently, the variation trend is consistent with our calculations. Also, the compressive strain in graphene/Cu is larger than that in graphene/SiO₂ at fixed thickness owing to the different mismatch existing in two systems. Thus, it is concluded that the compressive strains in these two systems are mainly contributed to the coordination number imperfections in surface and the mismatched lattice in interface.

Complex interface. On the other hand, Figure 2(b) shows the thickness-dependent mean strains of graphene membranes in graphene/Cu/Ni (the black line) and Cu/graphene/Ni (the red line), respectively. Clearly, the total strains of graphene in graphene/Cu/Ni and Cu/graphene/Ni increase with decreasing membrane thickness. It should be noted that the in-plane strain of graphene in graphene/Cu/Ni system can be calculated as follows: according to the definition of lattice strain, the in-plane strain of Cu is $\varepsilon_{Ni-Cu} = \varepsilon_{m1}(\varepsilon_{m1} + 1)h_{Cu}/t_m$, where ε_{m1} is the mismatch strain between Ni and Cu, and h_{Cu} is the mean bond length of Cu. Similarly, we can obtain the in-plane strain of the graphene, i.e., $\varepsilon_{||} = \varepsilon_{m2}(1 + \varepsilon_{m2})h_0/t_f$, here $\varepsilon_{m2} = (a_{Cu}(1 + \varepsilon_{Ni-Cu}) - a_f)/a_f$ is the mismatch strain between Cu and graphene, a_{Cu} is the lattice constant of Cu. In addition, in the case of Cu/graphene/Ni, the in-plane strain can also be obtained as following: the in-plane strain of graphene in graphene/Ni interface is $\varepsilon_{Ni-C} = \varepsilon_{m2}(\varepsilon_{m2} + 1)h_0/t_f$, and the in-plane strain of graphene in graphene/Cu interface is $\varepsilon_{Cu-C} = \varepsilon_{m3}(\varepsilon_{m3} + 1)h_0/t_f$, where ε_{m2} and ε_{m3} are, respectively, the mismatch strains in Ni/graphene and Cu/graphene. Therefore, the in-plane strain of graphene in Cu/graphene/Ni system can be given by $\varepsilon_{||} = (\varepsilon_{m2}(\varepsilon_{m2} + 1)h_0 + \varepsilon_{m3}(\varepsilon_{m3} + 1)h_0)/t_f$.

In our case we assume the Cu has a single layer in those two complex systems, which is in accord with Lahiri's consideration¹². Similarly, Murayama⁴³ reported that the misfit strain of Co layer in Cu/Co/Au/Cu(111) system increases with increasing Au-interlayer thickness and found that the in-plane strain in Co layer at the Co/Au interface gradually decreases as the Co thickness increases. Thus, it implies that the middle layers play the crucial role in the complex system.

Discussion

It is noted that the strain induced by surface effect and interface confinement condition of membranes would change the mechanical modulus due to different bond identities compared with the bulk

Table 1 | Input parameters for calculations. r_0 , a , h_0 , E , ν and Y_B are the interface equilibrium distance, in-plane lattice constant, bond length, binding energy per unit area, Poisson's ratio and Young's modulus, respectively

	r_0 [nm]	a [nm]	h_0 [nm]	E [meV/Å ²]	ν	Y_B [TPa]
Graphene	0.34 ³¹	0.2445 ⁶	0.142 ⁴		0.16 ¹⁰	1.0 ³¹
SiO ₂		0.499 ⁵¹				
Cu		0.256 ⁹	0.2556 ²⁶		0.34 ²⁶	0.14 ²⁶
Ni		0.2436 ¹²				
Graphene/SiO ₂	0.3 ⁵⁰			17.01 ⁵⁰		
Graphene/Cu	0.326 ^{6,15}			13.19 ^{6,15}		

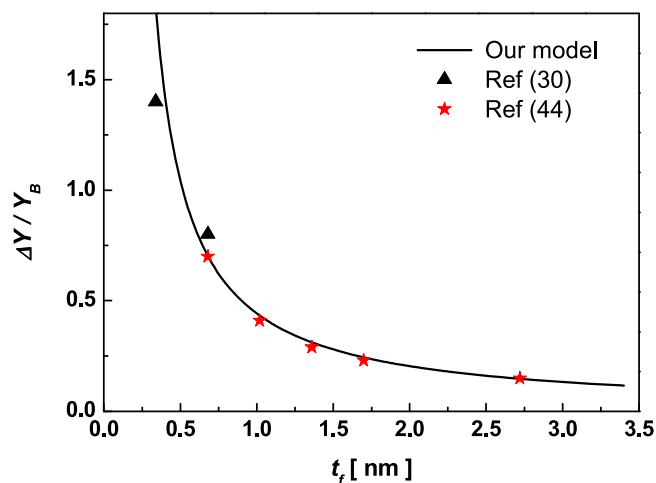


Figure 3 | Thickness dependence of the relative change of Young's modulus. The solid line denotes the consequence of Eq. 1.4. The symbols in (a) represent the experimental results and calculations^{30,44}.

counterpart. Using Eq.(1.4), we calculate the thickness-dependent Young's modulus ($Y(t_f)$) of graphene membranes, as shown in Figure 3. It is found that the Young's modulus of graphene membrane increases dramatically with decreasing graphene thickness. Lee *et al.*³⁰ demonstrated that the Young's modulus of single- and bilayer graphene are 2.4 ± 0.4 and 2.0 ± 0.5 TPa. Also, Tu *et al.*⁴⁴ calculated the Young's modulus of multiwalled carbon nanotubes using local density approximation, and obtained the Young's modulus are, respectively, 1.7, 1.41, 1.29, and 1.23 TPa for 2–5 layers and 1.15 TPa for 8 layers. Importantly, our predictions are exceedingly well agreement with the experimental measurements and theoretical calculations.

Furthermore, the thickness dependence of Young's modulus will lead to the changes of elastic strain energy and total free energy of graphene membranes. Figure 4(a) shows the thickness-dependent van der Waals interaction energy and elastic strain energy in graphene/SiO₂. Noticeably, these two energies show the opposite variation with thickness. Also, Figure 4 (b) shows the relationship among the total free energy, the number of layers and the interface separation in graphene/SiO₂. Strikingly, the minimum of total free energies have obvious shift with number of layers of graphene membranes. Meanwhile, the relationship between the critical interface separation and the membrane thickness based on Eq. (1.5) is shown in Figure 4(b). Surprisingly, the variation of interface separation becomes lower with decreasing membrane thickness. When the thickness goes to infinite, the $r^* \rightarrow r_0$. Therefore, it is concluded that the interface separation is influenced by the elastic relaxation of membrane. At the equilibrium state, the total free energy is negative, and the interface adhesion energy can be calculated as $\Gamma = -U_{total}(t_f)$. As illustrated in Figure 4 (c), the interface adhesion energy of graphene/SiO₂ shows the evident thickness effect. Clearly, the interfacial adhesion energy increases as the thickness decreases, which agrees very well with the experimental observations¹⁰.

Compared with the graphene/SiO₂, the case of graphene/Cu shows the similar interface adhesion properties shown in Figure 5. The adhesion energy in graphene/Cu decreases with increasing membrane thickness, while the interface separation between graphene and Cu becomes larger with increasing thickness. However, the shift of interface separation is wider than that in graphene/SiO₂. The main reason is that the mismatch in graphene/Cu is larger than that in graphene/SiO₂. Thus, the elastic strain energy stored in graphene/Cu at self-equilibrium state is more remarkable compared to that in graphene/SiO₂. Yoon *et al.*¹³ measured the adhesion energy of graphene/Cu is 0.72 ± 0.07 J/m², which is larger than that of $0.45 \pm$

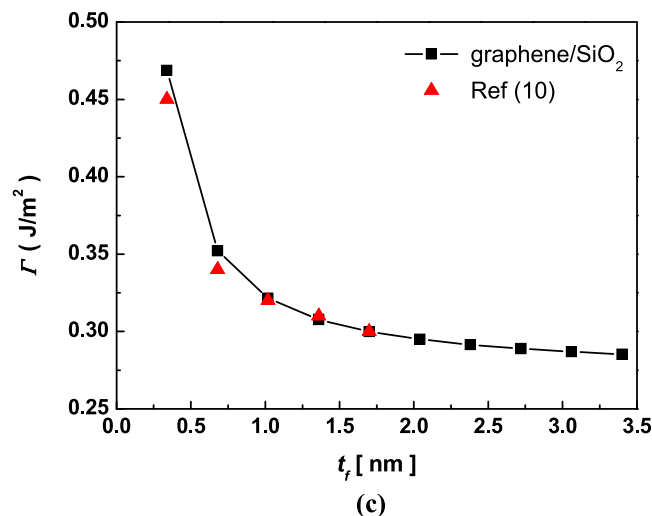
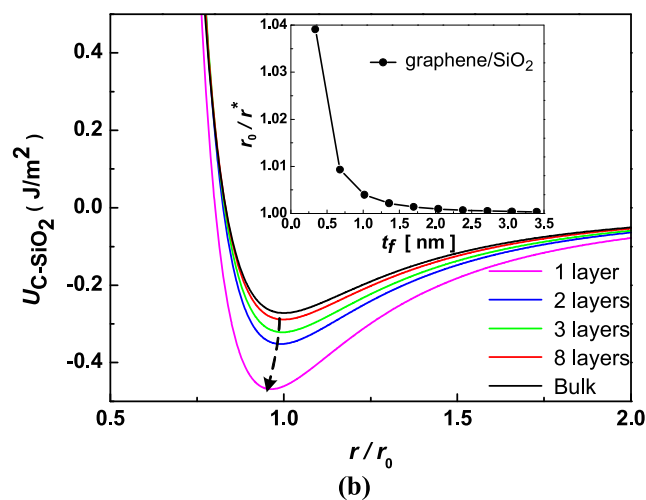
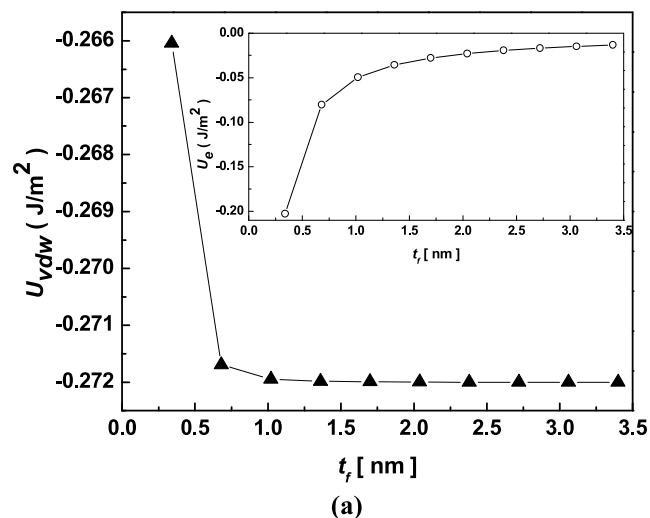


Figure 4 | Thickness-dependent interface van der Waals interaction of graphene/SiO₂ in (a), the total free energy of graphene/SiO₂ as a function of interface separation in (b), and thickness-dependent adhesion energy of graphene/SiO₂ in (c). The inset in (a) is the elastic strain energy stored in graphene membranes grown on SiO₂ under self-equilibrium state. The inset in (b) is the relationship between the critical interface separation and the membrane thickness. The symbols shown in (c) are the results measured by a pressurized blister test¹⁰.

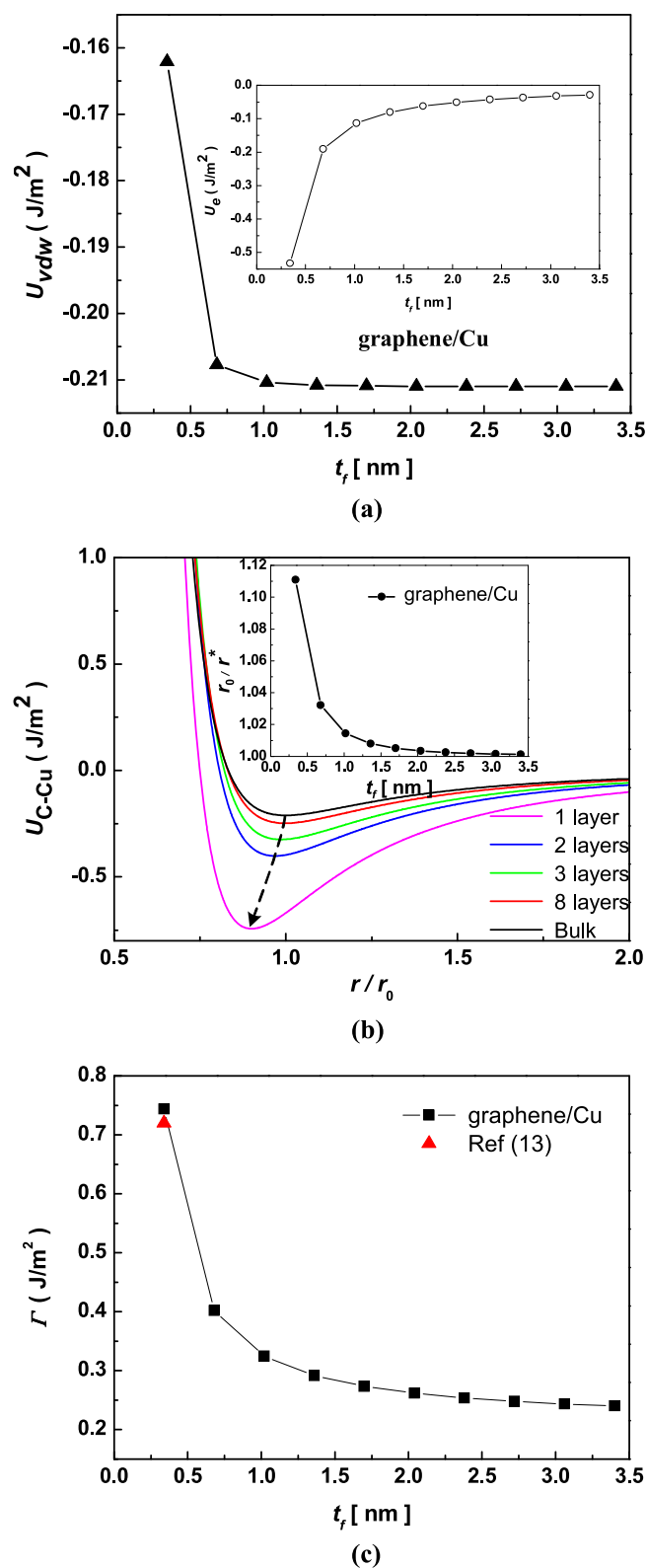


Figure 5 | Thickness-dependent interface van der Waals interaction of graphene/Cu in (a), the total free energy of graphene/Cu as a function of interface separation in (b), and thickness dependent adhesion energy of graphene/Cu in (c). The inset in (a) is the elastic strain energy stored in graphene membranes grown on Cu under self-equilibrium state. The inset in (b) is the relationship between the critical interface separation and the membrane thickness. The symbols shown in (c) are the results measured by double cantilever beam fracture mechanics testing¹³.

0.02 J/m² in graphene/SiO₂. The possible mechanism is that the electronic density in graphene/Cu interface is more remarkable than that in graphene/SiO₂. Therefore, the interatomic force between graphene and Cu becomes stronger than the typical van der Waals force between graphene and SiO₂. In our case, we take the combination from the interface misfit and surface relaxation in the graphene/substrate system, and further predict that the size-dependent adhesion energy in graphene/Cu and obtain the adhesion energies are 0.74, 0.40, 0.32, 0.29 and 0.27 J/m² for the graphene thickness change from 1 layer to 5 layers. In addition, Lahiri *et al.*¹² calculated the adhesion energy of Ni/graphene/Ni using density functional theory. They found that the adhesion energy can be expressed as a function of the thickness of Ni overlayer, from 3.5 to 3.0 J/m² for the monolayer to three layers in Ni (overlayer)/graphene/Ni (substrate), which shows the size-dependent adhesion energy in the complex interface, and suggested that the overlayer has a large impact on interfacial adhesion energy.

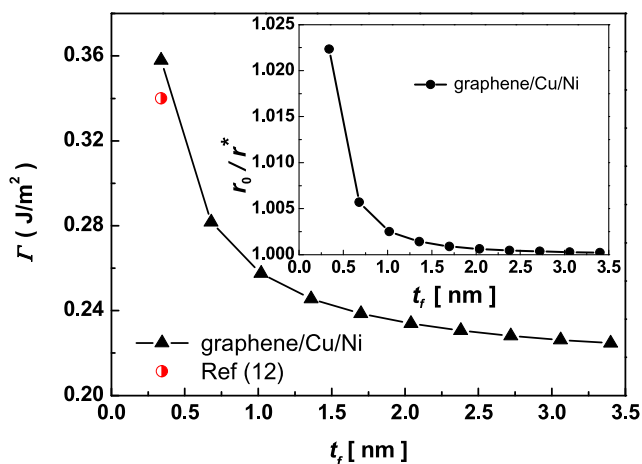
To further confirm the consistency of our analysis, we consider the complex interface conditions in our case. Taking graphene/Cu/Ni and Cu/graphene/Ni as two examples in our considerations, we plotted the graphene thickness-dependent adhesion energy shown in Figure 6. Interestingly, we show that the interface separations between graphene and Cu in graphene/Cu/Ni and Cu/graphene/Ni are different despite they show the same trends in comparison with other cases. Lahiri *et al.*¹² found the adhesion energy and the interfacial separation between graphene and Cu are 0.34 J/m² and 0.312 nm in graphene/Cu/Ni whereas those are 0.51 J/m² and 0.291 nm in Cu/graphene/Ni. The underlying mechanism is that the electronic density of Cu/graphene interface in Cu/graphene/Ni becomes larger than that of graphene/Cu interface in graphene/Cu/Ni, which leads to the results of adhesion in those systems different from each other. Interestingly, these results are consistent with our calculations. In fact, there are two types of interfaces in Cu/graphene/Ni, i.e., Cu/graphene and graphene/Ni. The coupling role original from two mismatch strains of Cu/graphene and graphene/Ni determines the equilibrium state of the system. Nevertheless, in graphene/Cu/Ni system, there is only a single interface that influences the final equilibrium state. Noticeably, the roles of Ni and Cu layers cannot be ignored. This is due to the mismatch between Cu and Ni would affect the Cu layer and further change the total free energy. Apparently, as plotted on Figure 6(a) and 6(b), the adhesion energy of Cu/graphene/Ni is larger than that of graphene/Cu/Ni owing to the difference of elastic properties, such as Young's modulus, Poisson's ratio and strain energy of the two systems. Therefore, the coupling role from surface and interface conditions has great effect on the interface adhesion properties in graphene membranes.

In summary, we have studied the interface adhesion energies of the graphene membranes on SiO₂ and Cu substrates with single interface (graphene/Cu and graphene/SiO₂) as well as Cu/graphene/Ni and graphene/Cu/Ni with complex interfaces on the basis of ABR consideration. Our theoretical results showed that the interface feature and the thickness effects play the dominant role for the interfacial adhesion energy in both of single and complex interfaces. The elastic relaxation energy stored in graphene membranes at the self-equilibrium state affects the physical properties such as the Young's modulus and the equilibrium separation between graphene and substrate. Likewise, different interface conditions would lead to the changes of adhesion energy. The theoretical predictions were consistent with the experimental measurements and the relevant calculations, which suggested that the developed method could be regarded as a theoretical tool to design the interface adhesion of graphene membranes in graphene-based nanomechanical and nanoelectronic devices.

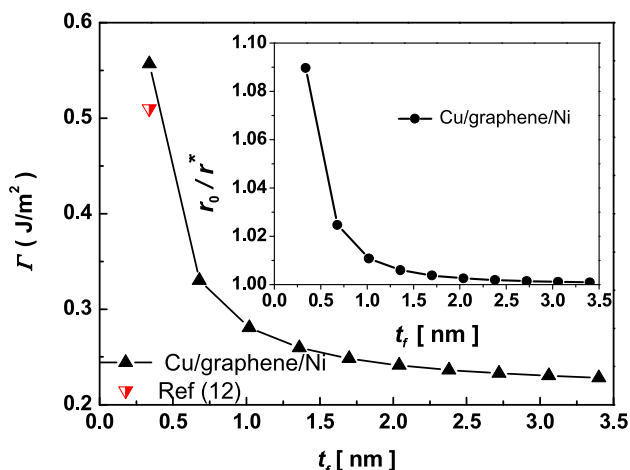
Methods

General consideration on the strain energy stored in graphene membranes.

According to the continuum mechanics, the mismatch strain in the interface will be taken place due to the lattice parameter difference between the graphene membranes



(a)



(b)

Figure 6 | Dependence of adhesion energy on the membrane thickness for (a) graphene/Cu/Ni and (b) Cu/graphene/Ni. The insets in (a) and (b) are the relationship between the critical interface separation and the membrane thickness. The symbols shown in the (a) and (b) are from the experimental measurements¹².

and their substrates. It can be usually expressed as: $\varepsilon_m = (a_s - a_f)/a_f$. Thus, the compatibility of the deformation of two layers is determined by^{45,46}, $\varepsilon_f - \varepsilon_m = \varepsilon_s$, where ε_f and ε_s are the mean biaxial strain stored in the in-plane direction of film and that in the substrate, respectively. In addition, the atomic bond length in the surface would contract spontaneously upon the elastic strain on account of imperfect coordination, which is under a more active energy state differently from that in the region of interface^{28,47,48}. Therefore, the total strain stored in the graphene is

$$\varepsilon_f = \left(\sum_{i < n} \varepsilon_i h_i + \varepsilon_{//} (t_f - \sum_{i < n} h_i) \right) / t_f \quad (2.1)$$

with

$$\varepsilon_i = c_i - 1$$

where ε_i is the strain in the surface layer, $\varepsilon_{//}$ is the strain in the interface layer, n is the number of layers, t_f and h_0 represent the thickness of a film and the average bond length in bulk. Based on the bond length and bond energy correlation, the bond contraction coefficient $c_i = 2 / (1 + \exp((12 - z_i) / 8z_i))$, with z_i being the effective CNs in the i th atomic layer⁴⁹. In addition, the $\varepsilon_{//}$ can be calculated as

$$\varepsilon_{//} = \frac{(1 + \varepsilon_m) \varepsilon_m h_0}{t_f} \quad (2.2)$$

Assuming the deformation of the substrate can be ignored, i.e., the lattice strain in the substrate is zero ($\varepsilon_s = 0$), the strain energy will be concentrated in the graphene membranes. Therefore, the strain energy per unit area is given by

$$U_e = \frac{Y(t_f) t_f \varepsilon_f^2}{1 - \nu} \quad (2.3)$$

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Author contributions

Y.H., W.F.C. and W.B.Y. established the theoretical models and plotted all the figures. Y.H. wrote the paper. G.O. and G.W.Y. supervised the project and revised the paper. All authors discussed the results and commented on the manuscript.

Additional information

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