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OPEN Channel-forming discharge based on the extreme value identification of sediment-carrying capacity index

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Channel-forming discharge (D_{cf}) is an important parameter in river management and reservoir flood regulation. Applying the methods for calculating D_{cf} to reaches downstream reservoirs characterized by drastic changes in water and sediment conditions and long-term scouring status is difficult. Based on the riverbed-shaping principle of sediment-laden water flow, while simultaneously considering the active action of water flow and response of the riverbed, this study proposes a new method for calculating D_{rf} by identifying the extreme value of the suspended sediment-carrying capacity index. The application of this method to the middle and lower reaches of the Yangtze River showed that after the impoundment of the Three Gorges Reservoir, D_{cf} in this section was reduced by an amplitude between 2500 and 4700 m³/s. The results can be used to guide the operation of the Three Gorges Reservoir and the management of the middle and lower reaches of the Yangtze River, thus providing reference for other river channels downstream of the reservoir.

Keywords channel-forming discharge, Suspended sediment-carrying capacity, Three Gorges Reservoir, Flood regulation of reservoirs, The middle and lower reaches of the Yangtze River

The riverbed shaping effect of the channel-forming discharge $(D_{\rm ef})$ is equivalent to a multi-year flow discharge $(D_{\rm f})$ process. It is closely related to flood magnitude, process, duration, and suspended sediment concentration (SSC) and its combination with the water flow process and river boundary conditions. It is not only an important parameter that reflects the geometry of the river¹, but also an indicator of the SSC of the river channel. It is the foundation of river evolution analysis and plays an important role in river planning and regulation^{2,3}

The $D_{\rm f}$ process when the water level ($Z_{\rm f}$) is flush with the surface of the sandbar in the river reach is widely applied in the determination of D_{cf} in plain rivers^{4–6}, and is referred to as the bankfull (BK) method. Certain viewpoints suggest that the peak D_f at a certain frequency has a greater effect on riverbed evolution⁷; therefore, it can be used as D_{cf}^{8} . This method is called the guaranteed rate (GR) method. The improvement in this method mainly focuses on the optimization of the guarantee rate⁹. Because the adjustment of the riverbed ultimately depends on incoming water and sediment, these two factors have been adopted to analyze D_{cf} in numerous studies. For example, the effective discharge concept has been used to characterize the Cumberland Basin streams¹⁰, Liaohe River¹¹, and middle Yangtze River^{12,13}. Makayev adopted discharge as the D_{cf} when the product of the suspended sediment-carrying capacity (SSCC) and its corresponding D_f guarantee rate was maximized^{14,15}, which is referred to as the MK method in this study. The results of the MK method were basically the same as those of the effective sediment transport discharges in Heilongjiang River¹⁶, but closer to the results of the BK method in the Huai River¹⁷ and Han River¹⁸. In the Yellow River, the difference between the MK and BK methods was relatively obvious¹⁹. In the fluctuating backwater area of Three Gorges Reservoir (TGR), the MK method results were similar to those of the GR method²⁰. In addition, the method based on the curve of the product of the SSC and its frequency was proposed. This method is simpler and its results for the Yellow River were not substantially different from those of the MK method²¹. The multiyear average value of the daily averaged flood $D_{\rm f}$ was also used as D_{cf} ; however, it is not suitable for urban river channels²².

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The D_{cf} values calculated using the methods above differed from each other^{23,24}, and have different adaptabilities to different rivers^{25,26}. The BK method is more suitable for channels with relatively stable sandbars and deep pools, whereas the MK method generally yields two D_{cf} values, which do not reflect drastic changes in water and sediment conditions²⁷. Optimized methods have also been developed. In the Yellow River, D_{cf} is defined as the first and second $D_{cf}^{28,29}$ and has been used to guide the regulation of the Xiaolangdi Reservoir³⁰. The introduction of parameters, such as SSCC³¹, SSC frequency^{27,32}, riverbed balance³³, sliding analysis correction³⁴, and the ratio of squared SSC to D_{f}^{35} has also optimized the calculation of D_{cf} . In addition, some methods are based on the optimization of certain parameters, such as the use of a formula for calculating the bed load sediment transport rate¹⁸, the selection of representative periods, and the index in the MK method³⁶. Certain methods are based on the distribution characteristics of flow frequency curves¹¹, numerical simulation, and deep learning models³⁷.

In summary, the above methods have mainly been applied to rivers with a high SSC^{38–40}. For those downstream of reservoirs with low SSC, the adjustment of the medium flood frequency and the relationship between water and sediment after reservoir regulation will have a significant impact on $D_{cf}^{41,42}$. Numerical experiments have also shown that sediment transport patterns, channel morphology, D_f variation, and recording length interact with each other, thereby affecting the estimation of D_{cf}^{43} and resulting in obvious changes in D_{cf}^{44} . The application of existing methods to reaches downstream of reservoirs characterized by drastic changes in water and sediment conditions and long-term scouring status is difficult and necessitates improvement. Based on the fundamentals of riverbed deformation and the background of channel reclamation downstream of reservoirs, this study proposes a method for accurately identifying the D_{cf} in view of the SSCC index in those altered flow and sediment regime conditions, thus enabling the scientific scheduling of reservoirs and ensuring the shaping effect of water flow downstream of the reservoirs, such as in the TGR.

Materials and methods Study area

With the commissioning of the TGR and a series of cascade reservoirs in the upper Yangtze River, hydrological elements, such as the D_f magnitude, temporal and spatial distribution, and the SSC entering the middle and lower reaches of the Yangtze River (MLYR) have changed, resulting in significant changes in the evolution of the riverbed downstream of the reservoirs⁴⁵. The first and foremost change was a reduction in the flood peak. For example, in 2010 and 2012, the peak floods flowing into the TGR reached 70,000 m³/s and 71,200 m³/s, respectively, but the D_f released by the reservoir was controlled to within 45,000 m³/s. The second was the increase in the medium water duration. From 2008 to 2012, the duration of D_f between 25,000 and 40,000 m³/s in July and August flowing into the MLYR, represented by the Yichang hydrographic station extended from 121 to 144 days. In addition, the increased D_f during the dry seasons before flood season and decreased D_f after flood season constitute changes in the temporal and spatial distribution of water flow.

The change in the sediment is relatively obvious, and was manifested by a significant reduction in the SSC and sediment particle size⁴⁶. The average annual transported sediment amounts at the Yichang, Hankou, and Datong hydrographic stations from 2003 to 2016 were 0.381×10^8 t, 1.03×10^8 t, and 1.4×10^8 t, respectively, which were 92%, 74%, and 67% less than those before storage in the TGR. The relationship between water and sediment was also altered, as shown by a lower SSC under the same $D_{\rm f}$. In future, following the completion and utilization of reservoirs in the upper reaches of the Yangtze River, the amount of sediment entering the MLYR will be further reduced, and the riverbed, not only the reach in the middle Yangtze River⁴⁷, but even the estuarine areas^{48,49} will undergo a longer period of scouring adjustment.

Based on the information above, the MLYR (Fig. 1) is a typical river section affected by reservoir impoundment. Therefore, it was selected as the study area and will provide reference for other river reaches in downstream reservoirs.

Data

The data used in this study mainly consisted of cross-sectional terrain data measured at different sections of the MLYR. This collection included topographic data from 16 sections measured during the dry seasons since 1981. To calculate the hydraulic elements, such as the flow velocity (U) and water depth (H) of the sections, daily averaged $D_{\rm fr}$ SSC, and $Z_{\rm f}$ data from the eight hydrographic stations upstream and downstream of the sections were collected simultaneously. In addition, certain river sections, such as the Nanyangzhou, Nanmenzhou, and Luxikou reaches, were selected to analyze the relationship between the hydraulic elements. These typical river sections have not yet implemented large-scale sandbar protection projects, and their evolution is almost natural, which is likely to reflect the shaping effect of water and sediment conditions on the riverbed. The positions of the cross sections and hydrographic stations are shown in Fig. 1b. All data were sourced from the Hydrological Bureau of the Yangtze River Water Resources Commission, and detailed information is provided in Table 1.

Method

Physical background of riverbed deformation

Riverbed deformation is the result of the sediment-laden water flow movement, which can be expressed in the following formula⁵¹:

$$\rho_s \frac{\partial z_b}{\partial t} = \alpha \omega \left(S - S^* \right)$$

where ρ_s is the dry weight of the sediment, z_b is the riverbed deformation amplitude over time t, α is the saturation recovery coefficient, ω is the sediment particle settling velocity, S is the SSC, and S^* is SSCC of the water flow, which is determined by the index U^3/H . Among them, ρ_s and ω are the basic properties of sediment, and α



Figure 1. Study area: (a) the Yangtze River Basin; (b) the middle and lower reaches of the Yangtze River. This figure was modified from the picture in reference⁵⁰, which includes the annotation of geographical information, such as boundary points Yibin, Yichang and Hukou among the upper, middle, and lower reaches of the Yangtze River, as well as the other important geographical locations, the hydrographic stations and cross-sections.

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Data type	Measurement	Source	
Daily averaged $D_{\rm fr}$ SSC and $Z_{\rm f}$ of the 8 hydrographic stations	1981-2022	Hydrological Bureau of the Yangtze River Water Resources	
Topographic data of the 16 cross-sections	Since 1981	Commission	

Table 1. Data information.

has a certain range of values, which can be determined by the calibration of measured data. Therefore, riverbed deformation mainly depends on the contrast between *S* and *S*^{*}. When *S* is greater than *S*^{*}, the riverbed is silted, and vice versa. When the two were comparable, the riverbed was in equilibrium. This indicates that the $D_{\rm f}$ corresponding to the maximum SSCC has the most significant bed shaping effect.

Method to recognize D_{cf} based on the SSCC index

Scouring under long-term subsaturated flow is the current and likely the considerable future state of the riverbed downstream of reservoirs. Channel development is the result of the combined effect of water flow, sediment, and channel boundaries, and the calculation of D_{cf} should consider these two factors simultaneously. There have been attempts to do so in the past, but when applied to rivers downstream of reservoirs, certain factors may change from primary to secondary, such as SSC. In rivers downstream of the reservoir, particularly downstream of the cascade reservoirs, the SSC is generally extremely small. For example, the annual sediment amount delivered into the MLYR has been below 1×10^7 t since 2014^{46} , and the average value from 2014 to 2016 has been reduced by more than 98% compared to the multi-year average value before storage in the TGR. The incoming SSC was

significantly mismatched with the SSCC. The shaping of the river channel by water flow is more dependent on its capacity to pick up sediment from the riverbed.

However, the SSCC does not always increase with the D_f but starts to decrease upon exceeding a certain value. Figure 2 shows the correlation between the Z_f , U, and the SSCC index U^3/H in several typical sections of the MLYR that have high sandbars and are minimally affected by human activities. As the Z_f increases, U does not continuously increase, but turns at a particular Z_f . This turning point is also the extreme value point of U^3/H , which indicates that the ability of the water flow to deliver sediment and shape the riverbed reaches its maximum value. The D_f corresponding to the Z_f at this extreme point can be considered to be D_{cf} . The specific steps of this method are as follows.

First, we selected cross sections with clear sandbars and deep pools that were less affected by human activities within the river channel and collected their terrain observation data. The selected river sections need to have a clear binary structure of sandbars and deep pools. Figure 3 shows the cross-sectional morphology of several typical river sections selected in this study. Evidently, the cross-section distribution of these river sections has obvious sandbars and deep pools. During the dry season, water flows in deep pools, while during the flood season, water flows over the sandbars and fills the cross-section. The relatively little disturbance caused by human activities refers to the lack of bank and sandbar protection. In this case, the river bed evolution is mainly influenced by water, sediment, and riverbed boundary conditions.

Second, we calculated U and U^3/H of the cross sections at different Z_f . For a given cross-section, it can be divided into multiple trapezoidal or triangular elements based on the measured points as shown in Fig. 4a. When Z_f is determined, the area (A_i) of each sub section is calculated using the triangle or trapezoidal area formula. The total area (A) and width (B) of the section corresponding to Z_f can be obtained by accumulating A_i and dx_i of the sub sections. According to the $Z_f \sim D_f$ relationship curve as shown in Fig. 4b, the D_f corresponding to Z_f can be found, then U and H can be calculated by $U = D_f/A$ and H = A/B. The correlation diagram between U, U^3/H , and Z_f is shown in Fig. 2.

Third, the Z_f corresponding to the extreme value points of U and U^3/H on the correlation diagram were determined. Determining this extremum necessitates the use of polynomials to fit the scatter points as shown in Fig. 2. When the first derivative of the fitted polynomial is 0, the corresponding Z_f is the one corresponding to the extreme point of U^3/H . Then the D_f corresponding to this Z_f was queried using the relationship between the Z_f and D_f at a nearby hydrographic station. This D_f is D_{cf} .

Results

D_{cf} in different river sections

Table 2 shows the D_{cf} and its changes along the MLYR before and after the TGR impoundment, calculated using the method proposed in this study. As seen in the table, the decreased magnitude of D_{cf} from before to after the TGR impoundment was generally between 2500 and 4700 m³/s, with the Zhicheng hydrographic station



Figure 2. Relationship between $Z_{\rm f}$, U, and SSCC index in typical river sections.







Figure 4. Diagram of hydraulic element calculation for cross-section: (a) cross-sectional terrain; (b) $Z_{\rm f} \sim D_{\rm f}$ relationship curve.

	$D_{\rm cf}$ (m ³ /s)				
Hydrographic station	Before TGR	After TGR	Changes	Representative cross section	
Zhicheng	34,900	30,200	-4700	Jing6	
Shashi	30,500	27,200	- 3300	Jing28, Jing58	
Jianli	27,500	25,000	-2500	Jing144, Jing177	
Luoshan	35,000	31,700	- 3300	CZ04 – 1, JieZ3 + 3, CZ10 – 1	
Hankou	43,000	40,200	- 2800	CZ58 – 1, CZ72, CZ76 – 1	
Jiujiang	44,000	40,700	- 3300	CZ108-1, CZ118	
Datong	50,500	47,700	- 2800	CX63+69, CX85, CX178	

Table 2. *D*_{cf} and its changes in the MLYR before and after the impoundment of TGR.

having the largest reduction and the Jianli hydrographic station the smallest. The reduction in the section below Chenglingji was approximately 3000 m^3 /s.

Examination of D_{cf}

The key to the method in this study is to determine the extreme value of the SSCC index, and there are requirements for the shape of the cross sections. This method is not applicable to a single channel without sandbars. To examine the reasonableness of this method, we further established the correlation relationship between D_f and SSC in the MLYR during 1981–2002 (Fig. 5). During this period, the MLYR was in a state of relative equilibrium between sediment erosion and siltation⁵². The correlations have turning points. The SSC corresponding to this turning point can be considered the SSCC, and the corresponding D_f has the strongest ability to shape the riverbed. This relationship does not exist or is not evident after the impoundment of the TGR (2003–2020), meaning that the entire MLYR is in a state of subsaturated sediment transport, and the SSC is far from the SSCC. There were no obvious trend turning points in the relationship after the impoundment of the TGR (Fig. 6). Therefore, this method was examined using only the data before the impoundment of the TGR.

Before the impoundment of the TGR, the characteristics of the alluvial plain river began to appear in the river section downstream of Zhicheng. As seen in Fig. 5, the turning features of this relationship are becoming increasingly apparent. The $D_{\rm f}$ at the stations corresponding to the turning point was very close to the $D_{\rm cf}$ calculated using this method, as shown in Table 2. This indicated that the proposed method was reasonable.

Discussion

Comparison of different methods

Based on the concept that the evolution of a river channel is subject to water and sediment movement, this study presents a method for calculating D_{cf} by identifying the extreme points of the SSCC index. The method is based on the cross-sectional topography and the relationship between the Z_f and D_f data of the studied river section, and is relatively simple, but with a good physical background. To test the rationality of this method, Fig. 7 shows a comparison of the D_{cf} calculated by the BK, GR, and MK methods, and the method proposed in this study, as well as the effective discharge. Table 3 lists the differences before and after water storage in the TGR.

Comparison of the results calculated by different methods revealed that before and after storage of the TGR, the D_{cf} calculated by the GR method exceeded those calculated by the other three methods. Specifically:



Figure 5. Relationship between *D*_f and SSC in MLYR before the TGR impoundment (1981–2002).

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Figure 6. Relationship between $D_{\rm f}$ and SSC in MLYR after the TGR impoundment (2003–2020).

- (1) The D_{cf} calculated using the MK method considers two factors: the SSCC of the D_{f} and the duration of different D_{f} , thus providing a theoretical basis and physical significance. However, the drawback of this method is that the relative change value is often limited by D_{f} classification, which makes it difficult for the method to reflect the changes along the river channel. The effective discharge¹² at Jianli station is relatively close to the MK method result. In addition, it shows that the effective discharge at Yichang station decreases with an amplitude ranging from 15,000 to 20,000 m³/s, and 5000 to 10,000 m³/s at Shashi station after 2002¹³.
- (2) The GR method is based on experience in selecting the flood $D_{\rm f}$ during a certain recurrence period as $D_{\rm cf}$. This method exhibits strong empiricism and subjectivity. However, a water depletion phenomenon has been observed in the MLYR after the construction of the TGR. Although the results obtained by this method can reflect the changing trend along the river channel, they depend solely on the flow process and do not reflect the response of the river boundary conditions.
- (3) The starting point of the BK method is the change in Z_f, which is often influenced by the water, sediment, and boundary conditions of the reach. This method can compensate for the shortcomings of the MK method by responding to changes along the river reach, but has two limitations. When selecting the terrain of the river channel at a certain period to determine the bankfull elevation at different positions, a large individual error is often made. In addition, most of the sandbars in the MLYR have implemented protection projects, which are influenced by both up-input water and sediment as well as human activities. Thus, it cannot fully reflect the shaping effect of water and sediment, leading to errors in the results.
- (4) The method proposed in this study considers both the shaping effect of water flow and the response of the riverbed, and is simultaneously verified using the characteristics of water flow loaded by sediment. The results are between those of the MK and BK methods and reflect the characteristics of changes along the river channel. The limitation of this method is that the studied river sections should have clearly distinguishable sandbars and deep pools. In this type of river, the synergistic effect of water flow and sediment in shaping the riverbed is relatively pronounced⁵³, which makes it easier to detect D_{cf} .

Influencing factors of D_{cf}

The water situation in the Yangtze River Basin has a certain periodicity. After the TGR impoundment, the upper reaches of the Yangtze River enter a hydrological cycle of runoff depletion. The insufficient precipitation leads



Figure 7. D_{cf} calculated by different methods: (a) before the TGR; (b) after the TGR.

Hydrographic station	MK method	GR method	BK method	Effective discharge ¹²	This study
Yichang	- 3000	-9100	-4200	-	-4200
Zhicheng	-6000	-13,100	-6200		-4700
Shashi	- 3000	- 8800	- 3800		-3300
Jianli	- 3000	- 6600	- 3000	-400	-2500
Luoshan	- 3000	- 8400	- 5000	-	- 3300
Hankou	- 3000	- 8200	-4400		-2800
Jiujiang	- 3000	-9100	-4900		- 3300
Datong	- 3000	-7000	-4800		-2800

Table 3. Difference in D_{cf} before and after the TGR.

to a corresponding decrease in the runoff entering the MLYR, which in turn leads to a reduction in the source of sediment in the river. Therefore, the relatively dry hydrological cycle of the main stream of the Yangtze River after the TGR impoundment is one of the important factors for the smaller calculated values of D_{cf} in the MLYR compared to before the impoundment.

The sediment interception effect of reservoir operation has led to a reduction of over 98% in sediment transport at Yichang station in recent years, which will have a direct impact on the parameter values in the MK method. With the gradual implementation of dry season replenishment, peak shaving during flood season, and early storage after flood season in reservoirs, the impact of reservoirs on the downstream river runoff process is becoming increasingly apparent. The replenishment during dry season and early storage after flood season mainly affect the flow of small and medium water, and have a relatively small impact on D_{cf} . The peak shaving scheduling during the flood season changes the natural flood process, with the most obvious being the reduction of peak flow. Therefore, when using the MK or GR methods to calculate D_{cf} the values after the TGR should be slightly smaller.

Reservoir regulation not only directly changes the water and sediment conditions, but also brings about changes in the river boundary. The riverbed is generally eroded, and the cross-sectional shape, longitudinal profile shape, sandbar shape, and even bed surface shape will be adjusted accordingly. The ultimate goal of these adjustments is to reduce the flow velocity, match the SSCC with the incoming SSC, and thus make the river tend towards an equilibrium state. In this sense, after the TGR impoundment, the D_{cf} downstream the dam should also decrease, thereby promoting the evolution of the river towards a balanced state.

To stabilize the river channel conditions, remediation projects, most of which are in the form of protection, have been implemented. In addition, embankments have been built to develop and utilize the sandbars. These projects have altered the mobility of local river boundaries and disrupted the natural and continuous response of protected geomorphic units to water and sediment processes. When determining the D_{cf} using the BK method or that proposed in this study, the deformation of the sandbars is limited and often cannot reflect the response relationship between sandbar erosion and changes in water and sediment conditions.

Implications on reservoir and river management

The operation of TGR, controlling reservoir in the upper reaches of the Yangtze River needs to ensure the flood safety of the reservoir and the downstream river channel, reduce sedimentation in the reservoir area, and ensure the development of the downstream river channel of the dam. This indicates that when encountering floods, it is not only necessary to control the peak flood D_f and total flood volume in combination with the reservoir flood control capacity, but also to maintain a certain D_f during the flood season to increase the sediment output capacity of the reservoir. In addition, the output D_f needs to reach the D_{cf} and maintain it for a certain period of time.

Since the TGR entered the experimental storage stage, peak shaving operations have been carried out for flood peaks exceeding 45,000 m³/s. The frequency of high floods occurring downstream of the dam has decreased, and the overflowing probability for high sandbars has decreased correspondingly. Comparison of the calculation results of different methods reveals that compared to before the water storage of TGR, the D_{cf} downstream the dam has decreased after the water storage, and the magnitude of reduction is smaller as it moves downstream. The actual evolution shows that the adjustments to the cross-sectional shape, longitudinal profile shape, and sandbars shape downstream the dam are within the expected range of changes. Certain branching channels have also exhibited expected shrinkage, and the reduction in D_{cf} is acceptable.

In the long run, maintaining the current peak shaving operation of the reservoir can achieve various goals such as flood control and reservoir sedimentation. However, at the same time, the output D_f exceeding the D_{cf} downstream of the dam with a certain duration within the year should be satisfactory. In each hydrological cycle, there should be a certain number of years that meets the duration of D_{cf} to avoid further reduction and ensure the normal development of the river. For the river management downstream reservoirs, full consideration should be given to the actual situation of reduced D_{cf} to develop effective response measures. This study provide a new method for determining the D_{cf} . However, the specific duration of D_{cf} and its total number of years in a hydrological cycle need to be analyzed in greater detail in future research studies.

Conclusions

By combining the actual river evolution in the MLYR and considering the water, sediment and riverbed boundary, this study proposed a method for determining D_{cf} by identifying extreme value of the SSCC index. The results indicated that this extreme value is easily detected in the MLYR. Calculations show that after the impoundment of TGR, the D_{cf} along the MLYR decreases to varying degrees, with an average of approximately 3360 m³/s. The maximum reduction (4700 m³/s) occurred in Zhicheng, followed by Yichang with 4200 m³/s. The reduction in Shashi, Luoshan, and Jiujiang stations were 3300 m³/s, while those in Hankou and Datong stations were 2800 m³/s. Jianli station reported the lowest reduction: 2500 m³/s.

In the river downstream of the reservoir, water and sediment conditions, and river boundaries can be derived by specific hydrological cycle changes, reservoir scheduling and operation, river management, and the development and utilization of sandbars. Among these, the focus was on hydrological cycle changes and reservoir operations. The former mainly affects the conditions of water and sediment, whereas the latter also affects the changes the river boundary conditions. The implementation of large-scale river regulation projects also has a significant impact on D_{cf} . The method proposed in this study is expected to provide D_{cf} in downstream river regulation and reservoir operation to better leverage the comprehensive benefits of the reservoir and improve the effectiveness of downstream river regulation projects.

Data availability

The datasets used in this study are available from the corresponding author upon request.

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Author contributions

H.G. contributed to the study conception, material preparation, data collection and analysis, and funding acquisition; L.Z. contributed to material preparation, data collection and analysis, visualization, and data curation. All the authors reviewed the manuscript.

Competing interests

The authors declare no competing interests.

Additional information

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