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Emission and performance analysis of diesel engine running with CeO₂ nanoparticle additive blended into castor oil biodiesel as a substitute fuel

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The implications of adding cerium oxide (CeO₂) nanoparticles as a fuel additive to a castor oil biodiesel–diesel fuel blend on engine performance and emissions in a single-cylinder four-stroke diesel engine under various speed were examined in the current study. The test fuels used were fossil diesel fuels, B5 blend biodiesel (as 5% biodiesel and 95% diesel), B10 blend biodiesel (as 10% biodiesel and 90% diesel), B15 blend biodiesel (as 15% biodiesel and 85% diesel), B20 blend biodiesel (as 20% biodiesel and 80% diesel), and B25 blend biodiesel (as 25% biodiesel and 75% diesel), with cerium oxide (CeO₂) nanoparticle additive (75 ppm). The result of the physio-chemical properties of the oil samples was within the limit of the ASTM standard. The addition of CeO₂ nano additive to the biodiesel–diesel blends has demonstrated a significant reduction in emission and increased in engine performance for all biodiesel–diesel blends for the engine operating speed range. From the result B25 have the maximum reduction rate in BSFC and B10 have the minimum reduction rate in BSFC. The average maximum increment of thermal efficiency was 22.2% for B10 with CeO₂ inclusion. CO emission increased as engine speed increased. HC emission was reduced for all blend, with and without CeO₂ nano additions as speed increased. Maximum NO_x emission was seen at the rated speed of 2700 rpm without nano additive and at 2900 rpm with nano additive. CeO₂ nano additive reduced the soot opacity by 11.56% for all biodiesel–diesel blends for the engine operating speed range. As the objective of this study the results indicates CeO₂ nano additive reduced emissions and improved the performance. So, using sustainable biodiesel–diesel blends made from castor oil with CeO₂ nano additive advisable in ideal operating conditions for diesel engines.

Keywords Performance, Emission, CeO₂, Biodiesel

List of symbols

ASTM	American society for testing and materials
B10	10% Biodiesel and 90% diesel
B15	15% Biodiesel and 85% diesel
B20	20% Biodiesel and 80% diesel
B25	25% Biodiesel and 75% diesel
B5	5% Biodiesel and 95% diesel
BSFC	Brake specific fuel consumption
BTE	Brake thermal efficiency
CeO ₂	Cerium oxide
CI	Compression ignition
CO	Carbon monoxide

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CO ₂	Carbon dioxide
DI	Direct injection
FFA	Free fatty acid
HC	Hydrocarbons
NaOH	Sodium hydroxide
NO _x	Nitrogen oxides
UHC	Unburned hydrocarbons

The world's energy demand occasionally increases significantly due to population growth, the development of new infrastructure, and technological developments^{1,2}. Diesel engines have higher braking thermal efficiency than gasoline engines and use less fossil fuel. Petroleum diesel is used extensively in a variety of industries. However, overall petroleum reserves are dwindling on a daily basis as a result of indiscriminate extraction, extravagant consumption and massive emissions^{3–6}. Numerous academics have been compelled to look for alternate energy alternatives due to the global energy demand^{7–9}. Fossil fuels like coal or petroleum are currently used to meet this increasing energy demand^{10–12}. As a result, the researchers believe that biodiesels are a feasible alternative to diesel fuel in diesel engines. Biodiesel can be made from a variety of renewable feedstocks, including edible oils such as palm oil, sunflower oil, and peanut oil, as well as non-edible oils such as castor, jatropha, cotton seed, and waste plastic oil^{3,13–15}.

Castor (*Ricinus communis* L.) is non edible oilseed crop adapted to dry lands of tropics and semi-arid tropics. In Ethiopia, Castor grows as annual in the low lands to small tree perennial in the high lands¹⁶. Vegetable oils are the most commonly used feedstocks in the extraction and production of biodiesel. Among these, castor oil offers two intriguing properties as a raw material for biodiesel: it doesn't compete with cooking oils and its growth doesn't require a lot of inputs¹⁷.

Among the different strategies available to reduce exhaust emissions, the use of fuel-borne catalysts is now being prioritized due to the benefits of increased fuel efficiency while lowering hazardous greenhouse gas emissions and health-threatening compounds^{18–21}. Recent research focused on alternative fuels and additives to improve engine performance and reduce emissions^{22,23}. CeO₂ nanoparticles promote combustion temperature at the time of reactions with oxygen and the engine power output is improved^{24,25}. Due to their similar characteristics to those of diesel, alternative fuels, in particular biodiesel and different additives, could eventually replace them^{26,27}.

Based on recent literature, the most common performance property was investigated by varying percentages of biodiesel and by adding different percentages of nanoparticle additives. Because biodiesel has a lower volatility and a higher viscosity, its highest cylinder pressure decreases as the amount of biodiesel in the blend increases^{28,29}. The use of Al₂O₃, CeO₂ and copper oxide as an additive increased cylinder pressure because those additives have oxygen in its molecule in addition to the oxygenated biodiesel, which accelerates the combustion process that leads to increased power and torque output^{30,31}. Because the metal-based nano additions are oxygenated, they raise the cetane number. Due to its oxygen content, one of these, the well-known metal oxide nano-additive cerium oxide, displays a notable redox response. Its reaction with carbon atoms, HC molecules, and CO molecules in soot produces large amounts of oxygen, allowing the fuel to burn entirely³².

Vegetable oils have less sulfur content, high cetane numbers, are highly oxygenated, have greater combustion efficiency, and a less amount of emission when they mix with the nano particles³³. According to recent research findings, nanoparticles can be used as an inventive diesel addition to enhance engine efficiency. Studies using a single diesel engine and a diesel–biodiesel mixture made from castor that has high CO and HC emissions are what led to the research gap in this area. As a result, it is critical to evaluate castor diesel–biodiesel blends with 75 ppm CeO₂ nanoparticles to minimize emissions and improve engine performance. This study's objectives include reducing emissions, using sustainable biodiesel–diesel blends made from castor oil, and determining the ideal operating conditions for diesel engines.

The novel idea of the present work lies in producing castor biodiesel by the optimization process and mixing with CeO₂ nanoparticles and formulating the nano-based bi-compound fuel additive to improve the fuel quality, engine functionality, and reduction of harmful exhaust emissions from diesel engine. The present investigation witnessed the ability of nano particles in boosting up the engine combustion performance and reduction of harmful emissions. The other novel finding of this research work was, the engine rated speed where the maximum torque achieved were at 2700 rpm. Hence, the rated engine speed is determined by the type of fuel blends and additives.

Materials and methods

Extraction of oil and preparation of biodiesel

In this research work, Castor seeds were used, as a feedstock for the synthesis of biodiesel, which were bought from farmers of the local market. The extraction process employed were solvent method and hydraulic press as shown in Fig. 1. During solvent method of extraction seeds were crushed, and soaked for forty-eight hours after stirred frequently and wait for some time to settle then filter paper was used for filtering to separate from the residue. For the bulk production of oil, a hydraulic press was used. During the extraction oil from 34 kg of castor seed the yield was 12.5 L. In this study castor seed have yield of 367.6 ml/kg. During the extraction process of the oil, the yield was 28% (v/w) and 51% (v/w) for the solvent method and hydraulic press method respectively.

Before the synthesis of the biodiesel from the parent oil of Castor seeds, it was mandatory to determine the free fatty acid (FFA) whether the process has to undergo through esterification or transesterification reaction. The parent oil's acid value was 4.6% that could lead to saponification. During the transesterification reaction, NaOH and analytical-grade methanol were used as seen in Fig. 1.

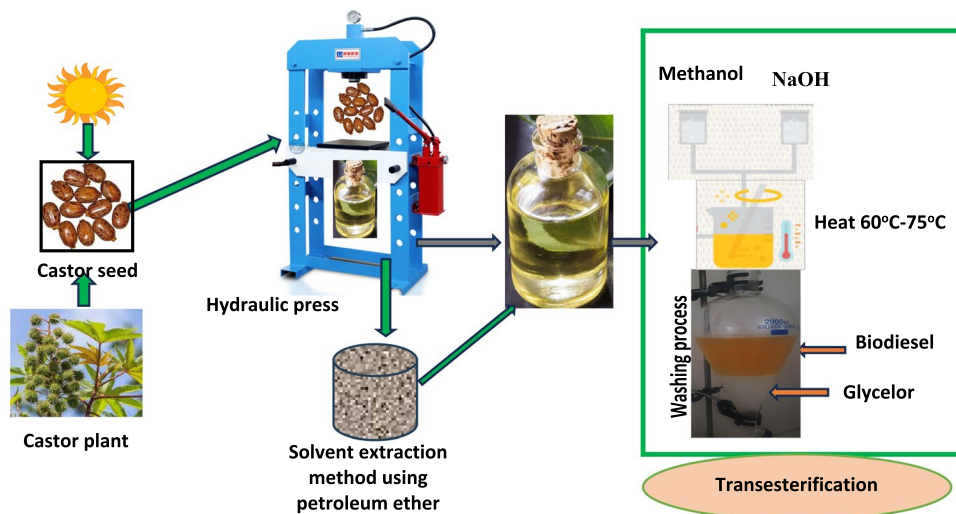


Figure 1. Procedures for Extraction of oil and Preparation of biodiesel.

The molar ratio of the alcohol to the oil was 1:5 and 0.8% volume of sulfur acid was added while the hotplate's speed and temperature were set to 800 rpm and 65 °C respectively for 70 min. At this stage, the acid value was lowered from 4.6 to 0.8 mg-KOH/g-oil. The second stage was the transesterification process by using base catalyst sodium hydroxide and methanol that dissolved to form metha-oxilate at which the ratio was 25-g NaOH to one liter methanol. The methyl ester was washed three times to remove the soap. The removal of the moisture content of the biodiesel was done using a furnace at a temperature of 130 °C. The properties of the oil of castor after esterification were characterized as per the ASTM 6571 standard to qualified the oil samples as biodiesel.

Experimental procedure and setup

After oil samples are qualified as biodiesel based on the ASTM 6571 standard the inclusion of CeO_2 in biodiesel–diesel blend were done. The size of the nano additive CeO_2 for the biodiesel–diesel mix was 25 nm, which was purchased from commercially available in Sigma Aldrich level with the density of 7.13 gm/ml with 100% purity level. During the inclusion of the nanoparticles, ultra-sonication was executed for 1 h at a frequency of 90 kHz for the proper dispersion of the nanoparticles. The prepared fuel samples were B0, B5, B10, B15, and B25 with 75 ppm CeO_2 nano additive. The reason why 75 ppm nano additive CeO_2 was used is because, a pilot test was executed by using doses of 55, 65, 75, 90 and 100 ppm. However, a slight reduction of the UHC and NO_x was seen as the dose increases and it was stable at 75 ppm. Therefore, 75 ppm dose was selected for this experimental research work.

The overall procedure done during this research work starting from castor seed collection to experimental test on engine test rig is indicated in Fig. 2.

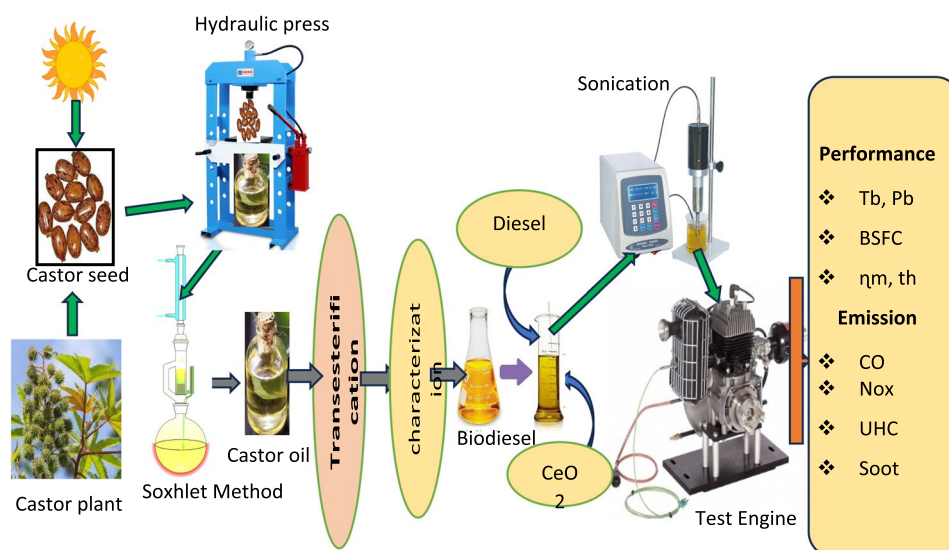


Figure 2. Over all experimental Procedures.

In this study, the fuel samples were investigated using the test setup unit, Gunt model CT110, as shown in the experimental setup in Fig. 3. The test stand consists of a CT110 engine mount, dynamometer, and CT110.22 diesel engine. The main function of the engine mount is to record and display data of experiments on the dashboard. The engine used for the performance test is a naturally aspirated mono-cylinder diesel engine. The test engine is started by the asynchronous motor equipped with the exhaust gas temperature sensor. The fuel tank, the vessel for the intake of air, and the fuel flow meter are fixed at the mobile frame. The fuel samples were tested at 80% load ranging from 1600 to 3000 rpm. The results of the experiment were displayed by the data acquisition system on a personal computer. Additionally, in each case, the exhaust gas analyzer shows the emission results like the HC, CO, and NO_x at their respective speed of measurement.

For emissions measurement, exhaust gas analyzer placed on the line of the engine exhaust gas was used to analyse the main pollutants (HC, CO₂, CO, O₂, NO_x) measured by Gunt, CT159.02 digital analyser. The detail specification of the exhaust gas analyser indicated in Table 1.

The combustion and performance characteristics have been performed on CT 110 single cylinder engine. The detail specification of the test engine explored in Table 2.

Uncertainty analysis

The highest mean percentage uncertainty (\bar{U}_{max}) predicted for engine exhaust emissions and engine combustion performance is shown by the accuracy connected with the measuring instruments, as shown in Table 3.

Result and discussion

The baseline diesel fuel and the biodiesel–diesel blended fuel properties were measured, and analyzed in this study. It revealed that all the blended castor oil biodiesel–diesel fuel satisfied the standard requirement of ASTM D6571 specifications. The result of the Physio-chemical properties of biodiesel–diesel blends are summarized in

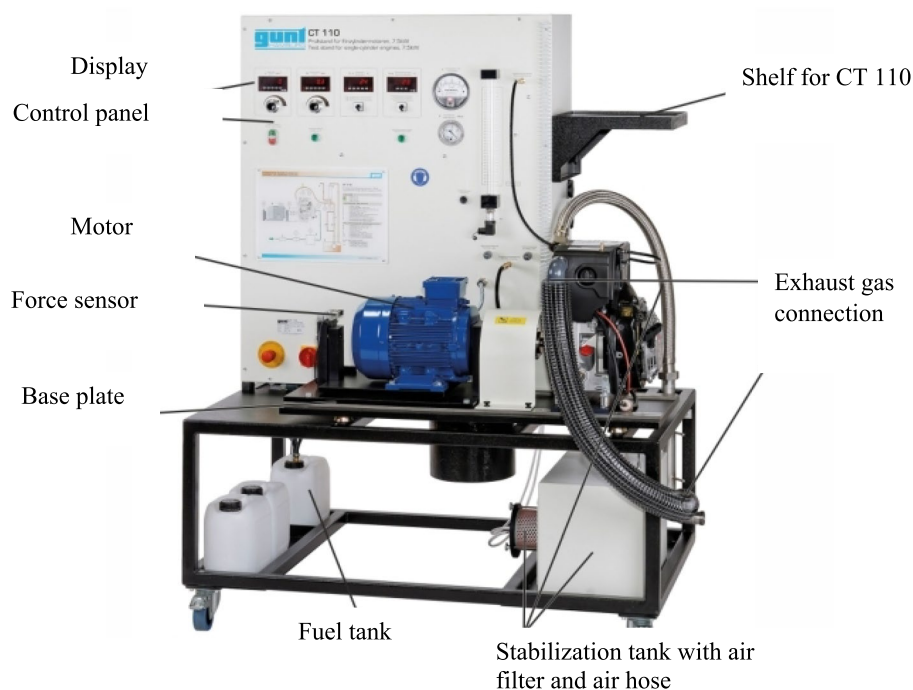


Figure 3. Experimental setup.

Parameters	Specification
Nominal/Power	0.2 KW
Type	Gunt, CT159.02
Volt	230 V
Frequency	50 Hz
Fabrication number	237,653

Table 1. Exhaust gas analyzer specification.

Engine parameters	Specification
Engine Model	EA300-E2-NB1
Type of stroke	Four-stroke diesel engine
Cooling system	Water-cooled
Cylinder arrangement	Single cylinder
Maximum power	7.5 kW@3000 min ⁻¹
Engine displacement	309 cm ³
Bore x stroke	75 mm × 70 mm
Compression ratio	23:1
Oil capacity	1,3 L
Noise level	95 dB(A)
Rotameter	30...300 L/h
Temperature sensor, exhaust gas temperature	0...1000 °C
Type of ignition	Compression ignition
Rod length	114.5 mm
Crank length	34.5 mm

Table 2. Specification of the test engine.

Measured parameters	Instrument	Measuring range	Accuracy%	\dot{U}_{\max} (%)
NO _x	Kane AUTO plus gas analyzer	0–5000 ppm	± 12 PPM	17.5
CO	CT159.02 Exhaust gas analyzer	0–10% vol	± 0.06% vol	8.7
HC		0–2500 ppm	± 3 ppm	6.2
Speed	CT 110.20	0–5000 rpm	± 12 rpm	0.51
Brake Power	CT 110.20	0–7.5 kW	± 0.1	2.72
Brake Torque	CT 110.20	– 50–50 Nm	± 0.2	1.96
TFC	CT 110.20	50 cm ³ /min	± 0.05	3.04

Table 3. Accuracy and uncertainties.

Table 4. The result of the physio-chemical properties of the oil samples was within the limit of the ASTM standard requirement of fuel for diesel engine propulsion. The flash point of biodiesels was 79.1 °C, 76.7 °C, 75.5 °C and 73.4 °C respectively for B25, B15, B10, and B5, which is higher than that of pure petro diesel of 72.3 °C. Therefore, biodiesel is safer to fire hazard during storage and custody transfer of fuel. The cloud point, of biodiesel was less than 0 °C, which is higher than pure diesel fuel with a cloud point of 0 °C. Hence, the biodiesel produced from castor has to be used in a hot climate so additives should be added to lowers the freezing point of the fuel. The biodiesel produced from castor was safer for storage and handling because biodiesel is denser than petro diesel, as indicated on Table 4. The boiling point of the biodiesel has a higher initial boiling point that affects starting

NO	Physio-chemical properties	ASTM	Limit	Test result of blends				
			6751-07b	B25	B15	B10	B5	B0
1	Density@15 °C , g/ml	D1298	Report	0.875	0.862	0.857	0.8525	0.85
2	Density@20 °C , g/l	D1298	Report	0.861	0.856	0.852	0.85	0.84
3	Flashpoint (°C)	D93	Max. 100	79.1	76.7	75.5	73.4	72.3
5	Cloud point, °C	D2500	Report	0	– 1	– 1	– 1	0
6	Pour point, °C	D97	Report	< – 8	< – 8	< – 8	< – 8	< – 8
7	Kinematic viscosity	D445	1.9–6	3.828	3.5116	3.2865	3.2013	3.1637
8	Cetain Index	D976	Min. 47	51.34	51.127	47.56	50.46	52.905
9	ASTM color	D1500	Max. 3	1 < x < 1.6	1 < x < 1.6	1 < x < 1.6	1 < x < 1.6	1
10	Water & segment, %V	D2709	Max. 0.03	< 0.03	< 0.03	< 0.03	< 0.03	< 0.03
11	Acidity, mg KOH/g	D974	0.5	0.105	0.048	0.0308	0.02421	0.0112
12	Ash content, mass%	D482	Max. 0.01	0.0009	0.0005	0.0004	0.0003	0.0002
13	Calorific value, Cal/g	–	Report	10,510	10,599	10,678	10,790	11,200

Table 4. Physio-chemical properties of diesel and biodiesel blends.

of engines at lower temperature and which causes higher fuel consumption during starting. Moreover, at lower engine speeds the unburned hydrocarbon emission due to this property.

Engine performance

Engine performance tests were conducted using the blended fuels B0, B5, B10, B15 and B25 with 75 ppm CeO₂ nano additive and without nano additive for comparison. All the engine tests were conducted from the speed range of 1600 rpm up to 3000 rpm at 80% load.

Brake power Engine's brake power was evaluated with diesel and biodiesel–diesel blends with and without the inclusion of CeO₂. The brake power showed a linear and insignificant increment as the ratio of the biodiesel in the blends increased. From the Fig. 4a and b, the brake power reduced slightly from the baseline fuel performance except for B25 because of the biodiesel blends have lower calorific value and higher viscosity as seen on Table 4. Similarly, other researchers showed the same outcome^{34–36}.

The result of the brake power output of the test engine with the inclusion of CeO₂ showed, an average increment of 0.15 kW, 0.12 kW, 0.18 kW, 0.19 kW, and, 0.09 kW for B0, B5, B10, B15, and B25 respectively. Moreover, the maximum power output was at rated speed of 2700 rpm for both cases. As shown on the plot in Fig. 4a and b, the inclusion of CeO₂ nanoparticles have shown a smooth power output in a wide speed operating range decreased at maximum speed.

Brake torque The torque output of this study for the blends with and without CeO₂ nanoparticles has shown similar patterns. However, the inclusion of CeO₂ additives on the diesel–biodiesel blends indicated a significant increment of engine torque for the blend B25 especially at the engine speed of 1700-rpm.

The brake torque output of the test engine with the inclusion of CeO₂ showed, average increment of 1Nm, 0.6Nm, 2.4Nm, 2.5 Nm, and 1.3Nm for B0, B5, B10, B15, and B25 respectively. Moreover, the maximum torque output was recorded at lower engine speed. As shown on the Fig. 5a and b, the inclusion of CeO₂ nanoparticles has shown a smooth torque output in a wide speed decreased as engine speed increased. Recent studies also reported similar results^{23,30,31,37}.

Brake-specific fuel consumption Fig. 6a and b shows, the effect of BSFC as a function of engine speed and biodiesel–diesel blends with and without CeO₂ nano-additives respectively. The result of the study showed that

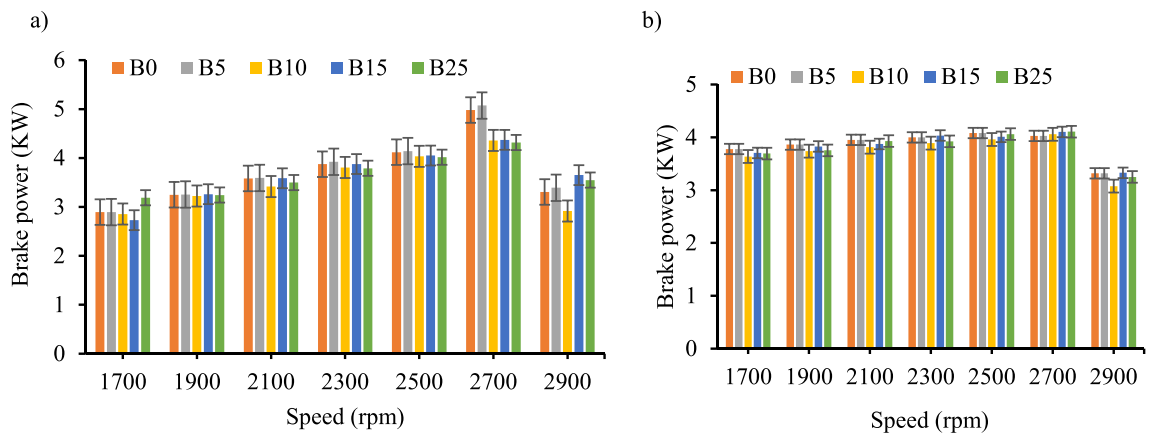


Figure 4. Brake power versus engine speed for all blend ratios. (a) Brake power with out CeO₂ Nano particle, (b) Brake power with CeO₂ Nano particle.

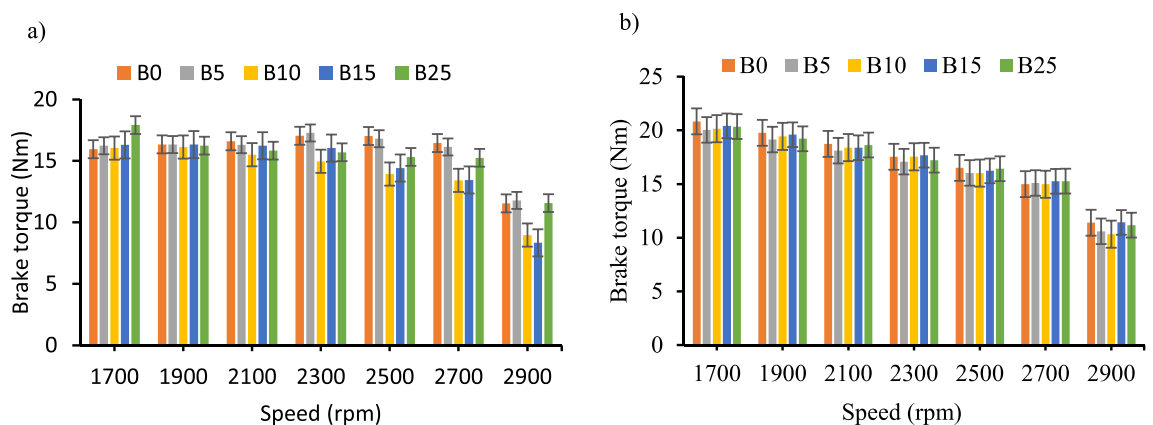


Figure 5. Brake torque versus engine speed for all blend ratios. (a) Brake torque with out CeO₂ Nano particle, (b) Brake torque with CeO₂ Nano particle.

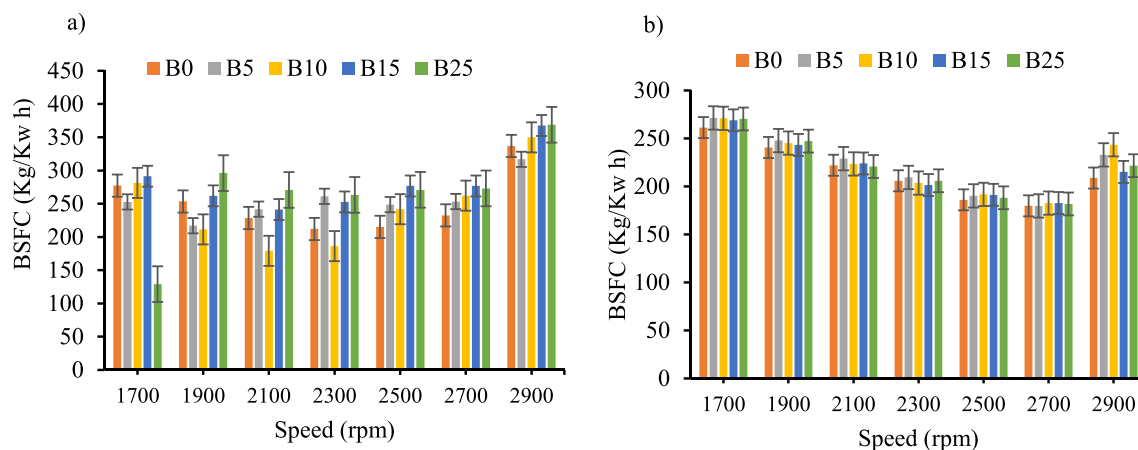


Figure 6. BSFC versus engine speed for all blend ratios. (a) BSFC with out CeO₂ Nano particle, (b) BSFC with CeO₂ Nano particle.

the BSFC for all the blends with and without CeO₂ were minimum at the intermediate engine speed which is the economic speed range of the test engine. However, in this speed range, the BSFC of the biodiesel–diesel blends with CeO₂ inclusion have shown a reduction of 16.71%, 16.32%, 12.01%, 23.14%, and 26.02%, for B0, B5, B10, B15, and B25 respectively. From the result B25 have the maximum reduction rate in BSFC and B10 have the minimum reduction rate in BSFC. Previous study has shown the higher percentage of biodiesel have higher reduction rate of BSFC when CeO₂ nano additives are mixed with biodiesel^{38,39}. Moreover, the fuel consumption reduced as the biodiesel ratio increased in the blends as shown in Fig. 6a and this is similar to a previous study conducted by^{40,41}.

Brake thermal efficiency Across the engine operating speed range, B15 and B25 had higher engine thermal efficiency as shown in Fig. 7a except at engine speed of 2700 rpm. According to a prior study, using castor biodiesel boosts brake thermal efficiency when compared to diesel fuel⁴⁰. As seen in prior research, the thermal efficiency increased as the fraction of biodiesel in the blends increased^{41–44}. The brake thermal efficiency with the inclusion of CeO₂ nanoparticles showed the maximum increment specifically at lower engine speed as shown in Fig. 7a and b. The average maximum increment of thermal efficiency was 22.2% for B10 with CeO₂ inclusion. The performance of internal combustion engines has been demonstrated to be significantly impacted by cerium oxide³². These additives work as a catalyst, bringing oxygen to the fuel mixture to speed up combustion and increase engine efficiency overall.

Mechanical efficiency As indicated on the Fig. 8a and b the mechanical efficiency decreased as the engine speed increased for both with and without CeO₂ nanoparticles. However, the maximum increment of mechanical efficiency of the biodiesel–diesel blends with CeO₂ inclusion was 3.2% and 3.6%, for B15 and B25 respectively. The decrement of mechanical efficiency with the engine speed were in line with earlier investigations^{23,41,45}.

Emission analysis

Carbon monoxide emission Carbon monoxide (CO) emission was generally lower than diesel fuel as shown in Fig. 9a in case where nano additive is not used from the rated idle speed to the rated maximum speed. Addition of CeO₂ nano additive to biodiesel–diesel blends increase the CO emission as engine speed increased as shown on Fig. 9b. When CeO₂ nanoparticles were added, the maximum average percentage reduction of CO emission

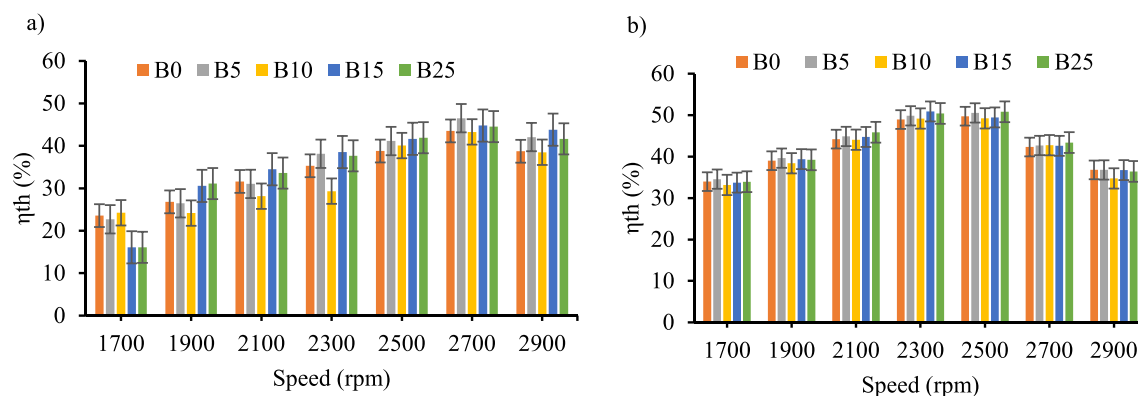


Figure 7. Thermal efficiency versus engine speed for all blend ratios. (a) η_{th} with out CeO₂ Nano particle, (b) η_{th} with CeO₂ Nano particle.

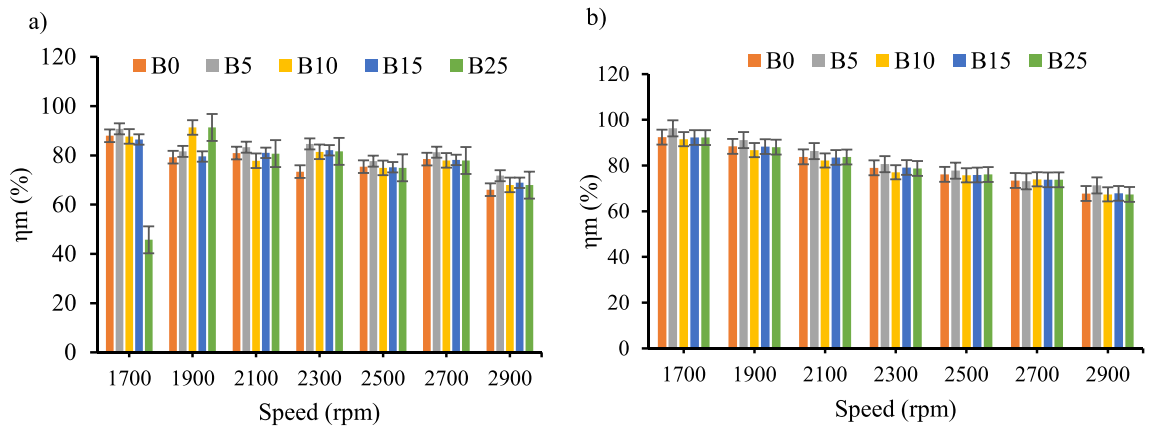


Figure 8. Mechanical efficiency versus engine speed for all blend ratios. (a) η_m with out CeO_2 Nano particle, (b) η_m with CeO_2 Nano particle.

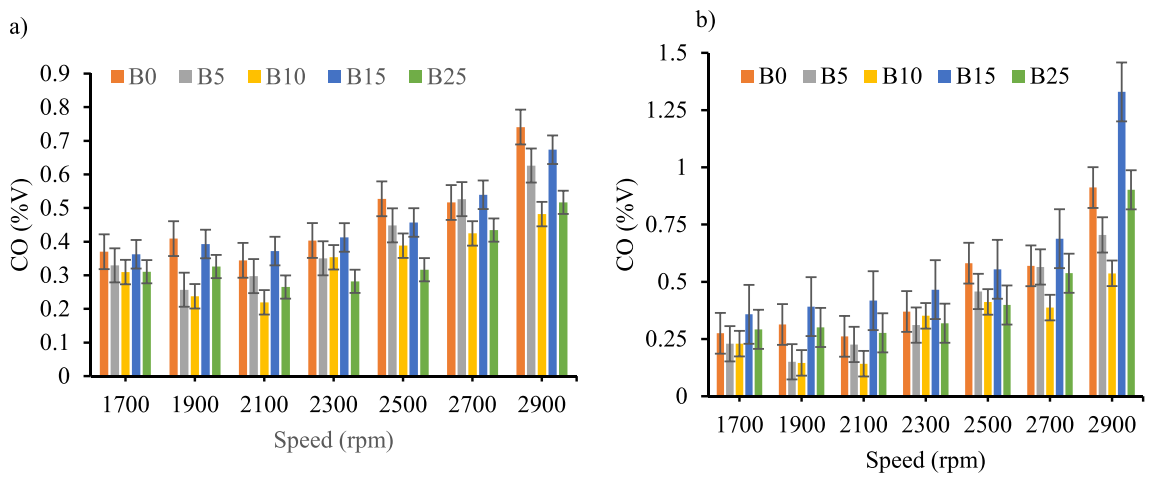


Figure 9. Carbon monoxide emission versus engine speed for all blend ratios. (a) CO Emission with out CeO_2 Nano particle, (b) CO Emission with CeO_2 Nano particle.

was 12% and 10.2% for B5 and B10 respectively. Whereas for the blends of B0, B15, and B25, CO emission was increased by 1.5%, 30% and 27% respectively. The increment of the CO emission with engine speed were in line with earlier investigations^{41,46–48}.

Unburned hydrocarbon emission The relationship between engine speed and hydrocarbon (HC) emissions is shown in Fig. 10a and b for blends with and without CeO_2 nano-additives. Except for B10 at the highest engine speed, the emission of HC reduced as the proportion of biodiesel increased shown in Fig. 10a. Additionally, HC emission was reduced for all blend, with and without CeO_2 nano additions as speed increased. Due to the

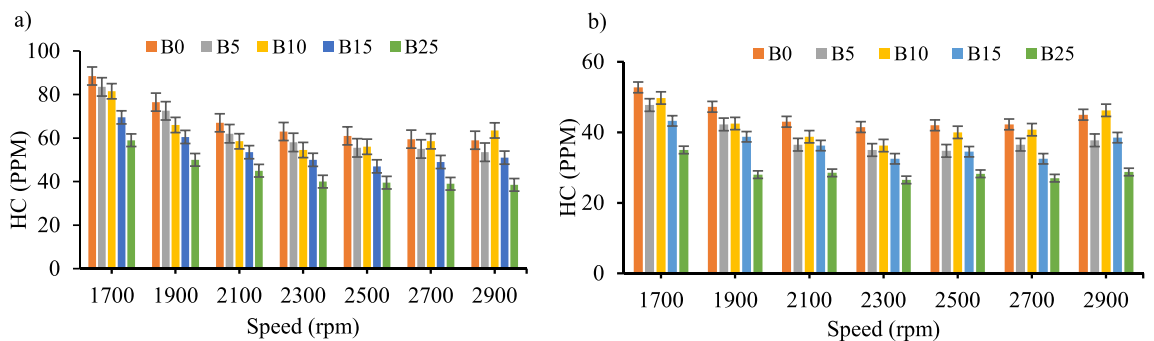


Figure 10. Unburned hydrocarbons emission versus engine speed for all blend ratios. (a) HC Emission with out CeO_2 Nano particle, (b) HC Emission with CeO_2 Nano particle.

higher cetane number, higher oxygen content biodiesel by itself, and inclusion of CeO_2 in the biodiesel–diesel blends, the formation of HC emission in the engine cylinder is minimized^{19,12,49,50}. The incorporation of CeO_2 nanoparticles showed an average percentage reduction in HC emission was 32.3, 37.7, 32.6, 33 and 32.8% for B0, B5, B10, B15, and B25, respectively. The percentage of reduction of HC emission when nano-additives used were also the same with the earlier research works^{40,41,51}.

Nitrogen oxide emission Fig. 11a and b depict the emissions of nitrogen oxide emission (NO_x) to speed for biodiesel–diesel blends without and with the inclusion of CeO_2 nano additions, respectively. Maximum NO_x emission was seen at the rated speed of 2700 rpm without nano additive and at 2900 rpm with the CeO_2 , where maximum power and torque are obtained. The trend of NO_x emissions increased as engine speed increase. In addition, the inclusion of nano additive CeO_2 reduced NO_x emissions by 5.5% and 2.4% for B0 and B5 respectively. Whereas for the blends of B10, B15, and B25, NO_x emission was increased by 4.3%, 3.3% and 8.5% respectively. This percentage reduction of NO_x emission when nano-additives incorporated were also the reported by earlier research works (Agarwal et al., 2015)^{23,51,52}.

Soot opacity The experiments result of smoke opacity are shown in Fig. 12a and b for both biodiesel–diesel blends with and without CeO_2 respectively. Averagely the use of CeO_2 nano-additives showed less than 12% smoke opacity. Biodiesel–diesel blends have demonstrated soot opacity of less than 10% between 1900 and 2600 rpm.

The fuel sample that had the greatest and the lowest amount of smoke opacity was B0 and B25 respectively through engine speeds. However, the addition of CeO_2 nano additive to the biodiesel–diesel blends has demonstrated a significant average reduction in soot opacity of 11.56% for all biodiesel–diesel blends for the engine operating speed range. This conclusion was consistent with the study's findings^{41,45,52–54}.

Conclusion

The current study investigates the effects of CeO_2 nanoparticles on four fuel mixes running in a single-cylinder DI diesel engine at dose levels of 75 ppm for investigation of performance and emission. This study has shown a rise in brake thermal efficiency with the inclusion of CeO_2 nanoparticles. Using CeO_2 nano-additives decreased the output of CO emissions for all biodiesel–diesel blends at all engine speeds. Due to the higher Cetane number and oxygen content of the biodiesel and the nano additions, the emission of HC in the engine cylinder was decreased

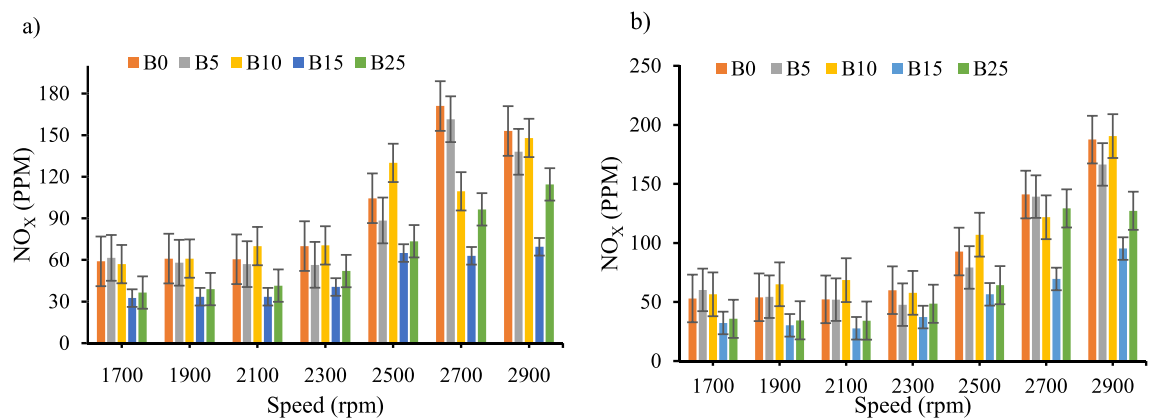


Figure 11. Nitrogen oxide emission versus engine speed for all blend ratios. (a) NO_x Emission with out CeO_2 Nano particle, (b) NO_x Emission with CeO_2 Nano particle.

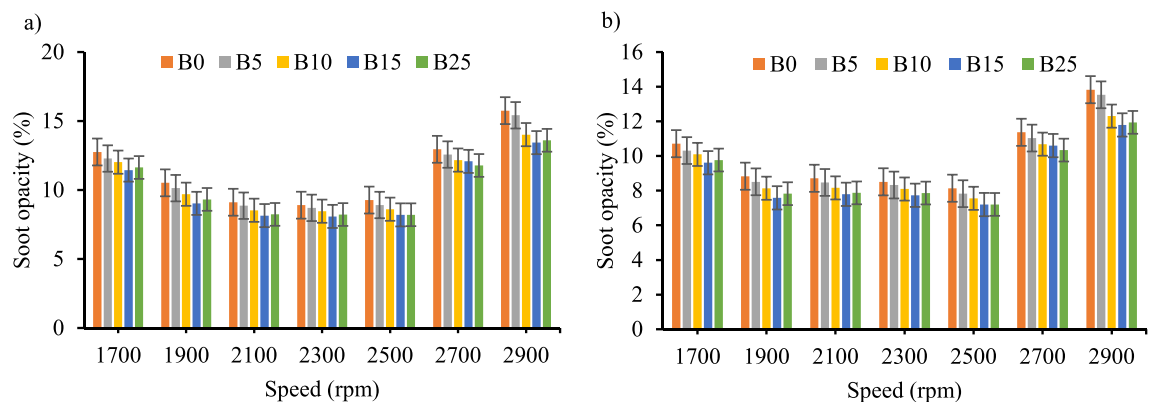


Figure 12. Soot opacity (%) versus engine speed for all blend ratios. (a) Soot opacity (%) without CeO_2 Nano particle, (b) Soot opacity (%) with CeO_2 Nano particle.

as CeO₂ nanoparticles were added to the diesel blends. The addition of CeO₂ demonstrated a considerable reduction of NO_x emission and soot opacity for all biodiesel–diesel blends for the engine operating speed range. By adjusting the blend ratio and engine speed with and without CeO₂, at a fixed compression ratio and 80% load, this study investigated the performance and emission characteristics of castor biodiesel–diesel blends. According to the results, B25 has the highest BSFC reduction rate and B10 has the lowest. For B10 with CeO₂ addition, the average highest improvement in thermal efficiency was 22.2%. As engine speed increased, so did CO emissions. As speed increased HC emission decreased for all blends, both with and without CeO₂ nano additions. Maximum NO_x emission was observed at 2900 rpm with nano additive and at the rated speed of 2700 rpm without it. Throughout the engine operating speed range, the CeO₂ nano addition decreased the soot opacity by 11.56% for all biodiesel–diesel mixes. In general, CeO₂ improves the properties of mixes of biodiesel. Additionally, it enhances the diesel engine's biodiesel blend's combustion efficiency and reduces pollutants. It is necessary to design new, modified injection strategies with several injection events to mitigate the increase in NO_x emissions. Consequently, we suggest that further research be done to investigate the performance, combustion, and emission characteristics of diesel engines by varying the injection timing, compression ratio, and injection rate.

Data availability

Upon reasonable request, the corresponding author will provide the data supporting the study conclusions.

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Author contributions

S.T.: Performed the experiments, analyzed data, wrote the paper. V.R.A., R.G., R.B.N.: Supervision, Writing paper and editing. Y.S. edit, wrote and data analyzed. All authors reviewed the manuscript.

Competing interests

The authors declare no competing interests.

Additional information

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