# SCIENTIFIC REPORTS

### OPEN

Received: 6 March 2018 Accepted: 2 August 2018 Published online: 22 August 2018

## High-altitude well log evaluation of a permafrost gas hydrate reservoir in the Muli area of Qinghai, China

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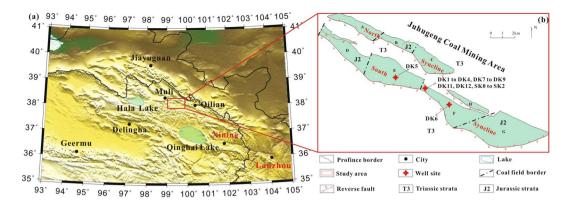
The Muli area is the only permafrost region on the Chinese mainland wherein gas hydrates have been discovered. The gas hydrates are present in the fractures and pore spaces of the host rocks with a lamellar or micro-disseminated structure. By combining conventional and image logs, we describe the thickness of the permafrost layer and the well log responses of the gas hydrate reservoir, and calculate the porosity and gas hydrate saturation. We then analyze the advantages and disadvantages of different logging methods for evaluating gas hydrate reservoirs. Our results indicate that (1) gas hydrates are present below the permafrost in the Muli area, (2) gas hydrates predominantly occur in rock fractures, (3) the apparent resistivity is sensitive to gas hydrates present in pore spaces, and both apparent resistivity and acoustic logs are sensitive to gas hydrate saturation can be effectively calculated by the Archie equation, the modified Archie equation, and the Indonesian equation.

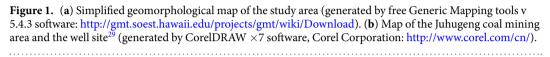
Gas hydrates are cage-structured compounds consisting of water and natural gas. They are mainly found in terrestrial permafrost regions and in marine sediments along the outer margins of continents, and they are a potential source of unconventional energy<sup>1</sup>. Permafrost-associated gas hydrates are primarily distributed in the high-latitude permafrost regions of the Arctic. These include the Prudhoe Bay-Kuparuk area on the North Slope of Alaska, USA, the Mackenzie Delta and Sverdrup Basin of Canada, the West-Siberian Basin, Lena-Tun-guska area, Timan-Pechora Basin, NE Siberia, and Kamchatka areas of Russia, the Svalbard Peninsula in Norway, and areas of Greenland<sup>2-4</sup>. At approximately  $2.15 \times 10^6$  km<sup>2</sup>, China has the third largest permafrost area in the world. Previous studies of permafrost regions in China have indicated that the Qiangtang Basin, Qilian montane area, Fenghuo-Wuli area, and the Mohe Basin may have experienced suitable conditions for gas hydrates to form. The gas hydrate resources in this region<sup>4</sup> has been approximated to be  $3.8 \times 10^{12}$  m<sup>3</sup>. From 2008 to 2017, the China Geological Survey conducted a scientific drilling project to evaluate the presence of gas hydrates in the south of the Qilian Mountains in Qinghai, which included obtaining gas hydrate samples from boreholes. Meanwhile, several geological, geophysical, and geochemical surveys and laboratory tests have characterized the reservoir and confirmed several indicators of gas hydrates<sup>5,6</sup>. The geophysical surveys conducted in this area consisted of 2D seismic reflections, audio Magnetotellurics, and well logging<sup>7</sup>. This study focuses on the data from well logs, which were collected using a Micro-Logger II system (Robertson Geologging Ltd., UK). Well logging included the production of electrode resistivity logs, spontaneous potential logs, natural gamma rays, acoustic wave velocities, borehole temperatures, ultra-sonic image logs, and so on.

Gas hydrates form under particular temperature and pressure conditions, and they may decompose when the environment changes. Therefore, it is very difficult to obtain undisturbed samples of gas hydrates. Well logging may provide the *in situ* information of the downhole formation, and therefore the most adequate data on gas hydrate-bearing reservoirs. Most investigations of gas hydrate reservoirs use well logging methods<sup>2,8–15</sup>. In permafrost areas and marine sediments, the well log responses of gas hydrate reservoirs are characterized by high resistivity, high P-wave velocity, high neutron porosity, and low density<sup>16–20</sup>. The purpose of well logging evaluations is to transform well logging data into reservoir parameters, such as porosity and gas hydrate saturation, which are critical for the evaluation and production of gas hydrate resources.

Here, we first introduce a method of determining permafrost thickness using temperature logs. We then extract the log responses of the gas hydrate reservoir, and select tested models for computing the porosity and gas

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hydrate saturation of the reservoir<sup>10,11,21-28</sup>. Finally, we develop a set of well logging methods that can be used to evaluate high-altitude permafrost gas hydrate reservoirs.

#### **Geological Setting**

The study area was located on the southern margin of the Qilian Mountain, at an elevation of 4100–4300 m and an annual mean surface temperature of 5.1 °C. The drill sites were located within the Juhugeng coal mining area of the Muli depression in the central Qilian Basin (Fig. 1). Previous geological studies have shown that the central part of the Juhugeng coal mining area is an anticline composed of Triassic strata, and the south and north flanks are two synclines composed of coal-bearing Jurassic strata<sup>29,30</sup> (Fig. 1). At present, there are three coal fields located on the northern syncline and four coal fields on the southern syncline.

The formations discovered in the coal field belong to the Muli and Jiangcang groups. The lower member of the Muli Group was formed in a floodplain with a braided river, and is composed of a sequence of coarse siliciclastic rocks and basal conglomerate<sup>29,30</sup>. The upper member of the Muli Group was formed in lacustrine and marsh environments, and contains several mineable coal seams. The lower member of the Jiangcang Group was formed in deltaic and lacustrine environments, and contains two to six coal layers. The upper member of the Jiangcang Group was formed in a shallow to semi-deep lake environment, and consists of shales and siltstones. Thus, the study area encompasses several paleoenvironments that likely serve as rich sources of gas, coal-bed methane, hydrocarbon source rocks, and oil shales that could further provide abundant sources for the formation of gas hydrates<sup>6</sup>.

#### **Results and Discussion**

**Permafrost thickness.** Permafrost thickness is a key factor in the accumulation of gas hydrates, and it can determine whether the gas hydrate exists within the permafrost or below it. We can then use permafrost thickness to decide upon the appropriate reservoir model: (1) gas hydrate and ice or (2) gas hydrate and water. The minimum and maximum permafrost thicknesses in the Muli area were approximately 70 m and 120 m (Fig. 2), respectively. Gas hydrates occurred at depths of 130–400 m and were distributed discontinuously across this range<sup>30</sup>.

Temperature logs indicated that there were two dominant patterns of temperature with depth (Fig. 2). One such pattern was the "C" curve, in which temperatures were higher at the shallowest depths, then decreased, and finally increased to their highest values with increasing depth (e.g., DK12). The other pattern observed was the "L" curve, in which temperatures were steady in the top section and then increased in the lower section (e.g., DK11 and SK2). Regardless of the pattern observed, all temperature logs could be used to determine the thickness of the permafrost region.

Drilling engineers must circulate mud to protect the coal mining area from collapse; however, temperature well logging requires this circulation to be halted for a long period of time so that there is no heat exchange between the mud and the rock units. In this study, temperature logs were generated 24–48 h after mud circulation had ceased; however, most wells exhibited a temperature above 0 °C. Thus, we suggest that when temperature logs cannot collect data at 0 °C, the resulting curve will display a "C" or "L" pattern. The intersection between the deep gradient lines of the host rock and the permafrost region can be considered as the bottom of the permafrost<sup>2</sup>.

**Well log responses of the gas hydrate reservoir.** The Muli area satisfies the requirements for the generation of gas hydrates based upon the gas source and permafrost conditions<sup>4–6</sup>. The general pattern of gas hydrate accumulation is as follows: natural gas from the pyrolysis of petroliferous gas migrates up-section along faults, accumulating in shallow rock units due to the sealing of mudstone and oil shales, and forms gas hydrates when it combines with water in permafrost regions<sup>31</sup>. Moreover, gas hydrates occur in cracks in rocks with lamellar structures or in the pore spaces of rocks with micro-disseminated structures. The lithology of the gas hydrate reservoir in this study is predominantly mudstone, oil shale, siltstone, and fine sandstone. The occurrence of gas hydrates varied with lithology and structure, so it is reasonable to analyze the log responses of the reservoir according to its lithology.

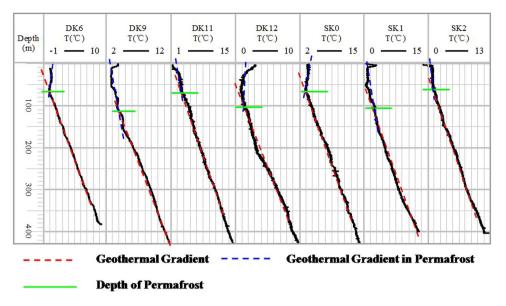


Figure 2. Temperature logs from seven boreholes (DK6, DK9, DK11–12, and SK0–2) in the Muli area.

Reservoir type	Lithology	Resistivity	P-wave velocity	Density
Pore type	Sandstone	Increase	Small anomaly	No anomaly
Fracture type	Mudstone	Increase	No anomaly	Decrease
Flacture type	Shale	Increase	Significant increase	No anomaly

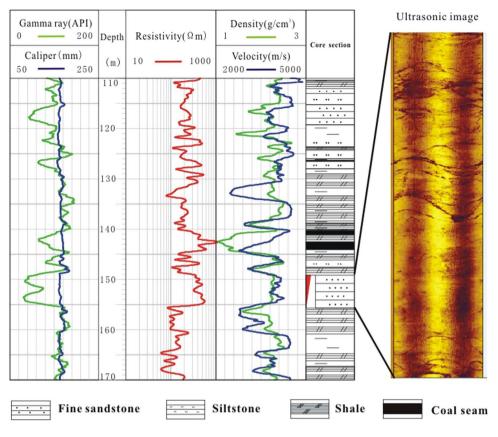
 Table 1. Well logging responses of the gas hydrate reservoirs in the Muli area.

	Medium sandstone Fine		Fine san	Fine sandstone S		Siltstone		Mudstone		Shale	
Borehole ID	Layers	Thickness (m)	Layers	Thickness (m)	Layers	Thickness (m)	Layers	Thickness (m)	Layers	Thickness (m)	Total thickness (m)
DK1	/	1	1	3.4	5	10.6	1	1	1	1	14.0
DK2	2	4.6	2	2.8	1	1	1	2.7	7	61.2	71.3
DK3	1	1.8	1	1	1	1	6	17.9	4	9.2	28.9
DK6	/	1	1	4.5	1	1	1	2.5	1	1	7.0
DK8	1	2.6	1	2.9	4	16.8	5	8.6	6	19.3	50.2
DK9	2	6.9	1	2.0	3	15.6	1	6.8	3	9.0	40.3
DK12	/	1	1	1	1	1	1	2.8	1	1	2.8
SK0	1	1.5	1	1	1	1	1	5.2	1	1	6.7
SK1	1	1	1	1	1	1	1	/	2	6.7	6.7
SK2	1	4.3	1	1	3	8.8	1	/	1	1	13.1
Total	8	21.7	6	15.6	15	51.8	16	46.5	22	105.4	241

Table 2. Distribution of the gas hydrate reservoir identified by well logging.

Table 1 summarizes the well log responses of the gas hydrate reservoir in the Muli area. Geological and mud logging indicated the presence of 67 layers of known or suspected gas hydrate reservoir within the 10 study wells. The accumulated thickness of the reservoir was 241 m (Table 2). The accumulated thickness of the gas hydrate-bearing sandstone, mudstone, and shale reservoirs were 89.1 m, 46.5 m, and 105.4 m, respectively. Thus, gas hydrates in the study area occur predominantly in fractures within mudstone and shale as both lithologies are characterized by low porosity. We evaluated the well log responses of each lithology by computing the resistivity, velocity, and density anomalies for each of the 67 gas hydrate-bearing layers and comparing them to layers without gas hydrates.

Pore-type gas hydrate reservoir (sandstone). The pore-space in the sandstone provides storage for gas hydrates. Well DK8 (fine sandstone) penetrated a gas hydrate reservoir from 150–155 m and exhibited a 200  $\Omega$ m increase in resistivity, a 150 m/s increase in velocity, a 0.05 g/cm<sup>3</sup> decrease in density, and a 5 mm increase in borehole diameter compared to the non-gas hydrate-bearing layers from 116–119 m (Fig. 3). The ultrasonic image of this section is bright and displays few dark cracks, indicating that the sandstone of is relatively intact with few fractures.



**Figure 3.** Well logs of sandstone (borehole DK8) with and without gas hydrate (red triangle indicates the gas hydrate layer).

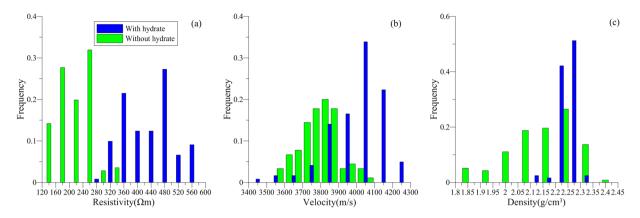
Twenty-nine gas hydrate-bearing sandstone formations were identified in the boreholes of the study area. Gas hydrate-bearing sandstones had resistivities of  $370-490 \Omega m$ , P-wave velocities of 3800-4100 m/s, and densities of  $2.2-2.3 \text{ g/cm}^3$  (Fig. 4). The formation of gas hydrates also generates a 'salt discharge' effect that can lead to a decrease in local conductivity. Thus, the apparent resistivity of the gas hydrate-bearing sandstone was twice that of a sandstone saturated with water. However, the apparent resistivity of the gas hydrate reservoir marine and polar permafrost areas are as much as 50 times that of a sandstone saturated with water<sup>32</sup>. This may be attributed to the low concentration of gas hydrates in the Muli sandstones.

In marine sediments, the velocities of gas hydrate reservoirs are important because they predominantly occur in uncemented rock units, and the generation of gas hydrates can change the physical properties of the reservoir and further alter rock velocities and densities. However, in the Muli area, gas hydrates occur in the sandstone that has already undergone diagenesis, so the generation of gas hydrates should not substantively alter the physical properties of the rock. This explains the lack of velocity and density anomalies in our results (Fig. 4).

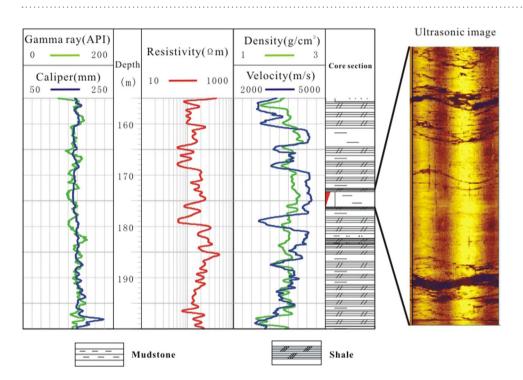
*Fracture-type gas hydrate reservoir (mudstone and shale).* A mudstone gas hydrate reservoir was observed in well DK8 at a depth of 173–175 m. The ultrasonic image logs of this section indicated that the rock was less broken with some developed fractures. Two wide fractures were observed that provided storage for gas hydrates. Compared to the mudstone reservoir without gas hydrates from 161–164 m, the gas hydrate-bearing mudstone exhibited a 100  $\Omega$ m increase in resistivity, a 50 m/s increase in velocity, a 0.2 g/cm<sup>3</sup> decrease in density, and a 2 mm increase in borehole diameter (Fig. 5).

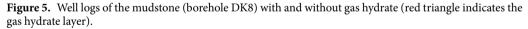
We identified 16 gas hydrate-bearing mudstone layers in the boreholes of study area. The gas hydrate-bearing mudstones had resistivities of  $150-250 \Omega m$ , P-wave velocities of 4400-4600 m/s, and densities of  $2.36-2.44 g/cm^3$  (Fig. 6). Compared to the mudstone without gas hydrate, the resistivity of the gas hydrate-bearing mudstone was 2–3 times higher, the density was slightly lower, and the P-wave velocity showed no prominent variation. This indicates that the formation of gas hydrates in mudstone fractures affected some of the physical properties of the host rock.

Two gas hydrate-bearing shale layers were found in well DK9 between 190 and 209.5 m depth, which also contained oil shale, mudstone, and fine sandstone. According to the ultrasonic logging images, cracks were well-developed in the shale formation, providing storage for gas hydrates (Fig. 7). Compared to shales without gas hydrates, the upper gas hydrate-bearing shale exhibited a 120  $\Omega$ m increase in resistivity, a 1800 m/s increase in velocity, a 0.2 g/cm<sup>3</sup> decrease in density, and a 14 mm increase in borehole diameter. The lower gas hydrate-bearing shale revealed a 40  $\Omega$ m increase in resistivity, a 1500 m/s increase in velocity, a 0.01 g/cm<sup>3</sup> decrease in borehole diameter.



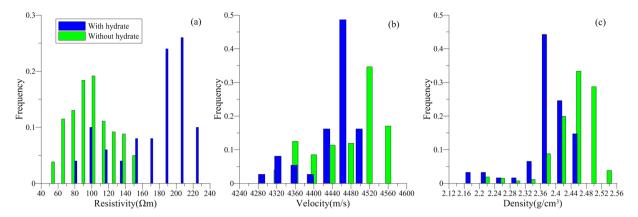
**Figure 4.** (a) Resistivity ( $\Omega$ m), (b) velocity (m/s), and (c) density (g/m<sup>3</sup>) responses of sandstone reservoirs with (blue bars) and without (green bars) gas hydrate in the study area.



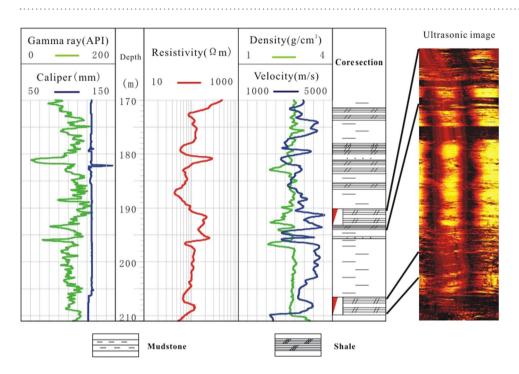


We identified 22 gas hydrate-bearing shale layers in the boreholes of study area. The gas hydrate-bearing shales had resistivities of  $75-210 \Omega m$ , P-wave velocities of 3600-4600 m/s, and densities of  $2.4-2.6 g/cm^3$  (Fig. 8). Compared to shales without gas hydrates, the resistivity of the gas hydrate-bearing shale was much higher, as much as five times higher, the P-wave velocity was 1.5 times higher, and the density exhibited no obvious anomalies. The increase in P-wave velocities indicates that the formation of gas hydrates could enhance the consolidation effect of the rock. By integrating the well logging characteristics of the gas hydrate-bearing mudstone and shale, we conclude that fracture-type gas hydrate-bearing reservoirs exhibit clear resistivity anomalies. The greater the P-wave velocity anomaly, the more fractures and crushed zones exist in the gas hydrate-bearing rock unit.

*Gas hydrate-bearing reservoir comparisons.* Similar to well logs from another permafrost region, represented by the Northwest Eileen State-2 well, and the marine well from the Deep Sea Drilling Project (DSDP), Leg 84, Site 570 (Table 3), the resistivity logs increased in the gas hydrate-bearing units in the Muli area. However, unlike these other regions, the acoustic and density logs of pore-type gas hydrate-bearing reservoirs in the study area showed no anomalies. Conversely, the acoustic and density logs of fracture-type gas hydrate-bearing reservoirs show similar anomalies to these other regions. The caliper log was slightly increased in the Muli area; however, the anomalies were weaker due to the lithology and low volume of gas hydrates.



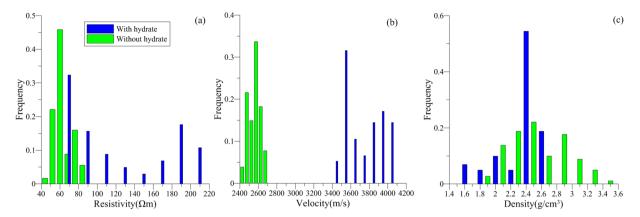
**Figure 6.** (a) Resistivity  $(\Omega m)$ , (b) velocity (m/s), and (c) density  $(g/m^3)$  responses of mudstone reservoirs with (blue bars) and without (green bars) gas hydrate in the study area.



**Figure 7.** Well logs of the shale (borehole DK9) with and without gas hydrate (red triangle indicates the gas hydrate layer).

**Well log evaluation.** *Porosity.* The porosity of the Muli Group as calculated by core testing was 5–10%. Core test porosities yield the pore space occupied by water, including free water, interlayered water, and irreducible water. Most porosity well logs measure a parameter that reflects the water content of the unit, so the core test porosity and the porosity computed from well logs should be consistent. In this study, core porosity was measured by a gas expansion method. That the porosity calculated by the density log ( $\phi_{\text{DEN}}$ ) is closer to the core test porosity than the porosity calculated by the acoustic log ( $\phi_{AC}$ ) is shown in Table 4. Excluding the effect of borehole diameter, one possible reason for this pattern is that the acoustic log was affected by methane dissolved in the mud because gas hydrates can decompose into methane when the temperature and pressure conditions are altered by drilling. Thus, the density log should be used to compute the porosity of rocks when the gas hydrate content is high as it appears to be more robust to the environmental degradation of gas hydrates. Both density and porosity varied greatly among the boreholes and lithologies. Figure 9a indicates that the porosity calculated by the density log is ~20% and pore connectivity should be studied in the future.

*Gas hydrate saturation.* The gas hydrate saturation calculated by the empirical equation based on the resistivity log performed better than that based on the acoustic log; thus, resistivity logs are more suitable for the evaluation of gas hydrate saturation in the Muli area. Using resistivity logs, we adopted the Archie equation, the modified Archie equation, and the Indonesian equation to compute gas hydrate saturation.



**Figure 8.** (a) Resistivity ( $\Omega$ m), (b) velocity (m/s), and (c) density (g/m<sup>3</sup>) responses of shale reservoirs with (blue bars) and without (green bars) gas hydrate in the study area.

Log data	Northwest Eileen State-2 well	DSDP Leg 84 Site 570 well		
Acoustic transit-time log	Decrease	Responded to gas hydrates		
Density	Decrease	Responded to gas hydrates		
Dual induction log	Increase	Responded to gas hydrates		
Caliper log	Increase	Responded to gas hydrates		

**Table 3.** Gas hydrate well log responses from a permafrost region (Northwest Eileen State-2 well) and the sea floor<sup>2</sup> (DSDP Leg 84 Site 570 well).

Borehole ID	Depth (m)	Lithology	Core test porosity (%)	ф <sub>DEN</sub> (%)	ф <sub>АС</sub> (%)
	108.50	medium sandstone	7.07	5.8	4.5
	110.50	medium sandstone	4.99	9.2	6.5
	115.50	mudstone	6.25	8.2	0.1
DK2	387.50	coarse sandstone	5.47	8.6	1.5
DK2	394.00	oil shale	8.19	8.2	0.1
	402.00	medium sandstone	3.81	6.5	0.1
	422.50	mudstone	4.90	4.4	2.2
	435.20	medium sandstone	5.56	8.4	2.0
	69.76	siltstone	4.84	5.1	3.8
	87.00	coarse sandstone	9.40	6.2	12
DK3	108.50	fine sandstone	7.07	3.0	7.5
	110.50	coarse sandstone	4.99	4.6	9.1
	113.00	coarse sandstone	6.03	3.8	10.7
	135.50	oil shale	3.21	3.2	7.2

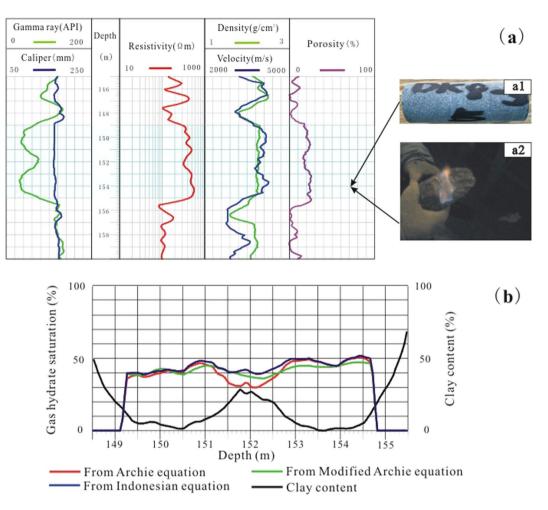
Table 4. Core test-measured porosity (%) and well log-calculated porosity (% density and % acoustic).

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Using the DK8 well as an example, core analysis at a depth of 154 m revealed a gas hydrate saturation of ~50%. Figure 9b illustrates the calculated gas hydrate saturation of the pore-type fine sandstone at a depth interval of 148–155 m, indicating that the values calculated by the Archie equation, the modified Archie equation, and the Indonesian equation were close to those derived from the core tests, and therefore suitable for evaluating gas hydrate saturation in the Muli area. Additionally, the Indonesian equation appeared to be suitable for units with low salinity waters, as exhibited in the study area, where resistivity of the formation water  $R_w = 3 \Omega m$ . The modified Archie equation and the Indonesian equation can be used for units with high clay contents ( $V_{sh} \ge 10\%$ ), because the equations contain correction terms to overcome the effect of clay.

As the drilling process can change the temperature and pressure conditions of the host rock and lead to decomposition of gas hydrates, both gas hydrate and gas are present in the pores, leading to a greater gas hydrate saturation when calculated by an acoustic log. Therefore, the acoustic log must be corrected before being used to compute gas hydrate saturation. The correction equation can be obtained by laboratory experiments.

The selection of a gas hydrate saturation model depends upon the distribution of gas hydrates and clay, pore type, lithology, and structure. While it remains a complex problem, it will plan an important role in the evaluation



**Figure 9.** (a) Well logs from borehole DK8. (b) Gas hydrate saturations estimated from the four models employed.

of gas hydrate reservoirs in the future. We tested three models in the Muli area and achieved reasonable results, which can provide insights into the evaluation of gas hydrate saturation in areas with similar geologic histories.

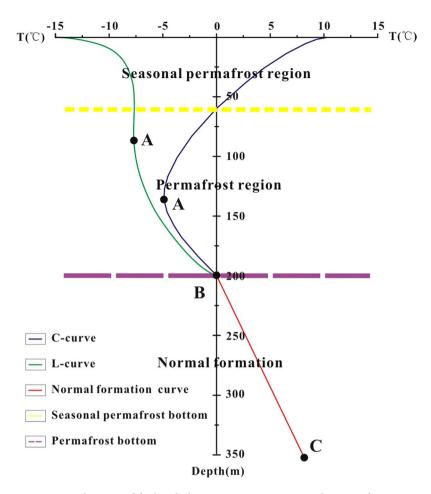
#### Conclusions

The range of the permafrost thickness in the Muli area is from 70 to 120 m. The pore-type gas hydrate reservoir can be identified by apparent resistivity logs, while the fracture-type gas hydrate reservoir can be identified by apparent resistivity and acoustic logs. The gas hydrate-bearing rocks of the study area are predominantly fracture-type reservoirs, which exhibit lower apparent resistivity values (75–250  $\Omega$ m), similar P-wave velocities (3600–4600 m/s), and higher densities (2.36–2.6 g/cm<sup>3</sup>) than the pore-type reservoirs. The pore-type gas hydrate reservoir has an apparent resistivity of 370–490  $\Omega$ m, a P-wave velocity of 3800–4100 m/s, and a density of 2.2–2.3 g/cm<sup>3</sup>. Using the density log is a particularly effective method for calculating reservoir porosity in this area. Our study indicates that the Archie equation is suitable for evaluating the gas hydrate saturation in formations with low clay contents (V<sub>sh</sub> < 10%), while the modified Archie equation and the Indonesian equation are both suitable for formations with high clay contents (V<sub>sh</sub> ≥ 10%).

#### Methods

**Determining permafrost thickness.** The thickness of the permafrost was determined using temperature logs. Within these temperature logs, obvious variations in the geothermal gradient were observed, which indicated the bottom depth of the permafrost.

We constructed a schematic model to illustrate the methods used to determine the bottom depth of the permafrost (Fig. 10). For a "C" temperature log curve, there were three components: the seasonal permafrost layer, the permafrost region, and the host rock. The thickness of the seasonal permafrost layer is affected by the seasons, wherein it is thinner in the summer and thicker in the winter. The minimum temperature appeared in the permafrost region. For a "L" temperature log curve, there was no seasonal permafrost layer. This pattern was observed in the borehole located on the lee side of a mountain at high altitude, so the surface temperature was below 0 °C even in the summer. However, the "C" temperature log curved may change to a "L" curve in the winter due to the decrease in surface temperatures.



**Figure 10.** Schematic of the borehole temperature variation in the permafrost region.

The "C" and "L" temperature log curves overlapped below the B point shown in Fig. 10, indicating that the section below the B point is not affected by the permafrost region, and that the temperature logs in the lower section should exhibit a steady slope (Fig. 10). The slope of the section BC (Fig. 10) is close to the geothermal gradient in the study area. Point A represents the minimum value of the permafrost region. Therefore, the intersection point of lines AB and BC indicate the bottom depth of the permafrost region (Fig. 2).

**Calculation of porosity.** Porosity is typically calculated by acoustic (AC) logs, density (DEN) logs, and neutron porosity (CNL) logs. Resistivity logs and nuclear magnetic resonance (NMR) logs are also used to compute the porosity of gas hydrate reservoirs, but porosities computed by resistivity logs may be lower than the actual porosities because the resistivity of gas hydrates is much higher than that of pore water<sup>10,11,21–25</sup>. A NMR log measures the porosity filled by free fluids; as gas hydrates are solid, it is not difficult to calculate the saturation of gas hydrates by combining other porosity logs and a NMR log<sup>26</sup>.

CNL and NMR have not been previously applied in the study area; therefore, in this study, density and acoustic logs were used to compute the porosity of gas hydrate reservoirs (Table 5) and compared to porosity determined by core tests.

**Calculation of gas hydrate saturation.** The composition and structure of gas hydrate-bearing reservoirs are very complex; therefore, we simplified the model structure during calculation. Because of this simplification, it was prudent to use multiple models to improve the accuracy of our interpretations. As the gas hydrate-bearing reservoir was below the permafrost, gas hydrate saturation was evaluated as a function of the primary matrix (i.e., silicate, calcitic, or clay) and pore fluid (i.e., bond water, free water, or gas hydrate).

The evaluation of gas hydrate saturation typically employs resistivity and acoustic logs because the resistivity and acoustic properties of gas hydrate differ from the other components of the host rocks<sup>10,11,21-25,27,28</sup>. The different models used for evaluating gas hydrate saturation evaluation are listed in Table 6. We performed core tests in the laboratory and obtained the values of the scale factor (*a*), the cementation factors (*m* and *b*), and the saturation factor (*n*) of the study area. Due to the lack of local water analyses, we calculated the resistivity of the formation water ( $R_w$ ) using the apparent resistivity of the water saturated rock units (Eq. 1):

Well logs	Equation	Parameter description		
Density log	$\phi = \frac{\rho_{\mathrm{ma}} - \rho_{\mathrm{b}}}{\rho_{\mathrm{ma}} - \rho_{\mathrm{h}}} - V_{\mathrm{sh}} \frac{\rho_{\mathrm{ma}} - \rho_{\mathrm{sh}}}{\rho_{\mathrm{ma}} - \rho_{\mathrm{h}}}$	$\begin{array}{l} \rho_{ma}\!=\!matrix\;density; \rho_{b}\!=\!density\;log;\\ \rho_{h}\!=\!density\;of\;gas\;hydrate; \rho_{sh}\!=\!shale\;density; V_{sh}\!=\!clay\;content; \varphi\!=\!porosity. \end{array}$		
Acoustic log	$\phi = \frac{AC - AC_{ma}}{AC_{\phi} - AC_{ma}} \cdot \frac{1}{C_p} - V_{sh} \frac{AC_{sh} - AC_{ma}}{AC_{\phi} - AC_{ma}}$	$\label{eq:acoustic log; AC_ma} \begin{split} AC = & a coustic cransit time of the rock matrix; \\ AC_{\varphi} = & a coustic transit time of the water; \\ AC_{sh} = & a coustic transit time of the shale; \\ V_{sh} = & clay \ content; \\ \varphi = & porosity. \end{split}$		
Constants <sup>32,33</sup>	$\label{eq:pma} \begin{split} \rho_{ma} = 2.65  g/cm^3; \\ \rho_h = 0.9  g/cm^3; \\ \rho_{sh} = 2.3  g/cm^3; \\ AC_{ma} = 182  \mu s/m; \\ AC_{\varphi} = 620  \mu s/m; \\ AC_{sh} = 250  \mu s/m; \\ Cp = 1.68 - 0.0002  \times H \ (H \ is \ depth). \end{split}$			

Table 5. Equations used for calculating reservoir porosity.

Model	Model equation	Parameter description		
Archie equation	$S_{\rm h} = 1 - \left(\frac{{a}R_{\rm w}}{\phi^m R_{\rm f}}\right)^{1/n}$	a = scale factor; $m =$ cementation factor; $n =$ saturation factor; $\phi =$ porosity; $R_t =$ resistivity of the formation; $R_w =$ resistivity of the formation water; $S_h =$ gas hydrate saturation		
modified Archie equation	$S_h = 1 - \left(\frac{R_0}{R_1}\right)^{\frac{1}{n}}$	$R_0$ = resistivity of the formation saturated by water		
Indonesian equation	$\sqrt{C_{t}} = \sqrt{\frac{C_{w}}{F}} S_{w}^{n/2} + V_{sh}^{1-V_{sh}/2} \sqrt{C_{sh}} S_{w}^{n/2} S_{h} = 1 - Sw$	$\begin{array}{l} C_t\!=\!conductivity \ of \ formation; \ C_w\!=\!conductivity \\ of \ formation \ water; \ C_{sh}\!=\!conductivity \ of \ shale; \\ V_{sh}\!=\!clay \ content; \ S_w\!=\!water \ saturation \end{array}$		
Constants <sup>32,33</sup>	$a = 0.91; m = 2.1; b = 0.98; n = 3.2; R_w = 3 \Omega m; V_w = 1.5 km/s; V_h = 3.35 km/s; V_{ma} = 5.4 km/s.$			

Table 6. Models used for evaluating gas hydrate saturation.

$$Rw = \frac{\phi^m Rt}{ab} \tag{1}$$

where  $\phi$  is porosity and *Rt* is rock unit resistivity. The resulting  $R_w$  of the study borehole is ~3  $\Omega$ m. To obtain the resistivity of the units saturated by water ( $R_o$ ), we used the following equation (Eq. 2):

$$Ro = \frac{aRw}{\phi^m} \tag{2}$$

where *a*, *b*, *m*, and *n* were obtained by core tests and the other empirical parameters were from the literature.

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#### Acknowledgements

This research was supported by the National 863 Plan [Grant No. 2014AA06A608], the National Special Research Fund (Gas Hydrate Resource Exploration and Production Testing Project) [Grant No. GZHL20110324], and the National Nature Science Foundation of China [Grant No. 41574121]. We thank Drs Miao Luo and Sinan Fang for their constructive suggestions.

#### **Author Contributions**

Z.Z.L. and H.P.P. wrote the main manuscript, H.F. and W.L.G. provided technical guidance for the writing of the manuscript, and D.M.L. was involved in well logging and prepared Figures 3, 5, and 7. All authors reviewed and consented to the publication of the manuscript.

#### Additional Information

Competing Interests: The authors declare no competing interests.

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