

ORIGINAL ARTICLE

Effects of ultrasound on the morphology and properties of propylene-based plastomer/nanosilica composites

Bo Peng¹, Hong Wu¹, Wenting Bao¹, Shaoyun Guo¹, Yong Chen², Hua Huang², Hongyu Chen², Shih-Yaw Lai² and Jinder Jow³

Propylene-based plastomer/nanosilica composites, with a filler content of 1–4 wt%, were prepared by a specially designed ultrasound-assisted extrusion system that was developed in our laboratory. The effects of ultrasound on the morphology, as well as the rheological and mechanical properties of the composites, were studied in this paper. In spite of slight ultrasound-induced degradation of the polymeric matrix, the results showed that the strength and elongation of the composites at break, in most cases, still improve in the presence of ultrasound because of ultrasound-induced homogeneous dispersion of nanoparticles in the polymeric matrix (as confirmed by scanning electron microscope, transmission electron microscope and differential scanning calorimetry studies). Dynamic rheological measurements also indicate that ultrasound-induced compatibilization has a more predominant role than does degradation. From dynamic mechanical measurements, it was found that ultrasound-induced degradation results in a drop in the dynamic storage modulus and glass transition temperature for composites with 4 wt% filler content, whereas ultrasound-induced compatibilization enhances their loss factor values.

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INTRODUCTION

In recent years, polymer/inorganic nanocomposites, in which the size of the dispersed particles is < 100 nm in at least one dimension, have attracted tremendous interest in both academic and industrial researchers. Many studies report significant improvement in the desired properties of nanocomposites, such as their mechanical properties, barrier properties, optical transparency and solvent/heat resistance, compared with those of bulk polymers or conventional microcomposites.^{1–3} These improvements can be achieved at a very low loading of the inorganic component (1–10 wt%) compared with conventional filled polymers, which require high loading (25–40 wt%). These studies indicate that polymer/inorganic nanocomposites are much lighter in weight and easier to process than conventional microcomposites.⁴

To a large extent, improvement in these properties depends on the morphology and dispersion of the nanoparticles in the matrix. However, obtaining a homogeneous dispersion of nanoparticles in a polymeric matrix is a very difficult task when using only a simple mixing method, because of the strong tendency of nanoparticles to agglomerate. To break down the agglomerates of nanoparticles, many researchers have attempted various routes to prepare nanostructural composites in recent years, such as the sol-gel process,⁵ *in situ* intercalative polymerization^{6,7} and *in situ* polymerization in the

presence of nanoparticles.⁸ These methods, characterized by complex polymerization and special conditions, are not only incompatible with current industrial processes such as extrusion and injection molding, but are also inapplicable for the mass production of polymer/inorganic nanocomposites. In view of the cost-effectiveness and feasibility of the available processing techniques, melt blending of polymers with nanoparticles is still the optimum method of compounding. To achieve homogeneous dispersions of nanoparticles in polymeric matrices and to enhance the interactions between fillers and polymer matrices during the melt-blending process, several methods are generally applied:^{4,9–13} (1) the surface modification of nanoparticles with coupling agents or active monomers; (2) the polar group functionalization of polymers with partial oxidation, γ -rays, electron beams, microwaves, UV irradiation or polar grafting; (3) the addition of a bifunctional component (compatibilizer) that can interact with both fillers and polymer matrices; and (4) the mechanochemical modification of nanoparticles.

In addition, power ultrasound is a clean, efficient and attractive oscillation technology that has been applied to the melt-blending process of polymer/inorganic nanocomposites. Additional local molecular vibration is produced under ultrasound to better promote dispersion of nanoparticles in a polymeric matrix or better intercalation and exfoliation of clay. Relevant studies are largely focused on

¹The State Key Laboratory of Polymer Materials Engineering, Polymer Research Institute, Sichuan University, Chengdu, PR China; ²The Dow Chemical (China) Company Limited, Shanghai, PR China and ³The Dow Chemical Company Limited, Freeport, TX, USA

Correspondence: Professor H Wu or Professor S Guo, The State Key Laboratory of Polymer Materials Engineering, Polymer Research Institute, Sichuan University, 24, South Section 1, Yihuan Road, Chengdu, Sichuan 610065, PR China.

E-mail: wh@scu.edu.cn or nic7702@scu.edu.cn

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polymer/layered clay systems.^{14–18} However, very few works are devoted to research on polymer-filled, non-layered inorganic nanoparticles. In the current work, a special single screw extruder equipped with an ultrasound generator was used to compound a novel propylene-based plastomer with nanosilica. Here, propylene-based plastomers, called ‘Developmental Plastomers’ (DP) by the Dow Chemical Company, are a versatile family of propylene–ethylene copolymers, greatly different from both Ziegler–Natta and metallocene catalyst-based copolymers of propylene. Their characteristics have already been described in our previous works.^{19,20} Here, the ultrasound-assisted extrusion processing is expected to achieve a more effective breakup of the particle agglomerates in the absence of solvent and chemicals, thus yielding useful polymer/non-layered inorganic nanocomposites. The effects of ultrasound on the morphology, as well as the rheological and mechanical properties of the composites, are also discussed in detail.

EXPERIMENTAL PROCEDURE

Materials and equipment

DP was supplied in pellet form by Dow Chemical Co. (Freeport, TX, USA). It had a melt flow index of 5.0 g per 10 min (2.16 kg at 230 °C) and a density of 0.888 g cm⁻³. Nano-SiO₂ with an average primary particle size of 20 nm was purchased from Hongsheng Technology Co., Ltd. (Zhoushan, China). The main processing equipment used was a specially designed ultrasound-assisted extrusion system developed in our laboratory, and the schematic diagram and working principle were described in our previous work.²¹ The maximum power output and fixed frequency of the ultrasound were 300 W and 20 kHz, generated by a piezoelectric transducer. The oscillation of the ultrasound was in the direction parallel to the flow of the polymer melt.

Composite preparation

DP and nano-SiO₂ were premixed and then fed into the ultrasonic ultrasound-assisted extruder. The processing temperatures at different zones, from the hopper to the die, were fixed at 110, 160, 160 and 160 °C. The screw rotation speed was 5 r.p.m. The extrudates were palletized and then compression molded into 1-mm-thick plates at a pressure of 12 MPa and a temperature of 160 °C to obtain specimens for further measurements and characterization.

Measurements and characterization

Tensile testing of the composites was conducted with dumbbell-shaped samples on an Instron 4302 tension machine (Instron, Canton, MA, USA) with a crosshead speed of 500 mm min⁻¹ at room temperature. The size of the narrow section of the samples was 25 × 4 × 1 mm³. The reported values of strength and elongation at break are the average value taken from five tests.

The morphology of the dispersed phase in the polymer matrix was investigated using a JSM-5900 LV scanning electron microscope (SEM) manufactured by JEOL Co. (JEOL, Tokyo, Japan) at an accelerating voltage of 20 kV and a Tecnai-20 transmission electron microscope (TEM) manufactured by FEI Co. (Hillsboro, OR, USA) at an acceleration voltage of 200 kV. The samples for SEM were fractured in liquid nitrogen and coated with gold before observation, and those for TEM were taken from ultrathin sections of the composites.

Dynamic rheological measurements were taken using a Gemini 200 (Malvern Co., Worcestershire, UK) dynamic stress rheometer in an air atmosphere with 25-mm parallel plate geometry and a 1-mm sample gap. The dynamic frequency sweep tests were executed in the frequency range of 0.025–0.3 Hz at 160 °C with a strain amplitude of 2%, in which the rheological behavior was in the linear viscoelastic range.

Dynamic mechanical analysis was performed with a DMA Q800 instrument (TA Co., Boston, MA, USA) to measure the loss factor $\tan \delta$ and storage modulus E' over the temperature range from –50 to 100 °C at a constant frequency of 10 Hz and a small strain region of 0.2% using specimens of 17 × 7 × 1 mm³ dimensions in the tensile mode. The heating rate was 5 °C min⁻¹.

Differential scanning calorimetry analysis was carried out by a differential thermal analyzer 2100 (Dupont Co., Parkersburg, WV, USA). Samples were

heated from room temperature to 150 °C at a rate of 10 °C min⁻¹ and kept at this temperature for 5 min. They were then cooled to room temperature. All samples were kept under nitrogen while cooling curves were recorded.

RESULTS AND DISCUSSION

Tensile properties

The dependence of the strength at break of the DP/nano-SiO₂ composites on the SiO₂ content with various amounts of ultrasound power is shown in Figure 1. Without nanosilica, no significant difference in the tensile strength at break was observed with or without ultrasound power up to 200 W. This observation suggests that the slight change in molecular weight reported in our previous work²⁰ does not have a significant impact on the tensile strength. When nanosilica is added to DP in the absence of ultrasound during extrusion, an increase in the strength at break is measured up to 2 wt%, whereas there is a decreasing trend in the strength at break with an increase in silica content up to 4%. It should be attributed to the poor dispersion and interface adhesion of nanoparticles in the DP matrix at a high filler content. When ultrasound is introduced into the melt of the composites during extrusion, it helps to reduce the size of the SiO₂ nanoparticle agglomerate. Thus, the strength at break improves in most cases, except those at the 1 or 2% filler content under 200 W. SEM, TEM and differential scanning calorimetry analyses will be used to confirm these claims. However, for DP/nano-SiO₂ composites, 200 W ultrasound conversely decreased the strength at break of the composites at 1% filler content and showed no difference in tensile strength at 2% filler content.

Ultrasound provides the local molecular vibration to disentangle polymer chains and slightly reduce the molecular weight, both of which improve the filler dispersion. Increasing the ultrasound power level or the filler level is expected to increase the local power density in the polymer matrix and result in a more mechanochemical degradation that can provide a greater reduction in tensile strength. Therefore, ultrasound-induced dispersion of nanoparticles (that is, compatibilization) and degradation of the polymeric matrix are two competitive mechanisms, together resulting in a final value of the strength at break for the composites. When the nanofiller content is relatively low, its distribution in the polymeric matrix is easily determined; thus, the degradation of the polymeric matrix using high-power ultrasound may be detrimental to the mechanical properties of the composites.

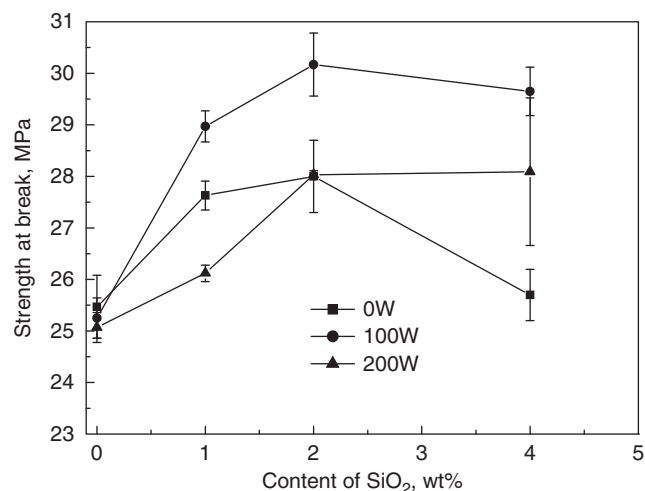


Figure 1 Dependence of strength at break of DP composites filled with SiO₂ on the SiO₂ content with various ultrasound power values.

However, when the filler content further increases, the nanoparticles are apt to agglomerate. Thereby, ultrasound-induced compatibilization has the more predominant effect on the strength at break of the composites compared with ultrasound-induced degradation. From Figure 2, using a 'mild' power (100 W) of ultrasound in our experiment seems more beneficial for enhancing the strength at break of the composites, even in chemically untreated nanoparticle-filled systems.

In addition, although the values of the elongation at break measured in this work have considerable deviations (Figure 2), the

results show a decreasing trend in elongation at break of DP by adding nano-SiO₂ in the absence of ultrasound, implying that the fillers cause a reduction in matrix deformation because of the introduction of mechanical restraints. On the other hand, the decline in the elongation at break of DP/nano-SiO₂ composites can be inhibited, and even the elongation at break increases with different degrees, by the aid of ultrasound-induced compatibilization during extrusion, especially for composites with a high filler content.

Morphology

Figure 3 presents SEM micrographs of the fractured surfaces of DP/nano-SiO₂ (96/4) composites. In the absence of ultrasound, large and stacked SiO₂ nanoparticles (~1 μm) can be observed on the fractured surfaces of the composites. However, the SiO₂ nanoparticles become smaller and the aggregation (~1 μm) of the SiO₂ nanoparticles disappears because of the 100-W ultrasound. In addition, a more homogeneous dispersion of SiO₂ nanoparticles into DP matrix is achieved. As shown in Figure 4, TEM micrographs further demonstrate the effect of ultrasound on the morphology of DP/nano-SiO₂ composites. When the composite melts flow into the ultrasound effect zone (that is, the die of the extruder), both the powerful vibration and the shatter of ultrasound lead to the disentanglement, and even scission, of macromolecular chains, and at the same time, they help to reduce the size of the agglomerates of SiO₂ nanoparticles and disperse them evenly in the DP matrix.

Dynamic rheological properties

The logarithm curves of dynamic rheological parameters, including the elastic modulus (G'), viscous modulus (G'') and complex viscosity

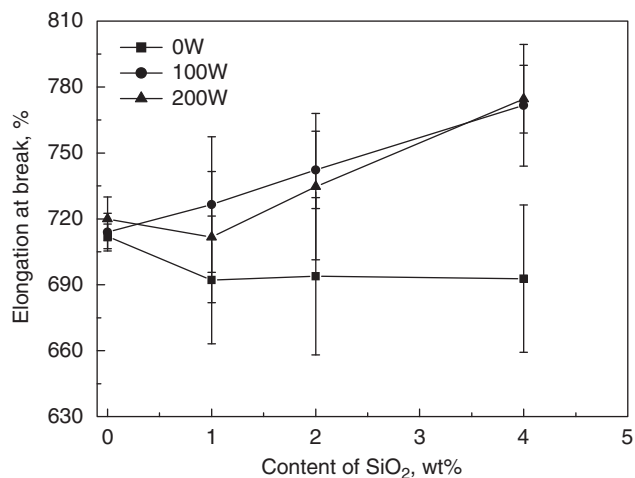


Figure 2 Dependence of elongation of DP composites filled with SiO₂ at break on the SiO₂ content with various ultrasound power values.

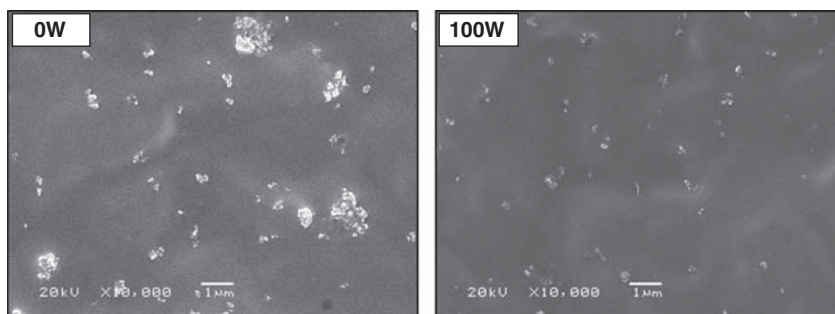


Figure 3 Effect of ultrasound on SEM micrographs for DP/nano-SiO₂ (96/4) composites.

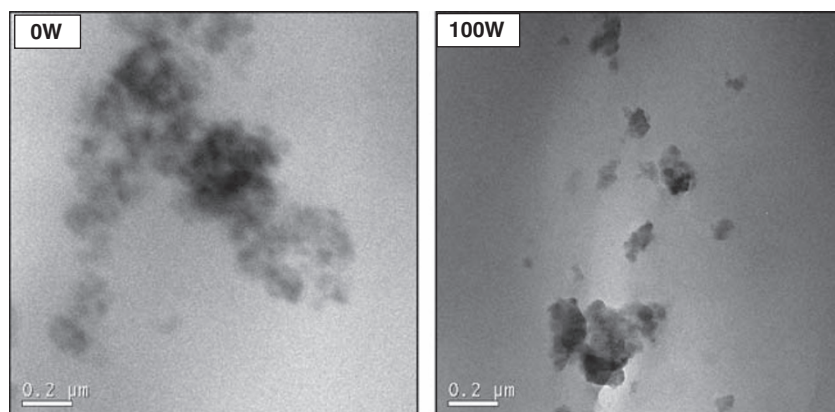


Figure 4 Effect of ultrasound on TEM micrographs for DP/nano-SiO₂ (96/4) composites.

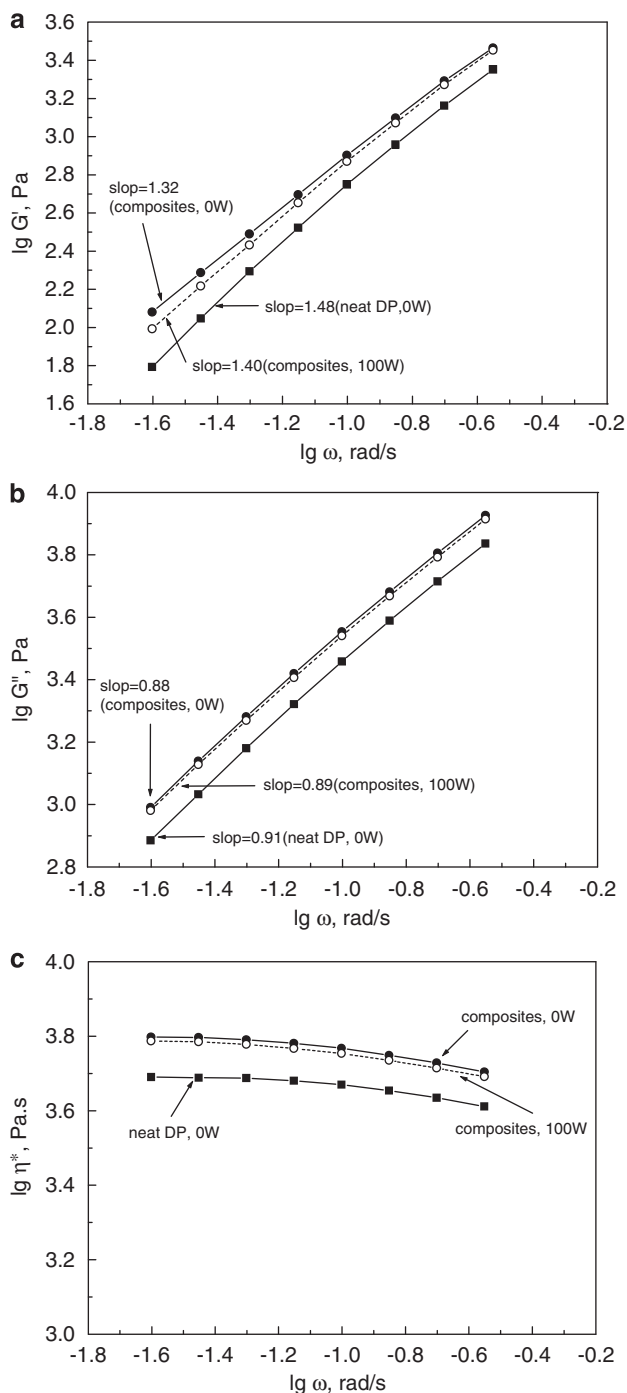


Figure 5 Dynamic rheological parameters, including (a) G' , (b) G'' and (c) η^* , versus ω for DP and DP/nano-SiO₂ (96/4) composites in the absence and presence of ultrasound.

(η^*), versus the angular frequency (ω) of the DP and DP/nano-SiO₂ (96/4) composites in the low frequency zone are shown in Figures 5a–c. As expected, the addition of nano-SiO₂ into the DP matrix results in an increase in G' , G'' and η^* . Conversely, the 100-W ultrasound applied during extrusion decreases the linear viscoelastic parameters of the composites. Ultrasound-induced dispersion of nanoparticles and degradation of the polymeric matrix can jointly determine the reduction.^{12,19,22} According to the linear viscoelastic

theory, the slopes of $\lg G' - \lg \omega$ and $\lg G'' - \lg \omega$ in the terminal zone (that is, the low-frequency zone) are closely related to the variation in the polydispersity of the polymer matrix and the composite morphology.^{23–26} In general, as the width of the molecular weight distribution increases, the slopes decrease. Previously mentioned in our work,^{19,20} the molecular weight distribution of neat DP increases, whereas its molecular weight decreases in the presence of ultrasound, indicating a decrease in the slopes of $\lg G' - \lg \omega$ and $\lg G'' - \lg \omega$. On the other hand, the better compatibility and more uniform dispersion of the particles in the polymeric matrix are beneficial and are shown by the rise in the slopes of $\lg G' - \lg \omega$ and $\lg G'' - \lg \omega$. As shown by the slopes marked in Figures 5a and b, the addition of nano-SiO₂ into the DP matrix reduces the slope values of DP. A similar phenomenon can be observed in most particle-filled systems.^{27,28} It is interesting that the slopes of composites increase with the introduction of ultrasound, which can be interpreted only by the fact that the effect of ultrasound-induced compatibilization on dynamic rheological properties is more significant than ultrasound-induced degradation.

Dynamic mechanical properties

Figures 6a and b depict the dynamic mechanical spectra (dynamic storage modulus E' and loss factor $\tan \delta$) as a function of temperature for DP and DP/nano-SiO₂ (96/4) composites in the absence and presence of 100-W ultrasound. Results clearly show that, in the absence of ultrasound, the addition of nano-SiO₂ particles into the DP matrix increases the E' values while decreasing the $\tan \delta$ values, indicating improved stiffness and deteriorative ductility of DP. The increase in stiffness is a result of the high modulus of nanosilica (70 GPa), whereas the reduction of ductility should be ascribed to the above-mentioned congregation of nano-SiO₂ particles. At the same time, all samples (Figure 6b) present a dispersive peak in the temperature range studied, which is attributed to the micro-Brownian motion of macromolecular chains in the amorphous phase of the DP matrix. The peak temperature is the glass transition temperature (T_g), the value of which is also marked in Figure 6b. Neat DP has a T_g of 12.4 °C, whereas 4 wt% filler loading decreases it to 11.3 °C. Liu *et al.*²⁹ obtained similar results in polypropylene/layered silicate nanocomposites.

With the introduction of ultrasound, the values of E' and T_g of the composites decreased, indicating a decrease in stiffness for the composites and an enhancement in the mobility for the DP chain segment. All these observations should be attributed to either the decreased molecular weight of DP or the disentangled polymer chains, both of which were induced by ultrasound. Simultaneously, ultrasound-induced degradation of the DP matrix results in an increase in $\tan \delta$ values.²⁰ In addition, a more uniform dispersion of nanoparticles in the presence of ultrasound increases the effective volume fraction of the filler in the DP matrix and conclusively enhances the dissipation capability of particle-filled systems to exterior energy. It also benefits the increase in $\tan \delta$ values of the composites.

Crystallization properties

Figure 7 shows the cooling curves of DP and DP/nano-SiO₂ (96/4) composites, and the data describing crystallization temperature (T_c) and enthalpy (ΔH_c) are listed in Table 1. These data show that the addition of nano-SiO₂ can lead to the heterogeneous nucleation of DP at a higher temperature and to the increase in the crystallization temperature. The crystallization temperature of DP in composites is enhanced further because of the presence of 100-W ultrasound, indicating that ultrasound is helpful to the distribution of nano-SiO₂ in the DP matrix. As the filler dispersion increases, the interfacial

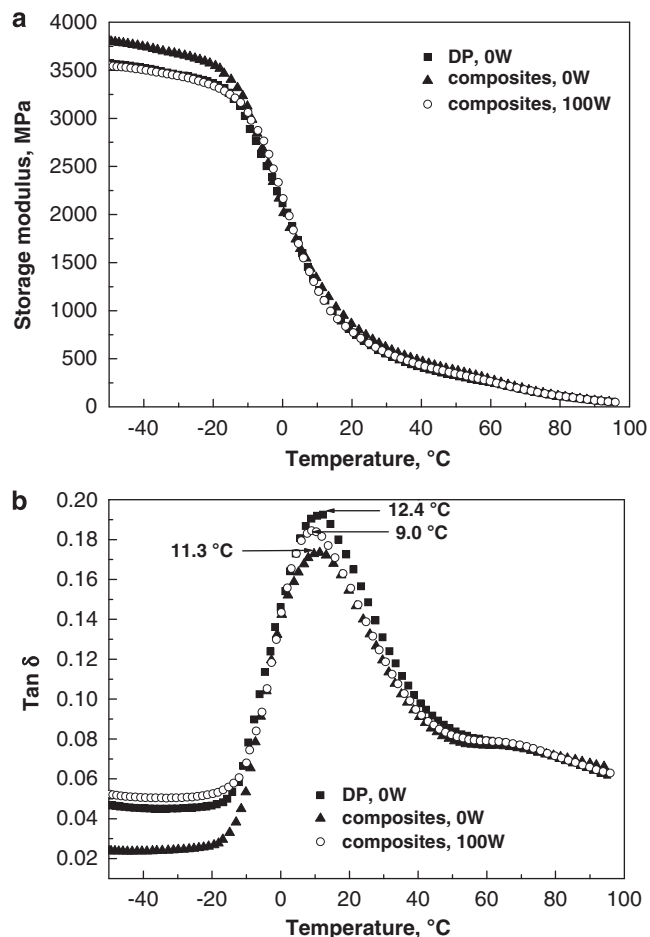


Figure 6 DMA traces of (a) storage modulus and (b) loss factor versus temperature for DP and DP/nano-SiO₂ (96/4) composites in the absence and presence of ultrasound.

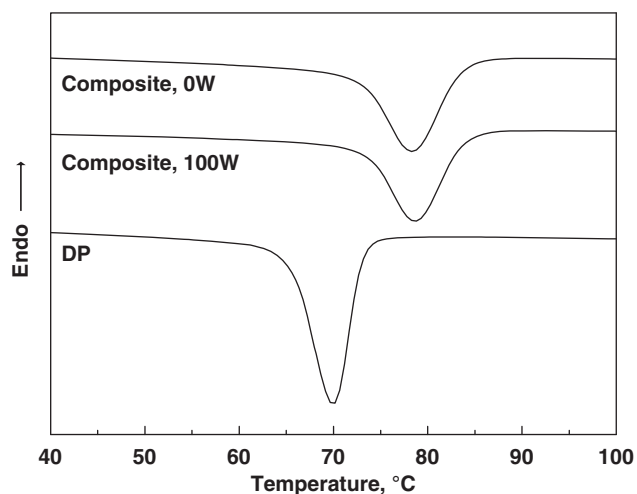


Figure 7 Differential scanning calorimetry cooling curves of DP and composites.

interaction strengthens, and the nucleation becomes more obvious. Further, the addition of nano-SiO₂ can reduce the crystallization enthalpy of DP because the movement of the molecular chain of

Table 1 DSC data of the samples

| Samples | DP | Composites, 0W ultrasound | Composites, 100W ultrasound |
|---------------------------------|------|------------------------------|--------------------------------|
| T_c , °C | 69.9 | 78.3 | 78.6 |
| ΔH_c , Jg ⁻¹ | 55.0 | 53.2 | 45.1 |

Abbreviations: DP, Developmental Plastomers; DSC, differential scanning calorimetry; ΔH_c , enthalpy; T_c , crystallization temperature.

DP is limited by the filler, and the crystal becomes more imperfect. It becomes more obvious when a 100-W ultrasound is applied to the composite.

CONCLUSIONS

In this paper, DP/nano-SiO₂ composites with a filler content of 1–4 wt% were prepared through an ultrasound-assisted extrusion at 160 °C. Ultrasound-induced homogeneous dispersion of nanoparticles in a polymeric matrix, as confirmed by SEM and TEM studies, as well as by ultrasound-induced compatibilization, can overcome the negative influence stemming from the ultrasound-induced degradation of the polymeric matrix. Thus, the strength and elongation at break (under conditions of a larger strain region) of the composites improved in most cases. With the introduction of ultrasound, an increase in the slopes of $\lg G' - \lg \omega$ and $\lg G'' - \lg \omega$ for the composites with 4 wt% filler content also indicates that the effect of ultrasound-induced compatibilization is dominant, along with the decrease in the values of G' , G'' and η^* . Nevertheless, ultrasound-induced degradation can result in a drop in the dynamic storage modulus E' (under conditions of a smaller strain region) and the glass transition temperature T_g for the composites with 4 wt% filler content. Together with the ultrasound-induced compatibilization, both result in the enhancement of the loss factor, $\tan \delta$. Finally, the results of differential scanning calorimetry also show that ultrasound is helpful in the distribution of nano-SiO₂ in the DP matrix.

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